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VIEWS FROM THE SPACECRAFT
DURING APOLLO 10 (MISSION F)
MAY 18, 1969 LAUNCH DATE

Flight Analysis Branch

MISSION PLANNING AND ANALYSIS DIVISION



MANNED SPACECRAFT CENTER
HOUSTON, TEXAS

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PROJECT APOLLO

VIEWS FROM THE SPACECRAFT DURING APOLLO 10
(MISSION F) MAY 18, 1969 LAUNCH DATE

By Alfred N. Lunde
Flight Analysis Branch

April 22, 1969

MISSION PLANNING AND ANALYSIS DIVISION
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
MANNED SPACECRAFT CENTER
HOUSTON, TEXAS

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VIEWS FROM THE SPACECRAFT DURING APOLLO 10 (MISSION F)

MAY 18, 1969 LAUNCH DATE

By Alfred N. Lunde

SUMMARY

The purpose of this document is to visually depict various aspects of the Apollo 10 (Mission F) lunar flight. Views of the earth and the moon as seen from the spacecraft are shown during the translunar and transearth coast phases as well as the view from the spacecraft during critical maneuvers. The data should prove invaluable in assuring the crew that maneuver attitudes are correct. All data presented in this report are for the first opportunity, 72° launch azimuth, May 18, 1969 launch date.

INTRODUCTION

The geometry of a lunar mission can be very difficult to visualize. The primary objective of this report is to provide views from the spacecraft during Apollo 10 (Mission F) because a knowledge of how the spacecraft should be oriented with respect to familiar objects visible from the spacecraft window would be invaluable for performance of the various maneuvers.

A detailed visual representation of Apollo 10 (Mission F) for the May 17, 1969 launch date is presented in reference 1. Because of the 1-day slip in the launch date, most of the data in reference 1 are no longer applicable to the Apollo 10 flight. A discussion of the trajectory geometry and the general information are presented in reference 1.

In the figures for the lunar orbit phase section, the location of the planets Venus, Mars, Jupiter, and Saturn has been shown.

SYMBOLS

c.g.	center of gravity
CDH	constant delta height
CM	command module
CSI	concentric sequencing initiation
CSM	command and service modules
DOI	descent orbit insertion
EI	entry interface
g.e.t.	ground elapsed time
h_E	altitude above earth's surface
h_M	altitude above moon's surface
LOI	lunar orbit insertion
LM	lunar module
PTC	passive thermal control
R_E	radius from center of earth
R_M	radius from center of moon
SEQ	star identification number
SM	service module
TEC	transearth coast
TEI	transearth injection
TLC	translunar coast
TLI	translunar injection
TPI	terminal phase initiation
V_i	inertial velocity

DISCUSSION OF THE DATA

The geometry associated with the Apollo 10 lunar mission is presented in figures 1 through 5. A detailed description of figures 1 through 4 can be found in reference 1. The nominal F mission rendezvous is presented in figure 5.

Translunar Injection Burn

The beginning, middle, and end of the TLI burn are shown in figure 6. The maneuver is executed in a heads down position. The horizon is in darkness until toward the end of the burn. The TLI burn places the spacecraft on its lunar trajectory so that at the end of the burn the velocity is 35 591 fps.

Earth and Moon Views During TLC

The earth is shown in figure 7 with a constant field of view. Because the earth gets quite small as the spacecraft progresses on its lunar trajectory, the earth with a variable field of view is presented in figure 8. The purpose of the enlarged views of the earth is to show details such as continents and terminator. Because these views are almost identical to the views shown on pages 60 through 77 in reference 1, only a few TLC variable field views are shown in this report. The reader who desires to find out what portion of the earth is visible to the crew every hour during TLC should consult the above mentioned pages in reference 1.

Views of the moon are presented in figures 9 and 10. Because of the earth-moon-sun geometry at this particular time, the moon will be almost totally dark as viewed from the spacecraft on the approach trajectory.

Lunar Orbit Insertion Maneuver

The beginning, middle, and end of the LOI burn are depicted in figure 11. There is a rather large yaw attitude component during this burn designed to place the spacecraft in an orbit similar to that of the lunar landing mission. The crew are in a heads down position during this burn, and the burn is performed in a retrograde attitude to brake the trajectory speed so that a lunar orbit may be achieved.

Lunar Orbit Phase

Various LM events after separation from the CSM and prior to docking again with the CSM are shown in figure 12. The view from the commander's front LM window and from the docking window are shown with the correct burn attitude for DOI burn, phasing burn, LM descent stage jettison burn, insertion burn, CSI burn, CDH burn, and the TPI burn. The reader should consult figure 5 for a better understanding of those views.

Transearth Injection Maneuver

As with TLI and LOI, the beginning, middle, and end of the TEI burn are shown in the correct burn attitude. This maneuver is a posigrade burn designed to free the spacecraft from the lunar gravitational attraction. The spacecraft attains a velocity of 8958 fps at the end of the burn to return the spacecraft to earth in approximately 54.5 hours.

Post-TEI Views

The four post-TEI views depict the view from the spacecraft as the earth comes into view over the lunar horizon. The Southeast Asia portion of the earth is visible at this time.

Transearth Coast

As with the translunar coast, the views of the earth and the moon are shown at various times during the coast period (figs. 15, 16, 17, and 18). During this coast period, approximately half of the earth and moon are in sunlight as seen from the spacecraft. The spacecraft leaves the lunar gravitational sphere of influence at approximately 148 hours g.e.t., at which time the velocity will gradually increase until it reaches 36 309 fps at entry.

Entry

The entry phase is shown in figure 19. The SM is jettisoned approximately 15 minutes prior to entry interface, and the CM is in a heatshield forward attitude. The angle between the spacecraft X-axis and the earth horizon is held at $+31.7^\circ$, which can be monitored on the 31.7° scribe on the window. The moon is visible during part of the entry phase. The entry REFSMMAT's were obtained from reference 2.

(Most of the vectors needed to generate the data shown in this report were obtained from reference 3.)

CONCLUSIONS

An understanding of spacecraft attitudes with respect to the sun, earth, moon, and stars is particularly useful to verify maneuver attitudes normally described by IMU gimbal angles. This information is especially useful for Apollo 10 (Mission F) because IMU gimbal angles are referenced to several specific inertial orientations (REFSMMAT) instead of to preferred platform alinements.

This report has presented numerous figures which depict the view from the Apollo 10 (Mission F) windows: star field, earth and moon terminators, and horizon orientations are included. This information should prove invaluable in assuring the crew that maneuver attitudes are correct.

TABLE I. - STAR IDENTIFICATION CATALOGUE

SEQ NO.	IDENTIFICATION	DECIMAL	RIGHT ASCENSION HRS	MIN	SEC	DEGREES	DECLINATION DEG	MIN	SEC	MAG	JO	IDENTIFICATION
1	3330	.00275000	.0	.0	9.9	-6.20061110	-6.0	12.0	31.0	4.66	30	PSC
2		.03244444	.0	.0	56.8	-17.53083300	-17.0	31.0	51.0	4.62	2	CET
3		.05905555	.0	3.0	32.4	-5.90333330	-5.0	54.0	12.0	4.66	33	PSC
4	127 ALPHERATZ	.10955555	.0	6.0	34.4	28.89722100	28.0	53.0	50.0	2.15	21	AND
5	147 CAPH	.12163889	.0	7.0	17.9	58.95666000	58.0	57.0	24.0	2.42	11	CAS
6	158	.12733333	.0	7.0	38.4	-45.94055500	-45.0	56.0	26.0	3.94	0	CHE
7	238 ALGENIB	.19049999	.0	11.0	25.8	14.98916660	14.0	59.0	21.0	4.87	80	PEG
8	272	.21438888	.0	12.0	51.8	-19.12666600	-19.0	7.0	36.0	4.68	7	CET
9	334	.25427777	.0	15.0	15.4	38.48749900	38.0	29.0	15.0	4.44	24	J
10	342	.27486110	.0	16.0	29.5	36.59138800	36.0	35.0	29.0	4.51	25	S
11	388	.29405555	.0	17.0	38.6	-9.01777770	-9.0	4.0	4.0	3.75	8	I
12	401	.30430555	.0	18.0	15.5	-65.08055500	-65.0	4.0	50.0	4.34	0	Z
13	503 ALGENIB	.39897221	.0	23.0	58.3	-77.45138800	-77.0	27.0	5.0	2.90	0	MYI
14	516	.40808333	.0	24.0	29.1	-43.87388800	-43.0	52.0	28.0	3.90	0	K
15	519 ANKAA	.49936111	.0	29.0	33.4	-42.49611000	-42.0	29.0	48.0	2.44	0	A
16	625	.51655555	.0	30.0	59.6	-63.15833300	-63.0	9.0	30.0	4.52	0	TUC
17	645	.58341666	.0	35.0	13	62.73888900	62.0	48.0	20.0	4.24	15	K
18	729	.58349999	.0	35.0	16	33.52694400	33.0	31.0	37.0	4.44	29	P
19	727	.61166666	.0	35.0	42.0	53.70444400	53.0	42.0	16.0	3.72	17	Z
20	759	.62416665	.0	37.0	27.0	29.12194400	29.0	7.0	19.0	4.52	30	E
21	774	.64180554	.0	39.0	40.5	30.66972200	30.0	40.0	11.0	3.49	31	D
22	782 SCHEDIR	.66124999	.0	39.0	47.2	56.34583300	56.0	20.0	45.0	2.47	18	A
23	823	.69644444	.0	41.0	50.0	-46.27694400	-46.0	16.0	37.0	4.65	0	M
24	846 DIPMDA	.69722222	.0	41.0	47.2	-57.65899900	-57.0	39.0	18.0	4.53	0	M
25	865	.71275000	.0	42.0	45.9	-18.18333300	-18.0	10.0	42.0	2.24	16	CET
26	882	.75797221	.0	45.0	28.7	48.09305500	48.0	5.0	35.0	4.70	22	CAS
27	940	.78105554	.0	46.0	51.8	24.07694400	24.0	4.0	37.0	4.30	34	Z
28	963	.79791665	.0	46.0	58.0	7.39500000	7.0	23.0	42.0	4.55	63	D
29	962 ACHIRD	.79791665	.0	46.0	58.0	57.63055500	57.0	37.0	50.0	3.64	24	M
30	989	.90966666	.0	54.0	34.8	40.88661000	40.0	53.0	19.0	4.42	35	M
31	1117	.91338888	.0	54.0	48.2	60.52779000	60.0	31.0	40.0	2.30	27	B
32	1122	.92222221	.0	55.0	20.0	38.31000000	38.0	18.0	36.0	3.94	37	M
33	1136	.94866666	.0	56.0	55.2	-29.54638800	-29.0	32.0	45.0	4.62	38	M
34	1172	1.01872221	1.0	1.0	7.4	-29.54638800	-29.0	42.0	47.0	4.39	0	A
35	1258	1.05997221	1.0	3.0	35.9	86.07055500	86.0	4.0	14.0	4.50	71	E
36	1288	1.07541665	1.0	4.0	31.5	-46.90583300	-46.0	54.0	21.0	3.35	0	B
37	1335	1.11380555	1.0	6.0	49.7	-10.36722100	-10.0	22.0	2.0	3.60	31	M
38	1384	1.11527777	1.0	6.0	55.0	-55.43299900	-55.0	25.0	57.0	4.13	0	Z
39	1387	1.12433332	1.0	7.0	27.6	47.05555500	47.0	3.0	20.0	4.28	42	V
40	1394	1.12941666	1.0	7.0	45.9	35.43555500	35.0	26.0	8.0	2.37	43	B
41	1400 MIRACH	1.14930554	1.0	8.0	57.5	54.96916600	54.0	57.0	51.0	4.52	33	J
42	1424	1.14930554	1.0	9.0	43.6	29.90916600	29.0	54.0	15.0	4.70	83	V
43	1441	1.16211109	1.0	9.0	43.6	24.39861100	24.0	23.0	55.0	4.64	85	V
44	1474	1.19736110	1.0	11.0	50.5	27.08055500	27.0	4.0	50.0	4.67	90	U
45	1591	1.29277777	1.0	22.0	32.2	-8.36361110	-8.0	21.0	49.0	3.83	45	J
46	1695	1.37119444	1.0	23.0	30.5	60.05916600	60.0	3.0	15.0	2.80	37	B
47	1715 KSORA	1.37180554	1.0	23.0	30.5	-43.49722200	-43.0	29.0	50.0	3.40	0	B
48	1787	1.44744442	1.0	26.0	50.8	15.16883320	15.0	9.0	57.0	3.72	99	M
49	1839	1.49344443	1.0	29.0	36.4	-49.25916600	-49.0	15.0	15.0	3.96	0	D
50	1847	1.49683331	1.0	29.0	47.7	41.23111100	41.0	13.0	52.0	4.18	50	U
51	1948	1.57888888	1.0	34.0	44.0	48.45166600	48.0	27.0	6.0	3.77	51	AND
52	1966	1.59719443	1.0	35.0	49.9	-57.41416600	-57.0	24.0	51.0	4.60	0	A
53	1979 ACHERNAR	1.60686110	1.0	36.0	24.7	5.31111110	5.0	18.0	40.0	4.68	106	M
54	2055	1.66011110	1.0	39.0	36.4	50.51305500	50.0	30.0	47.0	4.20	0	V
55	2102	1.69091664	1.0	41.0	27.3							

KAITOS

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

54	2123	1.70736109	1+0	42+0	26+5	-16+12111000	-16+0	7+0	16+0	3+65	52 T	CET
56	2139	1.72569442	1+0	43+0	32+5	8+98222220	8+0	58+0	56+0	4+50	110 0	PSC
58	2249	1.82886110	1+0	49+0	43+9	-10+50722210	-10+0	30+0	33+0	3+92	55 Z	CET
59	2272	1.85133332	1+0	51+0	4+8	29+74249900	29+0	44+0	46+0	3+58	2 A	TRI
60	2291	1.86008333	1+0	51+0	36+3	19+12277700	19+0	7+0	22+0	4+75	5 6	ARI
61	2309	1.86424999	1+0	51+0	51+3	63+49861100	63+0	29+0	25+0	3+44	45 E	CAS
62	2303	1.87072220	1+0	52+0	14+6	-48+47321000	-48+0	26+0	25+0	4+41	0 Y	PHE
63	2309	1.87836109	1+0	52+0	42+1	20+63777000	20+0	38+0	16+0	2+72	6 B	ARI
64	2331	1.90074998	1+0	54+0	2+7	-67+81916600	-67+0	9+0	9+0	4+72	0 K	HYI
65	2339	1.90994443	1+0	54+0	35+8	-51+78277000	-51+0	46+0	58+0	3+73	0 K	ERI
66	2369	1.92966665	1+0	55+0	46+0	-47+55555500	-47+0	33+0	20+0	4+74	0 A	PHE
67	2405	1.94111110	1+0	57+0	40+0	-61+73972100	-61+0	44+0	23+0	3+02	0 A	HYI
68	2419	1.97258331	1+0	58+0	21+3	-21+24666600	-21+0	14+0	48+0	4+18	59 U	CET
69	2424	1.98408331	1+0	59+0	2+7	70+73861000	70+0	44+0	19+0	4+61	48	CAS
70	2243	ALRUCCABA	1+0	59+0	24+3	89+10222100	89+0	6+0	8+0	2+12	0 A	UMI
71	2452	KAITAIN	2+0	0	14+0	2+59555550	2+0	35+0	44+0	4+33	113 A	PSC
72	2445	2+00475000	2+0	0	24+3	72+25333300	72+0	15+0	12+0	4+06	50	CAS
73	2477	ALAMAK	2+0	1+0	44+5	42+16277000	42+0	9+0	46+0	4+24	0 6	AND
74	2506	2+02902770	2+0	2+0	55+3	-29+48416700	-29+0	27+0	51+0	4+74	0 M	FOR
75	2538	2+00468320	2+0	5+0	11+7	23+29777700	23+0	17+0	52+0	2+23	13 A	ARI
76	2572	2+12422210	2+0	7+0	27+2	34+82250000	34+0	49+0	21+0	3+08	4 B	TRI
77	2454	2+19902770	2+0	11+8	8+5	8+68333300	8+0	41+0	1+0	4+54	45 C	CET
78	2742	2+25377770	2+0	15+0	13+6	33+68338000	33+0	41+0	11+0	4+07	9 6	TRI
79	2756	2+25430550	2+0	15+0	15+5	-51+67381100	-51+0	40+0	25+0	3+78	0 V	ERI
80	2796	2+29291660	2+0	17+0	34+5	-3+13555550	-3+0	8+0	8+0	2+00V	48 0	CET
81	2872	2+35200000	2+0	21+0	7+2	-68+81833200	-68+0	49+0	6+0	4+26	0 0	HYI
82	2954	2+43241000	2+0	25+0	42+1	-47+84027700	-47+0	51+0	37+0	4+44	0 K	ERI
83	2952	2+43588880	2+0	26+0	9+2	67+24666600	67+0	14+0	48+0	4+59	0 I	CAS
84	2960	2+43824990	2+0	26+0	17+7	8+30416660	8+0	18+0	15+0	4+34	73 C	CET
85	3192	2+62808320	2+0	37+0	41+1	-17861111	0	10+0	43+0	4+04	82 D	CET
86	3217	2+64108330	2+0	38+0	27+9	-43+04111100	-43+0	2+0	28+0	4+53	0	ERI
87	3240	2+65074990	2+0	39+0	2+7	-68+41638900	-68+0	24+0	59+0	4+26	0 E	HYI
88	3237	2+65749970	2+0	39+0	17+1	-40+00444400	-40+0	14+0	14+0	4+04	0 I	ERI
89	3273	2+68986110	2+0	41+0	23+5	27+55444000	27+0	33+0	34+0	4+58	35	ARI
90	3276	2+69141660	2+0	41+0	29+1	3+08916670	3+0	5+0	21+0	3+58	8 6	CET
91	3277	2+69461110	2+0	41+0	47+8	49+08166600	49+0	4+0	54+0	4+22	13 J	PER
92	3300	2+70258330	2+0	42+0	27+3	-14+00611100	-14+0	10	22+0	4+39	89 P	CET
93	3309	2+71744440	2+0	43+0	2+8	9+96250000	9+0	58+0	33+0	4+34	87 M	CET
94	3318	2+72447210	2+0	43+0	28+1	-18+71972200	-18+0	43+0	11+0	4+61	1 Y	ERI
95	3354	2+76363890	2+0	45+0	49+1	29+10277800	29+0	6+0	10+0	4+62	39	ARI
96	3387	2+79374990	2+0	47+0	37+5	-32+52221000	-32+0	33+0	8+0	4+50	0 8	FOR
97	3391	2+79843890	2+0	47+0	55+1	27+11760000	27+0	7+0	3+0	3+68	41	ARI
98	3390	2+80213890	2+0	48+0	7+7	55+75166600	55+0	45+0	6+0	3+93	15 M	PER
99	3401	2+80611110	2+0	48+0	22+0	38+17583300	38+0	10+0	33+0	4+27	16	PER
100	3419	2+82252770	2+0	49+0	21+1	34+91694400	34+0	55+0	1+0	4+67	17	PER
101	3463	2+84461100	2+0	50+0	40+6	-75+20999900	-75+0	12+0	36+0	4+70	0 N	HYI
102	3462	2+86272220	2+0	51+0	45+8	52+62055500	52+0	37+0	14+0	4+06	18 Y	PER
103	3539	2+891191660	2+0	54+0	42+9	-99+03888900	-99+0	2+0	11+0	4+05	3 M	ERI
104	3567	2+949191660	2+0	56+0	30+9	39+52388800	39+0	31+0	26+0	4+62	22 P	PER
105	3584	2+94988880	2+0	56+0	54+0	-40+44416660	-40+0	26+0	39+0	3+42	0 J	ERI
106	3582	2+95341660	2+0	57+0	12+3	21+20138900	21+0	12+0	5+0	4+44	48 E	ARI
107	3595	2+96391660	2+0	57+0	50+1	8+76888890	8+0	46+0	8+0	4+69	9 L	CET
108	3643	HEKAB	3+0	0	26+8	3+95361110	3+0	57+0	13+0	2+82	92 A	CET
109	3649	3+00744440	3+0	0	50+9	-23+76555500	-23+0	45+0	38+0	4+16	11 Y	ERI
110	3644	3+03747220	3+0	2+0	14+9	53+37083300	53+0	22+0	15+0	3+08	23 6	PER
111	3682	3+04877770	3+0	2+0	55+6	38+70583300	38+0	42+0	21+0	3+00V	25	PER
112	3733	ALGOL	3+0	5+0	53+0	40+82222100	40+0	49+0	20+0	2+30	24 8	PER
113	3740	GORGONA	3+0	6+0	31+8	49+46811100	49+0	28+0	52+0	4+17	0 I	PER

CYNSR
OKDA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

114	3755	MISAM	3+11874990	3 0	7 0	7 5	44722611000	44 0	43 0	34 0	4 00	27 K	PER
115	3805	ROUTEIN	3+16038880	3 0	9 0	37 4	19+59555500	19 0	35 0	44 0	4 53	57 D	ARI
116	3831		3+17628880	3 0	10 0	35 0	-29+12416600	-29 0	7 0	27 0	3 95	0 A	FOR
117	3979		3+29930550	3 0	17 0	57 5	-21+88416600	-21 0	53 0	3 0	4 72	16 T	ERI
118	3981		3+30361110	3 0	18 0	13 0	28+92277800	28 0	55 0	22 0	4 72	0	ARI
119	4000		3+30886100	3 0	18 0	31 9	-43+20277700	-43 0	12 0	10 0	4 30	82	ERI
120	4041	MIRFAK	3+36355550	3 0	21 0	48 8	49+73833300	49 0	44 0	18 0	1 90	33 A	PER
121	4070		3+38211100	3 0	22 0	55 6	8+90694440	8 0	54 0	25 0	3 80	1 0	TAU
122	4107		3+42113880	3 0	25 0	16 1	9+61194450	9 0	36 0	43 0	3 75	2 C	TAU
123	4113		3+4367210	3 0	26 0	13 1	59+82027700	59 0	49 0	13 0	4 42	2	CAM
124	4133		3+44758320	3 0	26 0	51 3	49+38916600	49 0	23 0	21 0	4 67	34	PER
125	4158		3+4682770	3 0	28 0	5 8	47+87611100	47 0	52 0	34 0	4 55	5 S	PER
126	4184		3+4822770	3 0	28 0	56 2	12+81805550	12 0	49 0	5 0	4 28	5	TAU
127	4244		3+52133330	3 0	31 0	16 8	-9+57555550	-9 0	34 0	32 0	3 81	18 E	ERI
128	4258		3+53733330	3 0	32 0	14 4	-21+7916600	-21 0	44 0	57 0	4 34	19 T	ERI
129	4287		3+56555550	3 0	33 0	59 4	48+07777700	48 0	4 0	10 0	4 26	37 V	PER
130	4313		3+58474990	3 0	35 0	5 1	6+29166666	6 0	17 0	30 0	4 40	10	TAU
131	4329		3+5972770	3 0	35 0	50 2	-40+38861000	-40 0	23 0	19 0	4 58	0	ERI
132	4427		3+6772220	3 0	40 0	25 4	47+67722100	47 0	40 0	38 0	3 10	39 D	PER
133	4455		3+69225000	3 0	41 0	32 1	-37+42305500	-37 0	25 0	23 0	4 64	0	ERI
134	4450	RANA	3+69283330	3 0	41 0	34 2	-9+80083330	-9 0	52 0	51 0	3 72	23 D	ERI
135	4461	ATIKS	3+70197210	3 0	42 0	7 1	32+17888800	32 0	10 0	44 0	3 94	38 0	PER
136	4477	ELECTRA	3+71322220	3 0	42 0	47 6	24+00472200	24 0	8 0	17 0	3 81	17	TAU
137	4474		3+71372220	3 0	42 0	48 5	42+46972100	42 0	28 0	11 0	3 93	41 N	PER
138	4486	TAYGETA	3+71866660	3 0	43 0	7 2	24+35889900	24 0	21 0	32 0	4 37	19	TAU
139	4500	MAIA	3+72899990	3 0	43 0	48 4	24+25972100	24 0	15 0	35 0	4 02	20	TAU
140	4517		3+72922220	3 0	43 0	45 2	-64+91694300	-64 0	55 0	1 0	3 80	0	RET
141	4512	MEROPE	3+73741660	3 0	44 0	19 7	23+84083300	23 0	50 0	27 0	4 25	23	TAU
142	4525		3+74141660	3 0	44 0	29 1	-12+21027760	-12 0	12 0	37 0	4 64	26 P	ERI
143	4547		3+75569440	3 0	45 0	20 5	-23+35194300	-23 0	21 0	7 0	4 33	27 Y	ERI
144	4541	ALCYONE	3+75666660	3 0	45 0	24 0	23+99833300	23 0	59 0	54 0	2 96	25 M	TAU
145	4553		3+77150330	3 0	46 0	17 7	65+41999900	65 0	25 0	12 0	4 71	0	CAM
146	4557		3+77719440	3 0	46 0	37 9	71+22694900	71 0	13 0	37 0	4 67	0	6
147	4586	ATLAS	3+78461110	3 0	47 0	4 6	23+94778000	23 0	56 0	52 0	3 80	27	TAU
148	4633		3+78602770	3 0	47 0	45 7	-74+34666600	-74 0	20 0	48 0	4 24	0	6
149	4624		3+80238880	3 0	48 0	8 6	-36+30527700	-36 0	18 0	19 0	4 24	0	ERI
150	4688	MENKIB	3+86544440	3 0	51 0	55 6	31+78111100	31 0	46 0	52 0	2 91	44 Z	PER
151	4758		3+92497220	3 0	55 0	29 9	39+91055500	39 0	54 0	38 0	2 96	45 E	PER
152	4778	ZAURAK	3+93916660	3 0	56 0	23 7	-13+40694440	-13 0	36 0	25 0	3 19	34 6	ERI
153	4779		3+94480550	3 0	56 0	41 3	35+61944000	35 0	41 0	31 0	4 05	46 C	PER
154	4808		3+96977770	3 0	58 0	11 2	-81+49861100	-81 0	29 0	55 0	4 41	0	RET
155	4801		3+97386100	3 0	58 0	25 9	-24+11444400	-24 0	8 0	52 0	4 69	36 T	ERI
156	4805		3+97897210	3 0	58 0	44 3	12+39277770	12 0	23 0	34 0	3 90	35 L	TAU
157	4855		4+0041660	4 0	1 0	23 1	-62+25666600	-62 0	15 0	24 0	4 46	0	RET
158	4862		4+02152770	4 0	2 0	17 5	5+89361110	5 0	53 0	37 0	4 50	38 M	TAU
159	4897		4+04369440	4 0	2 0	37 3	21+98777700	21 0	59 0	16 0	4 50	37	TAU
160	4924		4+06613880	4 0	3 0	58 1	50+25605500	50 0	15 0	29 0	4 33	47 L	PER
161	4947		4+10186100	4 0	6 0	6 7	47+62083300	47 0	37 0	15 0	4 03	48 U	PER
162	5056	BEID	4+16924990	4 0	10 0	9 3	-6+92749990	-6 0	55 0	39 0	4 14	38 0	ERI
163	5099		4+20533330	4 0	12 0	19 2	48+32222200	48 0	19 0	20 0	4 29	51 M	PER
164	5121		4+21400000	4 0	12 0	50 4	-42+37999900	-42 0	48 0	48 0	3 83	0 A	HOR
165	5134		4+22719430	4 0	13 0	37 9	8+80611110	8 0	48 0	22 0	4 32	49 M	TAU
166	5138		4+22766660	4 0	13 0	39 6	-7+70611110	-7 0	42 0	22 0	4 49	40 0	ERI
167	5164		4+23283320	4 0	13 0	58 2	-62+54110000	-62 0	33 0	40 0	3 36	0 A	RET
168	5179		4+25177770	4 0	15 0	6 4	-51+57416600	-51 0	34 0	27 0	4 36	0	6
169	5194		4+26005550	4 0	15 0	36 2	50+21138900	50 0	12 0	41 0	4 60	0	6
170	5194		4+26458320	4 0	15 0	52 5	-59+38583300	-59 0	23 0	9 0	4 42	0	RET
171	5201		4+27613880	4 0	16 0	34 1	-33+88277700	-33 0	52 0	58 0	3 59	41 U	ERI

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

172	5226	4+29663880	4+0	17+0	47+9	15+544444450	15+0	32+0	40+0	3+94	54 6	TAU
173	5304	4+34855550	4+0	20+0	54+8	17+461944400	17+0	27+0	43+0	3+93	61 0	TAU
174	5349	4+37866660	4+0	22+0	43+2	-34+09722100	-34+0	5+0	50+0	4+06	43 U	ERI
175	5350	4+38799990	4+0	23+0	16+8	22+21527700	22+0	12+0	55+0	4+34	45 K	TAU
176	5354	4+39102780	4+0	23+0	27+7	17+84944400	17+0	50+0	56+0	4+24	68 U	TAU
177	5370	4+40350000	4+0	24+0	12+6	22+73583300	22+0	44+0	9+0	4+40	49 U	TAU
178	5375	4+40580550	4+0	24+0	20+9	15+54027700	15+0	32+0	25+0	4+60	71	TAU
179	5430	4+44283320	4+0	26+0	34+3	19+10416600	19+0	6+0	15+0	3+63	74 E	TAU
180	5433	4+44286100	4+0	26+0	34+3	15+80583320	15+0	53+0	9+0	4+04	77 J	TAU
181	5436	4+44433320	4+0	26+0	39+6	15+79472210	15+0	47+0	41+0	3+62	78 J	TAU
182	5558	4+53100000	4+0	31+0	51+6	14+77222200	14+0	46+0	20+0	4+75	86 M	TAU
183	5572	4+53561100	4+0	32+0	8+2	-29+83638900	-29+0	50+0	11+0	4+59	50 U	ERI
184	5600	4+55397210	4+0	33+0	14+3	-55+11694400	-55+0	7+0	1+0	3+47	0 A	DOB
185	5599	4+56213880	4+0	33+0	43+7	10+09055500	10+0	5+0	26+0	4+38	88	TAU IUM
186	5605	4+56516660	4+0	33+0	54+6	16+44037800	16+0	26+0	25+0	1+04	87 A	TAU
187	5614	4+56980550	4+0	34+0	11+3	-30+63305500	-30+0	37+0	59+0	3+88	52 U	ERI
188	5609	4+57097220	4+0	34+0	15+5	41+19472200	41+0	11+0	41+0	4+46	58	PER
189	5617	4+57613890	4+0	34+0	34+0	-3+42277700	-3+0	25+0	22+0	4+12	48 M	ERI
190	5645	4+60330550	4+0	36+0	11+9	12+42222100	12+0	26+0	32+0	4+30	90	TAU
191	5657	4+60961100	4+0	36+0	34+6	-14+37111100	-14+0	22+0	16+0	3+98	53	ERI
192	5695	4+64849990	4+0	38+0	54+6	-19+73750000	-19+0	44+0	15+0	4+54	54	ERI
193	5708	4+65719940	4+0	39+0	25+9	-41+92972200	-41+0	55+0	47+0	4+52	0 A	CAE
194	5714	4+66902770	4+0	40+0	8+5	22+89138000	22+0	53+0	29+0	4+33	94 Y	TAU
195	5794	4+72916660	4+0	43+0	45+0	-3+31750000	-3+0	19+0	3+0	4+18	57 M	ERI
196	5875	4+7987220	4+0	47+0	56+3	6+90166670	6+0	54+0	6+0	3+31	1 P	ORI
197	5892	4+81169440	4+0	48+0	42+1	8+84166660	8+0	50+0	30+0	4+35	2 P	ORI
198	5911	4+8223320	4+0	49+0	20+4	5+54666660	5+0	32+0	48+0	3+78	3 P	ORI
199	5924	4+84261100	4+0	50+0	33+4	6+22853200	6+0	17+0	9+0	4+38	9 A	CAM
200	5954	4+85288880	4+0	51+0	10+4	-5+51000000	-5+0	30+0	36+0	4+45	61 A	ERI
201	5978	4+8737770	4+0	52+0	25+6	2+38472220	2+0	23+0	5+0	3+90	8 P	ORI
202	5987	4+8827770	4+0	52+0	58+0	10+09666650	10+0	5+0	48+0	4+74	7 P	ORI
203	6025	4+90669440	4+0	54+0	24+1	13+46055540	13+0	27+0	38+0	4+28	9 0	ORI
204	6017	4+90788880	4+0	54+0	28+4	53+69833000	53+0	41+0	54+0	4+44	7	CAM
205	6029	4+91166100	4+0	54+0	42+7	33+11249900	33+0	6+0	45+0	2+90	3 1	AUR
206	6048	4+94552770	4+0	54+0	43+9	1+66166665	1+0	39+0	42+0	4+73	10 P	ORI
207	6123	4+99088880	4+0	59+0	27+2	43+77333300	43+0	44+0	24+0	3+00V	7 E	AUR
208	6137	5+00047210	5+0	60	1+7	41+02666600	41+0	1+0	36+0	3+90	8 2	AUR
209	6136	5+00494440	5+0	60	17+8	60+39361100	60+0	23+0	37+0	4+22	10 8	CAM
210	6158	5+01469440	5+0	60	1+1	21+54166600	21+0	32+0	30+0	4+70	102 1	TAU
211	6191	5+0427770	5+0	60	34+0	15+35494450	15+0	21+0	25+0	4+65	11	ORI
212	6212	5+05244430	5+0	60	8+8	-35+52999900	-35+0	31+0	48+0	4+62	0 6	CAE
213	6231	5+06630550	5+0	60	58+7	-22+41944400	-22+0	25+0	1+0	3+47	2 E	LEP
214	6226	5+06761110	5+0	60	3+4	41+18888800	41+0	11+0	20+0	3+48	10 M	AUR
215	6274	5+10213880	5+0	60	7+7	-5+13027770	-5+0	39+0	49+0	2+92	67 8	ERI
216	6304	5+12449990	5+0	70	28+2	-8+79749990	-8+0	51+0	4+34	4+34	49 L	ERI
217	6374	5+1772210	5+0	10+0	39+8	-11+80722200	-11+0	54+0	35+0	4+54	3 1	LEP
218	6382	5+18930550	5+0	11+0	21+5	-16+24983300	-16+0	14+0	45+0	3+50	5 M	LEP
219	6381	5+19099990	5+0	11+0	27+6	2+82083330	2+0	59+0	15+0	4+64	17 M	ORI
220	6387	5+19355540	5+0	11+0	36+8	-12+98166660	-12+0	58+0	54+0	4+46	4 K	LEP
221	6410	5+21424990	5+0	12+0	51+3	-8+24083330	-8+0	14+0	27+0	1+34	19 8	ORI
222	6427	5+23500000	5+0	14+0	8+0	45+84844400	45+0	57+0	52+0	4+21	13 A	AUR
223	6460	5+26583320	5+0	15+0	54+3	-6+88083330	-6+0	52+0	51+0	3+88	20 Y	ORI
224	6531	5+29936110	5+0	17+0	57+7	-13+21166660	-13+0	12+0	42+0	4+59	6 L	LEP
225	6559	5+31588880	5+0	18+0	57+2	-21+27361100	-21+0	16+0	25+0	4+73	0	LEP
226	6579	5+33291660	5+0	19+0	58+5	-4+1555555	-4+0	24+0	54+0	4+65	22 0	ORI
227	6646	5+37099990	5+0	22+0	15+6	-7+83888880	-7+0	50+0	20+0	4+21	29	ORI
228	6655	5+37861100	5+0	22+0	43+0	-2+42777770	-2+0	25+0	40+0	3+44	28 M	ORI
229	6660	5+38213880	5+0	22+0	55+7	1+81583333	1+0	48+0	57+0	4+73	25	ORI

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

230	668	BELLATRIX	5-38752780	5-0	23-0	15-1	6-31944440	4-0	19-0	10-0	1-70	24 6	ORI
231	681	ELNATH	5-40130550	5-0	24-0	4-7	28-57972200	28-0	34-0	47-0	1-78	18 8	TAU
232	6713		5-41649440	5-0	25-0	1	3-06666660	3-0	47-0	10-0	4-66	30 Y	ORI
233	6762	NINAL	5-44574990	5-0	26-0	44-7	-20-70611000	-20-0	47-0	10-0	2-96	9 8	LEP
234	6813		5-48183330	5-0	28-0	54-6	5-92277770	5-0	55-0	22-0	4-32	32	ORI
235	6846		5-49947220	5-0	29-0	58-1	-35-49527700	-35-0	29-0	43-0	3-72	0 E	COL
236	6841		5-50266660	5-0	30-0	9-4	18-56972200	18-0	34-0	11-0	4-70	119	TAU
237	6847	MINTAKA	5-50361100	5-0	30-0	13-0	-32-261110	-7-0	19-0	25-0	2-48	34 0	ORI
238	6850		5-50394430	5-0	30-0	14-2	-7-32503330	-7-0	19-0	33-0	4-64	36 0	ORI
239	6875	ARNEB	5-51975000	5-0	31-0	11-1	-17-04611000	-17-0	50-0	46-0	2-69	11 A	LEP
240	6907		5-54830550	5-0	32-0	53-9	9-46750000	9-0	28-0	3-0	4-53	37 V	ORI
241	6915	MEKA	5-55347220	5-0	33-0	12-5	9-91222200	9-0	54-0	44-0	3-66	39 L	ORI
242	6944		5-55530550	5-0	33-0	19-1	-62-51250000	-62-0	30-0	45-0	4-00V	0 8	DOR
243	6926		5-55555540	5-0	33-0	20-0	-6-02308090	-4-0	1-0	25-0	4-67	0	ORI
244	6934		5-56097220	5-0	33-0	39-5	-4-85999990	-4-0	51-0	36-0	4-65	42	ORI
245	6937	MATYSA	5-56199990	5-0	33-0	43-2	-5-93138890	-5-0	55-0	53-0	2-87	44 I	ORI
246	6960	ALNILAM	5-57394440	5-0	34-0	26-2	-1-22277777	-1-0	13-0	22-0	1-75	46 E	ORI
247	6972		5-58302780	5-0	34-0	58-9	9-27305560	9-0	16-0	23-0	4-39	40 V	ORI
248	6985		5-59252780	5-0	35-0	33-1	21-12277700	21-0	7-0	22-0	3-00	123 Z	TAU
249	7031		5-61647220	5-0	36-0	59-3	-2-61808880	-2-0	37-0	8-0	3-78	48 S	ORI
250	7042	PHAKT	5-62227770	5-0	37-0	20-2	4-10305550	4-0	6-0	11-0	4-54	47 M	ORI
251	7078		5-63966660	5-0	38-0	22-8	-34-09166600	-34-0	6-0	30-0	2-75	0 A	COL
252	7089	ALNITAK	5-64986110	5-0	38-0	59-5	-1-95972221	-1-0	57-0	35-0	2-05	50 Z	ORI
253	7197		5-71672220	5-0	43-0	7-2	-22-45861100	-22-0	27-0	31-0	3-80	13 6	LEP
254	7246		5-74516660	5-0	45-0	42-6	-65-74661000	-65-0	44-0	55-0	4-52	0 D	DOR
255	7247		5-75613880	5-0	45-0	22-1	-14-83388870	-14-0	50-0	2-0	3-67	14 Z	LEP
256	7264	SAIPH	5-76824990	5-0	46-0	5-7	-9-6803320	-9-0	40-0	51-0	2-80	53 K	ORI
257	7287		5-77425000	5-0	46-0	27-3	-51-07861100	-51-0	4-0	43-0	3-94	0 B	PIC
258	7277		5-77913890	5-0	46-0	49-9	39-17111000	39-0	10-0	16-0	4-44	29 Y	AUR
259	7334		5-81722220	5-0	49-0	3-8	39-14027700	39-0	8-0	25-0	4-18	32 M	AUR
260	7353		5-81983330	5-0	49-0	11-4	-56-17472200	-56-0	10-0	29-0	4-38	0 6	PIC
261	7364		5-82875000	5-0	49-0	43-5	-56-17472200	-56-0	10-0	50-0	4-62	0 6	COL
262	7362		5-83024990	5-0	49-0	48-9	-20-88033000	-20-0	36-0	20-0	4-54	134	TAU
263	7389		5-85211110	5-0	51-0	7-6	27-60555500	27-0	14-0	17-0	4-62	54 X	ORI
264	7419	BETELGEUSE	5-87180550	5-0	52-0	18-5	20-27138800	20-0	16-0	17-0	4-00V	58 A	ORI
265	7451		5-88794440	5-0	53-0	16-6	7-40194440	7-0	24-0	7-0	4-53	0	PIC
266	7477		5-89719440	5-0	53-0	49-9	-63-10027700	-63-0	6-0	1-0	4-53	0	PIC
267	7492		5-91350000	5-0	54-0	48-6	-14-17277780	-14-0	10-0	22-0	3-77	16 M	LEP
268	7536		5-93824990	5-0	56-0	17-7	-35-28611000	-35-0	17-0	10-0	4-36	0 6	COL
269	7521		5-94408330	5-0	56-0	38-7	54-28416600	54-0	17-0	3-0	3-88	33 0	AUR
270	7543	MENKALINAN	5-94933320	5-0	56-0	57-6	44-94583300	44-0	56-0	45-0	2-07	34 8	AUR
271	7557		5-95555550	5-0	57-0	20-0	37-21194300	37-0	12-0	43-0	2-71	37 J	AUR
272	7554		5-95611000	5-0	57-0	20-2	45-93555500	45-0	56-0	8-0	4-59	35 P	AUR
273	7591		5-96788880	5-0	58-0	4-4	-42-81638900	-42-0	48-0	59-0	4-03	0 M	COL
274	7597		5-97172220	5-0	58-0	18-2	-3-07416660	-3-0	4-0	27-0	4-68	0	ORI
275	7635		6-00761110	6-0	1-0	27-4	9-64888890	9-0	38-0	56-0	4-19	61 M	ORI
276	7675		6-03066670	6-0	1-0	50-4	20-14083300	20-0	8-0	27-0	4-71	62 X	ORI
277	7676		6-03319440	6-0	1-0	59-5	23-26944000	23-0	16-0	1-0	4-30	1	LEM
278	7742		6-07616660	6-0	4-0	34-2	-14-93083330	-14-0	55-0	51-0	4-67	18 J	LEP
279	7772		6-09288890	6-0	5-0	34-4	14-77416660	14-0	46-0	27-0	4-40	67 M	ORI
280	7889		6-16583330	6-0	9-0	57-0	14-21833320	14-0	13-0	6-0	4-35	70 C	ORI
281	7949	TEJAT PRIOR	6-21274990	6-0	12-0	45-9	22-51861100	22-0	31-0	7-0	3-00V	7 M	LEM
282	7981		6-21913890	6-0	13-0	8-9	29-51277700	29-0	30-0	46-0	4-45	44 K	AUR
283	7986		6-21913890	6-0	13-0	8-9	-6-26277700	-6-0	15-0	46-0	4-09	5 6	MON
284	8020		6-24988880	6-0	14-0	59-6	69-35277000	69-0	20-0	7-0	4-73	22	CAM
285	8062		6-25503320	6-0	15-0	18-3	-35-12605500	-35-0	7-0	41-0	4-51	0 K	COL
286	8068		6-27561110	6-0	16-0	32-2	59-02611000	59-0	1-0	34-0	4-42	2	LYN
287	8170	FURUD	6-31613880	6-0	18-0	58-1	-30-04666600	-30-0	2-0	48-0	3-10	1 Z	CMA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

288	6214		6.34722220	6.0	20.0	50.0	-33.4177700	25.0	4.0	3.98	3 0	COL
289	8208	TEJAT POSTERIOR	6.34730880	6.0	20.0	50.4	22.53333300	32.0	1.0	3.19	13 M	6EM
290	8223	MIRZAH	6.35263880	6.0	21.0	9.5	-17.93722100	17.0	58.0	1.99	2 B	CHA
291	8202		6.36522220	6.0	21.0	54.8	4.61194400	9.0	43.0	4.48	8 A	HOM
292	8302	SUMEL	6.36625000	6.0	23.0	10.5	-52.67611100	52.0	30.0	-0.86	0 A	CAR
293	8410	CANOPUS	6.44783330	6.0	26.0	52.2	-32.55694400	-32.0	33.0	4.40	0 L	CHA
294	8394		6.44808320	6.0	26.0	53.1	20.23583300	20.0	9.0	4.04	18 N	6EM
295	8413		6.45197220	6.0	27.0	7.1	-7.00716660	-7.0	33.0	4.64	11 B	HOM
296	8476		6.50661100	6.0	30.0	23.8	-23.39194400	-23.0	23.0	4.35	4 C	CHA
297	8506		6.51686110	6.0	31.0	1.7	7.35999900	7.0	21.0	4.50	13	HOM
298	8577		6.55980540	6.0	33.0	35.3	-22.93583300	-23.0	9.0	4.54	5 C	CHA
299	8604		6.57005540	6.0	34.0	12.2	-52.94638900	-52.0	47.0	4.44	0	CAR
300	8624		6.58594440	6.0	35.0	9.4	-19.22500000	-19.0	30.0	4.14	7 M	CHA
301	8633	ALHENA	6.59483330	6.0	35.0	41.4	16.43055500	16.0	50.0	1.93	24 0	6EM
302	8660		6.60583330	6.0	36.0	21.0	-18.20583300	-18.0	12.0	4.65	8 N	CHA
303	8675		6.61149990	6.0	36.0	41.4	-43.16444400	-43.0	9.0	3.18	0 M	PUP
304	8720		6.65083330	6.0	39.0	3.0	9.92722220	9.0	52.0	4.68	15	HOM
305	8786	HEBSUTA	6.65633320	6.0	41.0	4.8	25.16749900	25.0	10.0	3.18	27 E	6EM
306	8793		6.70025000	6.0	42.0	9.9	13.26472210	13.0	53.0	4.65	30	6EM
307	8823		6.72208320	6.0	43.0	19.6	12.93722220	12.0	50.0	3.40	31 C	6EM
308	8833	SIRIUS	6.72677770	6.0	43.0	36.4	-16.66466600	-16.0	40.0	-1.37	9 A	CHA
309	8892		6.74724990	6.0	46.0	2.1	2.45194400	2.0	7.0	4.70	18	HOM
310	8941		6.7722210	6.0	47.0	50.0	-21.90361000	-21.0	13.0	3.30	0 A	PIC
311	8976		6.80888880	6.0	48.0	32.0	-22.46694400	-22.0	20.0	3.78	13 K	CHA
312	8969		6.81777780	6.0	49.0	9.0	-50.57222200	-50.0	34.0	2.83	0 Y	PUP
313	8972		6.81825000	6.0	49.0	5.7	-53.58032000	-53.0	51.0	4.38	0	CAR
314	8989		6.84138880	6.0	50.0	29.0	34.00527800	34.0	19.0	3.64	34 J	6EM
315	9034		6.86724990	6.0	52.0	2.1	-20.17972200	-20.0	10.0	4.66	18	CHA
316	9051		6.87605540	6.0	52.0	33.8	-11.99361120	-11.0	59.0	4.25	14 J	CHA
317	9059		6.87783320	6.0	52.0	40.2	13.22361120	13.0	25.0	4.70	38	6EM
318	9059		6.8797210	6.0	52.0	40.7	-24.13916600	-24.0	8.0	4.12	16 0	CHA
319	9074		6.90175000	6.0	54.0	6.3	-20.09055500	-20.0	26.0	9.62	18 0	CHA
320	9082		6.90419440	6.0	54.0	15.1	58.47083300	58.0	15.0	4.54	38	LYN
321	9107		6.90958330	6.0	54.0	34.5	-17.00750000	-17.0	27.0	4.39	20 1	CHA
322	9073	ADHARA	6.91652770	6.0	54.0	59.5	77.02583300	77.0	1.0	9.75	24	CAM
323	9188	ADHARA	6.95416670	6.0	57.0	15.0	-28.92333300	-28.0	55.0	1.63	21 C	CHA
324	9274		7.00541660	7.0	1.0	19.5	-22.88361100	-22.0	53.0	3.68	22 B	CHA
325	9307		7.02605550	7.0	1.0	33.8	-23.78111000	-23.0	48.0	3.12	24 0	CHA
326	9313	MEKBUDA	7.03388880	7.0	2.0	2.0	20.62333300	20.0	29.0	3.90	43 2	6EM
327	9320	MULIPHEIN	7.03624990	7.0	2.0	10.5	-15.58027770	-15.0	34.0	4.07	23 0	CHA
328	9493	WEZEN	7.11613880	7.0	6.0	58.1	-24.33666600	-24.0	12.0	1.98	25 0	CHA
329	9494		7.14855550	7.0	8.0	54.8	30.30416600	30.0	18.0	4.48	46 7	6EM
330	9514		7.15088110	7.0	9.0	3.1	-70.49222100	-70.0	28.0	3.87	0 0	VOL
331	9518		7.16794440	7.0	10.0	4.6	-4.33333333	4.0	26.0	4.09	22 0	HOM
332	9569		7.19269440	7.0	11.0	33.7	-46.65999900	-46.0	42.0	4.47	0	PUP
333	9604		7.20783330	7.0	12.0	28.2	-44.58194400	-44.0	34.0	4.50	0 4	PUP
334	9608		7.21375000	7.0	12.0	49.5	-24.29111000	-24.0	17.0	4.66	27	CHA
335	9625		7.22316660	7.0	13.0	23.4	-26.71083300	-26.0	42.0	3.83	28 0	CHA
336	9706		7.26511110	7.0	15.0	54.4	-37.03361100	-37.0	1.0	2.74	0 P	PUP
337	9701		7.26805550	7.0	16.0	5.0	14.60499900	14.0	36.0	3.65	54 L	6EM
338	9747		7.2808890	7.0	16.0	51.2	-67.89333200	-67.0	53.0	4.02	0 0	VOL
339	9733		7.28936100	7.0	17.0	3.7	-36.66916600	-36.0	40.0	4.88	0 U	PUP
340	9736		7.28761110	7.0	17.0	15.4	-24.88944400	-24.0	53.0	4.40	30 7	CHA
341	9755	WASAT	7.30058330	7.0	18.0	2.1	22.04833300	22.0	2.0	3.51	58 0	6EM
342	9886	ALUDRA	7.37850000	7.0	22.0	42.4	-29.23388900	-29.0	14.0	2.0	2 4	CHA
343	9897		7.39258330	7.0	23.0	33.3	27.86916600	27.0	9.0	3.87	40 1	6EM
344	9909		7.40130550	7.0	24.0	4.7	49.28305500	49.0	16.0	4.45	21	LYN
345	9947	GOMEISA	7.42088880	7.0	25.0	15.2	8.36111110	8.0	21.0	3.09	3 8	CHA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

346	9974	7.43743080	7.0	26.0	15.5	8.99777770	8.0	59.0	52.0	4.6U	4 6	CHI
347	9987	7.44772210	7.0	26.0	51.8	31.85555500	31.0	51.0	20.0	4.1B	62 R	SEM
348	10040	7.46866660	7.0	28.0	7.2	-43.22972100	-43.0	13.0	47.0	3.27	0 3	PUP
349	10120	7.53947210	7.0	32.0	22.1	31.96638800	31.0	57.0	59.0	1.58	66 A	SEM
350	10134	7.54255550	7.0	32.0	33.2	-22.21944400	-22.0	13.0	10.0	4.52	108 U	PUP
351	10167	7.56200550	7.0	33.0	46.1	26.97500000	26.0	58.0	30.0	4.22	69 U	PUP
352	10178	7.56624990	7.0	33.0	58.5	-28.29111100	-28.0	17.0	28.0	4.55	0	PUP
353	10246	7.60119440	7.0	36.0	4.3	-34.88888800	-34.0	53.0	20.0	4.62	0	PUP
354	10264	7.61405550	7.0	36.0	50.6	-25.28444400	-25.0	4.0	4.0	4.64	0	PUP
355	10281	7.62311100	7.0	37.0	23.2	-26.72111100	-26.0	43.0	16.0	4.50	0 K	PUP
356	10277	7.62499990	7.0	37.0	28.2	5.31583330	5.0	18.0	57.0	4.8	10 A	CHI
357	10345	7.65958320	7.0	39.0	34.5	-9.46833300	-9.0	28.0	6.0	4.07	26 A	MON
358	10373	7.68544440	7.0	41.0	7.6	28.96972100	28.0	59.0	11.0	4.26	75 B	SEM
359	10444	7.70438890	7.0	42.0	15.8	-22.52249900	-22.0	31.0	21.0	3.89	0 3	VOL
360	10403	7.70561110	7.0	42.0	20.2	24.48333300	24.0	29.0	.0	3.68	77 K	SEM
361	10417	7.70649450	7.0	42.0	24.1	-28.87027700	-28.0	52.0	13.0	4.10	3	PUP
362	10438	7.71961110	7.0	43.0	10.4	28.11222200	28.0	6.0	44.0	1.21	78 B	SEM
363	10442	7.73344440	7.0	44.0	14	-37.88277700	-37.0	54.0	58.0	3.72	0	PUP
364	10532	7.77716660	7.0	46.0	37.8	-25.84916700	-25.0	50.0	5.0	4.59	0 0	PUP
365	10553	7.78824990	7.0	47.0	17.7	-46.98661000	-46.0	59.0	19.0	4.64	0	PUP
366	10542	7.79702770	7.0	47.0	49.3	-24.77083300	-24.0	46.0	15.0	3.47	7 C	PUP
367	10576	7.80286100	7.0	48.0	10.3	-46.28444400	-46.0	17.0	4.0	4.25	0	PUP
368	10655	7.85022210	7.0	51.0	4.8	-40.48472200	-40.0	29.0	5.0	3.76	0 A	PUP
369	10661	7.85475000	7.0	51.0	24.3	-38.77138800	-38.0	46.0	17.0	4.53	0	PUP
370	10689	7.87122210	7.0	52.0	16.4	-48.01111100	-48.0	40.0	40.0	4.32	0	PUP
371	10756	7.92355550	7.0	55.0	21.2	-22.78555500	-22.0	47.0	4.0	4.35	11	PUP
372	10770	7.93147220	7.0	55.0	53.3	-52.88777700	-52.0	53.0	16.0	3.60	0 X	CAR
373	10802	7.95388880	7.0	57.0	14.0	-49.14916600	-49.0	8.0	57.0	4.00V	0	PUP
374	10825	7.97163890	7.0	58.0	17.9	-18.30222200	-18.0	18.0	8.0	4.64	232	PUP
375	10891	8.00741670	8.0	2.0	26.7	2.43194440	2.0	25.0	55.0	4.52	0	CHI
376	10947	8.03922210	8.0	6.0	3.2	-39.90361000	-39.0	54.0	13.0	2.27	0 2	PUP
377	11034	8.10088870	8.0	6.0	50.1	-24.20250000	-24.0	12.0	9.0	2.88	15 R	PUP
378	11051	8.11391650	8.0	6.0	27.8	-2.88055550	-2.0	52.0	50.0	4.41	29 2	MON
379	11071	8.12438870	8.0	7.0	49.5	-19.14138800	-19.0	8.0	29.0	4.34	16	PUP
380	11098	8.13041650	8.0	7.0	27.2	-68.51465000	-68.0	30.0	51.0	4.46	0 E	VOL
381	11105	8.16049990	8.0	9.0	37.8	-47.23277800	-47.0	13.0	58.0	1.90	0 6	VEL
382	11134	8.21341660	8.0	12.0	48.3	-12.82194440	-12.0	49.0	19.0	4.88	19	PUP
383	11149	8.24363880	8.0	14.0	6.4	-39.51333300	-39.0	30.0	48.0	4.43	0	PUP
384	11215	8.28741660	8.0	17.0	14.7	-40.24037700	-40.0	14.0	25.0	4.43	0	PUP
385	11254	8.34077770	8.0	20.0	24.8	9.29472220	9.0	17.0	41.0	3.76	17 B	CNC
386	11343	8.36211100	8.0	21.0	43.4	-36.55000000	-36.0	33.0	.0	4.43	0	PUP
387	11419	8.34077770	8.0	19.0	27.4	-76.80972100	-76.0	48.0	35.0	4.08	0 A	CMA
388	11401	8.34211100	8.0	20.0	24.8	43.30194400	43.0	18.0	7.0	4.43	31	LYN
389	11481	8.36211100	8.0	21.0	43.4	-77.37222200	-77.0	22.0	20.0	4.26	0 J	CHA
390	11463	8.36277770	8.0	21.0	47.8	-59.39638800	-59.0	23.0	47.0	1.74	0 E	CAR
391	11499	8.39852770	8.0	23.0	51.7	-3.79111100	-3.0	47.0	28.0	3.95	30	MON
392	11547	8.42272210	8.0	25.0	24.7	-66.01972100	-66.0	1.0	11.0	3.45	0 8	VOL
393	11593	8.45614330	8.0	27.0	22.3	60.83694400	60.0	50.0	13.0	3.47	1 0	UMA
394	11823	8.59674990	8.0	35.0	48.3	5.82644440	5.0	49.0	37.0	4.18	4 0	HVA
395	11852	8.60686100	8.0	38.0	24.7	-42.88611100	-42.0	51.0	58.0	4.13	0	VEL
396	11856	8.61547210	8.0	38.0	55.7	3.46527780	3.0	27.0	55.0	4.54	5 8	HVA
397	11923	8.64552770	8.0	39.0	43.9	-35.18305500	-35.0	10.0	59.0	4.04	0 8	PVX
398	11943	8.65483320	8.0	39.0	17.4	-52.79222000	-52.0	47.0	50.0	3.68	0 0	VEL
399	11951	8.65722100	8.0	39.0	27.8	-48.52361100	-48.0	31.0	25.0	4.06	53	VEL
400	11964	8.66408330	8.0	39.0	50.7	-59.63583300	-59.0	38.0	9.0	4.42	0	CAR
401	11982	8.68722100	8.0	41.0	15.8	-59.63583300	-59.0	38.0	44.0	4.73	43 0	CNC
402	11987	8.68944440	8.0	41.0	23.4	21.59555600	21.0	35.0	44.0	4.32	7 M	HVA
403	12006	8.69924980	8.0	41.0	57.3	3.52527770	3.0	31.0	31.0	4.70	31	MON
						-7.10666660	-7.0	6.0	24.0	4.70		

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

404	12018		8.70308320	8.0	42.0	11.1	-33.05944400	-33.0	3.0	34.0	3.70	0 A	PYA
405	12022	ASELLUS-AUSTR.	8.71143800	8.0	42.0	41.9	18.28416600	18.0	17.0	3.0	4.17	47 D	CNC
406	12050		8.71913870	8.0	43.0	8.9	-42.52146600	-42.0	31.0	18.0	4.12	0	VEL
407	12049		8.72694430	8.0	43.0	44.2	-54.57972100	-54.0	34.0	47.0	2.01	0 0	VEL
408	12083		8.74305540	8.0	44.0	35.0	28.88916700	28.0	53.0	21.0	4.20	48 I	CNC
409	12097		8.74526100	8.0	44.0	43.3	-13.91888870	-13.0	25.0	8.0	4.44	12	HYA
410	12109		8.74733320	8.0	44.0	50.4	-45.91277700	-45.0	32.0	46.0	4.09	0	VEL
411	12102		8.74872210	8.0	44.0	55.4	6.54833300	6.0	54.0	54.0	3.48	11 E	HYA
412	12138		8.75341640	8.0	45.0	48.3	-56.64055500	-56.0	38.0	26.0	4.43	0	CAR
413	12118		8.77633330	8.0	46.0	34.8	5.98472220	5.0	58.0	65.0	4.42	13 E	HYA
414	12216		8.81744440	8.0	46.0	2.8	-27.57916600	-27.0	34.0	45.0	4.19	0 6	PYA
415	12327		8.89241640	8.0	53.0	32.7	6.07972220	6.0	4.0	37.0	3.30	16 Z	HYA
416	12359		8.9042770	8.0	54.0	15.4	-60.51027800	-60.0	30.0	39.0	3.99	0	CAR
417	12406	ACUBENS	8.94291650	8.0	56.0	34.5	11.99416670	11.0	59.0	39.0	4.27	65 A	CNC
418	12407	TALITHA	8.94699990	8.0	56.0	49.2	48.18027700	48.0	10.0	49.0	3.12	9 I	UMA
419	12434		8.97291650	8.0	58.0	22.5	41.92249900	41.0	55.0	21.0	4.09	10	UMA
420	12451		8.97969420	8.0	58.0	46.9	-41.11666600	-41.0	7.0	.0	4.42	91	VEL
421	12503		9.02074990	9.0	1.0	14.7	47.29611100	47.0	17.0	46.0	3.68	12 K	UMA
422	12532		9.03163890	9.0	1.0	53.9	-66.25611000	-66.0	15.0	22.0	4.18	0 A	VOL
423	12545		9.04908320	9.0	2.0	56.7	-46.95777700	-46.0	57.0	28.0	3.69	0	VEL
424	12565		9.07180550	9.0	4.0	18.5	38.59333300	38.0	35.0	36.0	4.71	0	CAR
425	12595		9.08452740	9.0	5.0	4.3	-72.46194300	-72.0	27.0	43.0	4.50	0	CAR
426	12604		9.10688880	9.0	6.0	24.8	51.7422100	51.0	49.0	50.0	4.54	15	UMA
427	12823	SUHAII	9.1117770	9.0	6.0	42.4	-43.29055500	-43.0	17.0	26.0	2.22	0 L	VEL
428	12896	ALSUMAIL	9.1342220	9.0	8.0	3.2	63.65749900	63.0	39.0	27.0	4.74	14 T	UMA
429	12896		9.16741640	9.0	10.0	2.7	-58.62305500	-58.0	47.0	23.0	3.54	0	CAR
430	12707		9.17474990	9.0	10.0	29.1	-62.17305500	-62.0	10.0	23.0	4.18	0	CAR
431	12743		9.20908320	9.0	12.0	32.7	2.4627770	2.0	27.0	46.0	3.84	22 J	HYA
432	12764	MIAPLACIDUS	9.21374990	9.0	12.0	49.5	-69.57305500	-69.0	34.0	23.0	1.80	0 8	CAR
433	12787		9.23916650	9.0	14.0	21.0	-37.26666600	-37.0	16.0	4.0	4.70	0	VEL
434	12813		9.2530320	9.0	15.0	12.9	-57.39449300	-57.0	23.0	40.0	4.18	0	CAR
435	12831	TUREIS	9.2692220	9.0	16.0	9.2	-59.12805500	-59.0	7.0	41.0	2.25	0 1	CAR
436	12830		9.27786100	9.0	16.0	40.3	36.95194400	36.0	57.0	7.0	3.82	38	LYN
437	12880		9.31547220	9.0	18.0	55.7	34.54166700	34.0	32.0	30.0	3.30	40 A	LYN
438	12938		9.35047210	9.0	21.0	1.7	-54.86083300	-54.0	51.0	39.0	2.63	0 K	VEL
439	12972		9.37699990	9.0	22.0	37.2	26.33388900	26.0	20.0	2.0	4.61	1 K	LEO
440	13044	ALPHARD COR-HYORAE	9.43111100	9.0	25.0	52.0	-8.50611110	-8.0	30.0	22.0	2.16	30 A	HYA
441	13091		9.46330550	9.0	27.0	47.9	-35.79777700	-35.0	47.0	52.0	4.64	0 E	ANT
442	13109		9.4796320	9.0	28.0	47.4	63.21611000	63.0	12.0	58.0	3.75	23	UMA
443	13140		9.48866660	9.0	29.0	19.2	-40.31277700	-40.0	18.0	46.0	3.64	0 Y	VEL
444	13143		9.49544430	9.0	29.0	43.6	23.12333300	23.0	7.0	24.0	4.48	4 L	LEO
445	13160		9.50261090	9.0	30.0	9.4	-56.87944400	-56.0	52.0	46.0	3.00	0	VEL
446	13153		9.50330550	9.0	30.0	11.9	-1.0297221	-1.0	1.0	47.0	4.50	32 T	HYA
447	13157		9.5087740	9.0	31.0	31.6	51.83777700	51.0	50.0	16.0	3.26	25 J	UMA
448	13192		9.52274990	9.0	31.0	21.9	-62.6361100	-62.0	38.0	1.0	4.00	0	CAR
449	13171		9.52366670	9.0	31.0	25.2	69.98585900	69.0	59.0	8.0	4.57	24	UMA
450	13203		9.53749990	9.0	32.0	5.1	36.55388900	36.0	33.0	14.0	4.62	10	LMI
451	13174		9.53741640	9.0	32.0	14.7	81.4833200	81.0	29.0	.0	4.58	1	DRA
452	13212		9.5404110	9.0	32.0	24.2	52.20805500	52.0	12.0	29.0	4.65	26	UMA
453	13246		9.55713880	9.0	33.0	25.7	-59.07305500	-59.0	4.0	23.0	4.20	0	CAR
454	13293		9.59288870	9.0	35.0	34.4	-49.19777700	-49.0	11.0	52.0	4.49	0	VEL
455	13341		9.63447210	9.0	38.0	4.1	-98.305555	-98.0	58.0	59.0	4.10	35 I	HYA
456	13355		9.63966640	9.0	38.0	23.8	-61.16916600	-61.0	10.0	9.0	4.67	0	CAR
457	13366	SUBRA	9.65472210	9.0	39.0	17.0	10.0522220	10.0	3.0	8.0	3.74	14 0	LEO
458	13373		9.66141660	9.0	39.0	41.1	-23.93166600	-23.0	25.0	54.0	4.74	0	HYA
459	13443	RAS-ELASED AUSTR.	9.73113870	9.0	43.0	52.1	23.93611100	23.0	56.0	10.0	3.12	17 E	LEO
460	13462		9.7380310	9.0	44.0	17.1	-62.34583300	-62.0	20.0	45.0	4.00	0	CAR
461	13504		9.77047220	9.0	46.0	13.7	-64.90916600	-64.0	33.0	3.08	3.08	0 U	CAR

HYA ALFARU

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

462	13540	9.80861110	9.0	48.0	31.0	59.20444400	59.0	12.0	14.0	3.89	29 U	UMA
463	13559	9.82894440	9.0	49.0	44.2	54.22800000	54.0	13.0	14.0	4.54	30 V	UMA
464	13570	9.82988890	9.0	49.0	47.6	14.68166660	-14.0	40.0	54.0	4.29	39 U	MYA
465	13587	9.83872210	9.0	50.0	19.4	-46.38305500	-46.0	22.0	59.0	4.56	0	VEL
466	13590	9.84627760	9.0	50.0	46.6	26.17289900	26.0	19.0	21.0	4.10	24 M	VEL
467	13711	9.8271430	8.0	55.0	37.9	54.40055500	54.0	2.0	3.70	2.0	0 V	VEL
468	13861	10.05692210	10.0	3.0	26.1	-12.89444430	-12.0	53.0	40.0	4.72	40 U	MYA
469	13876	10.08949980	10.0	5.0	22.2	35.41611100	35.0	24.0	58.0	4.47	21	LMY
470	13899	10.09044420	10.0	5.0	25.6	16.93388800	16.0	56.0	2.0	3.58	30 M	LEO
471	13911	10.10080530	10.0	6.0	2.9	10.16972210	10.0	10.0	11.0	4.86	31	LEO
472	13916	10.10244430	10.0	6.0	8.8	-20.000000	0	12.0	0	4.50	15 A	SEX
473	13926	KALB10.10849980	10.0	6.0	30.6	12.13888800	12.0	8.0	20.0	1.34	32 A	LEO
474	13982	10.14799980	10.0	8.0	52.8	-12.18055550	-12.0	10.0	50.0	3.83	41 L	MYA
475	14074	10.21516650	10.0	12.0	54.6	-69.86388900	-69.0	51.0	50.0	3.56	0 W	CAR
476	14076	10.22105530	10.0	13.0	15.8	-41.94833300	-41.0	56.0	54.0	4.09	0	VEL
477	14107	ADMAFERA	10.0	14.0	44.8	23.59222200	23.0	35.0	32.0	3.65	36 Z	LEO
478	14113	TANIA BOR.	10.0	14.0	54.6	43.08972200	43.0	5.0	22.0	3.52	33 L	UMA
479	14133	10.26519130	10.0	15.0	54.7	-61.15694400	-61.0	9.0	25.0	3.44	187	CAR
480	14177	ALGIEBA	10.0	18.0	2.7	20.01916600	20.0	1.0	9.0	2.61	41 8	LEO
481	14195	10.30491650	10.0	18.0	17.7	-54.85333300	-54.0	51.0	18.0	4.58	0	VEL
482	14220	10.32677770	10.0	19.0	36.4	-55.86638800	-55.0	51.0	59.0	4.65	0	VEL
483	14232	TANIA AUSTR.	10.0	20.0	18.0	41.67611100	41.0	40.0	34.0	3.21	34 M	UMA
484	14323	10.39511100	10.0	23.0	42.4	-73.85333300	-73.0	51.0	12.0	4.08	0	CAR
485	14326	10.40661110	10.0	24.0	23.8	-16.65694400	-16.0	37.0	28.0	4.04	42 M	MYA
486	14352	10.42580540	10.0	25.0	32.9	-30.88916600	-30.0	53.0	21.0	4.42	0 A	ANT
487	14358	10.43108310	10.0	25.0	51.9	36.88722200	36.0	53.0	14.0	4.41	31 8	LMY
488	14388	10.44316650	10.0	26.0	35.4	-58.56027700	-58.0	37.0	37.0	4.08	0	CAR
489	14489	10.51291640	10.0	30.0	48.6	-61.50500000	-61.0	30.0	18.0	3.58	0	CAR
490	14497	10.51616640	10.0	30.0	58.2	9.48722220	9.0	27.0	14.0	3.85	47 R	LEO
491	14570	10.57063880	10.0	34.0	44.3	-57.37611100	-57.0	22.0	34.0	4.54	0	CAR
492	14604	10.58452740	10.0	35.0	41.3	-78.42611000	-78.0	25.0	34.0	4.10	0 8	CMA
493	14614	10.59711100	10.0	35.0	49.6	-48.04361100	-48.0	2.0	37.0	4.06	0	VEL
494	14647	10.62358320	10.0	37.0	24.9	-59.00855500	-59.0	25.0	15.0	4.73	0	CAR
495	14662	10.62183320	10.0	37.0	54.6	-25.42083300	-25.0	25.0	3.00	4.25	0	VEL
496	14755	10.69505540	10.0	41.0	42.2	-64.21083300	-64.0	22.0	3.00	3.03	0 J	CAR
497	14762	10.70333330	10.0	42.0	12.0	-60.38277700	-60.0	22.0	5.00	4.49	0	CAR
498	14822	10.75430540	10.0	45.0	15.5	-49.23472200	-49.0	14.0	5.0	2.84	0 M	VEL
499	14863	10.75799970	10.0	45.0	28.8	-80.35555600	-80.0	21.0	20.0	9.62	0 D	CHA
500	14898	10.79827770	10.0	47.0	53.8	-16.01000000	-16.0	0	36.0	3.32	0 M	MYA
501	14941	10.85599990	10.0	51.0	21.6	34.40388900	34.0	24.0	14.0	3.92	46 0	LMY
502	14980	10.86774980	10.0	52.0	3.9	-58.66722200	-58.0	40.0	2.0	3.88	0	CAR
503	15016	10.89536100	10.0	53.0	43.3	24.93666600	24.0	5.0	12.0	4.51	54	LEO
504	15047	10.91819440	10.0	55.0	5.4	-36.94944400	-36.0	5.0	58.0	4.70	0 I	ANT
505	15106	ALKE	10.0	58.0	4.4	-18.11194400	-18.0	4.0	43.0	4.20	7 A	CRT
506	15118	10.97572210	10.0	58.0	32.6	-42.03777700	-42.0	2.0	16.0	4.56	239	VEL
507	15145	MERAK	10.0	59.0	44.5	54.57027700	54.0	34.0	13.0	2.44	48 B	UMA
508	15162	11.00722220	11.0	0	27.8	20.36777700	20.0	22.0	4.0	4.42	60	LEO
509	15185	DUBHE	11.0	1.0	35.0	61.94027700	61.0	56.0	25.0	1.95	50 A	UMA
510	15235	11.02638870	11.0	3.0	12.7	7.52555550	7.0	31.0	32.0	4.66	63 A	LEO
511	15329	11.01813870	11.0	7.0	5.3	-58.78527700	-58.0	47.0	7.0	4.02	260	CAR
512	15340	11.12838800	11.0	7.0	42.2	44.68861100	44.0	41.0	19.0	3.15	0 Y	UMA
513	15385	11.16555540	11.0	9.0	56.0	-22.63444400	-22.0	38.0	4.0	4.52	11 B	CRT
514	15415	11.18486090	11.0	11.0	5.5	-60.12644400	-60.0	7.0	37.0	4.73	0	CAR
515	15438	ZOSMA	11.0	12.0	15.0	20.71555500	20.0	42.0	56.0	2.58	68 0	LEO
516	15441	CORA	11.0	14.0	24.3	15.62111110	15.0	27.0	14.0	3.41	70 J	LEO
517	15511	11.24602750	11.0	14.0	52.9	-73.45999990	-73.0	37.0	36.0	4.58	74 Y	LEO
518	15537	ALULA-AUSTR.	11.0	16.0	19.2	31.72638900	31.0	43.0	35.0	3.88	53 C	UMA
519	15547	ALULA-BOR.	11.0	16.0	35.5	33.28555500	33.0	17.0	8.0	3.71	54 M	UMA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

520	15567	11-23133870	11-0	17-0	35-3	-14-58888890	-14-0	35-0	20-0	3-84	12 0	CRT
521	15600	11-32219430	11-0	19-0	19-9	6-22138890	6-0	17-0	17-0	4-13	77 5	LEO
522	15601	11-32338880	11-0	19-0	24-2	-54-29916600	-54-0	17-0	5-0	4-26	0 9	CEN
523	15652	11-36836100	11-0	22-0	6-1	10-72222220	10-0	23-0	20-0	4-03	78 1	LEO
524	15669	11-38550000	11-0	23-0	7-8	-17-49166600	-17-0	23-0	20-0	4-14	15 6	CRT
525	15799	11-48911090	11-0	29-0	20-8	69-52444300	69-0	31-0	28-0	4-06	1 1	ORA
526	15845	11-52127770	11-0	31-0	16-4	-21-66388900	-31-0	39-0	50-0	3-72	0 1	MYA
527	15899	11-56930540	11-0	34-0	9-5	-62-82611000	-62-0	49-0	34-0	3-34	0 1	CEN
528	15927	11-58594830	11-0	35-0	9-4	-4-30555555	0	37-0	50-0	4-47	92 0	LEO
529	16131	11-73238870	11-0	43-0	56-6	-66-53472100	-66-0	32-0	5-0	3-80	0 1	MUS
530	16135	11-73433320	11-0	44-0	3-6	6-72555550	6-0	43-0	32-0	4-20	3 0	VIR
531	16137	11-73600540	11-0	44-0	12-5	47-97333300	47-0	50-0	24-0	3-85	63 1	MYA
532	16147	11-74683320	11-0	44-0	48-6	-40-98388800	-60-0	59-0	2-0	4-22	65	CEN
533	16173	11-76969440	11-0	46-0	10-9	20-41333300	20-0	24-0	48-0	4-54	93	LEO
534	16176	11-77574990	11-0	49-0	32-7	-66-62027700	-66-0	37-0	13-0	4-71	0 0	MUS
535	16189	11-78791660	11-0	47-0	18-5	14-76777760	14-0	46-0	4-0	2-23	94 8	LEO
536	16201	11-79949980	11-0	47-0	58-2	-63-59388800	-63-0	35-0	38-0	4-52	0	CEN
537	16215	11-81452770	11-0	48-0	52-3	1-96194443	1-0	57-0	43-0	3-80	5 8	VIR
538	16236	11-82311090	11-0	49-0	23-2	-44-97861000	-44-0	58-0	43-0	4-71	0 0	CEN
539	16258	11-82524980	11-0	51-0	8-1	-33-71333300	-33-0	42-0	46-0	4-40	0 0	MYA
540	16268	PHECDA11-86661090	11-0	51-0	59-8	53-88916600	53-0	53-0	21-0	2-54	64 6	MYA
541	16425	11-98463870	12-0	5-0	13-9	6-80944440	6-0	48-0	34-0	4-57	8 9	VIR
542	16463	12-0202770	12-0	1-0	10-7	-63-11805500	-63-0	7-0	5-0	4-48	0 1	CRU
543	16512	12-05711100	12-0	3-0	25-6	8-92722210	8-0	55-0	38-0	4-24	9 0	VIR
544	16551	12-08402770	12-0	5-0	2-8	-64-41861000	-64-0	25-0	7-0	4-30	0 0	CRU
545	16594	12-10891650	12-0	6-0	32-1	-50-52777800	-50-0	31-0	40-0	2-88	0 0	CEN
546	16596	12-11005540	12-0	6-0	36-2	-24-23388900	-24-0	33-0	2-0	4-18	1 1	CRV
547	16618	12-13849440	12-0	8-0	19-3	-22-42527800	-22-0	25-0	31-0	3-21	2 2	CRV
548	16651	12-16355550	12-0	9-0	40-6	-52-17388900	-52-0	10-0	26-0	4-20	0 0	CEN
549	16724	12-22124980	12-0	13-0	18-5	-58-55444400	-58-0	33-0	16-0	3-06	0 0	CRU
550	16736	KAFFA12-22361110	12-0	1-0	42-1	57-22649400	57-0	13-0	37-0	3-44	69 0	MYA
551	16740	12-23338870	12-0	19-0	27-5	-17-34777700	-17-0	20-0	52-0	2-78	4 8	CRV
552	16764	12-26105540	12-0	15-0	37-8	-67-76611000	-67-0	48-0	48-0	4-16	0 8	MUS
553	16775	12-27094440	12-0	16-0	15-4	-79-11805500	-79-0	7-0	5-0	4-38	0 0	MYA
554	16785	12-27541660	12-0	16-0	31-5	-63-80888900	-63-0	48-0	32-0	4-26	0 2	CRU
555	16813	12-30188880	12-0	18-0	6-8	-4-72500000	-4-0	28-0	21-0	4-00	18 0	VIR
556	16849	12-32430550	12-0	19-0	27-5	-60-20805500	-60-0	12-0	29-0	3-57	0 8	CRU
557	16953	12-41061110	12-0	21-0	38-2	-62-90527700	-62-0	54-0	19-0	1-00	0 1	CRU
558	16964	12-41991650	12-0	25-0	11-7	28-46277700	28-0	27-0	44-0	4-56	15 6	COM
559	16990	12-43563080	12-0	26-0	8-3	-50-03722200	-50-0	2-0	14-0	4-16	0 3	CEN
560	17029	12-46749980	12-0	28-0	3-0	-16-32083300	-16-0	19-0	15-0	3-11	7 0	CRV
561	17052	12-48686110	12-0	29-0	12-7	-56-91749900	-56-0	58-0	3-0	1-61	0 6	CRU
562	17087	12-50438870	12-0	30-0	15-8	-16-00249900	-16-0	0	9-0	4-42	8 0	CRV
563	17084	12-50588640	12-0	30-0	21-2	-71-94000000	-71-0	56-0	24-0	4-04	0 6	MUS
564	17124	12-53330560	12-0	31-0	59-9	49-98083300	49-0	58-0	51-0	3-88	5 1	ORA
565	17147	12-53472210	12-0	34-0	5-0	41-54722200	41-0	32-0	50-0	4-32	8 0	CEN
566	17139	12-54241660	12-0	32-0	32-7	-23-20333300	-23-0	12-0	12-0	2-64	9 8	CRV
567	17179	12-58461090	12-0	35-0	4-6	-68-94305500	-68-0	56-0	35-0	2-94	0 1	MUS
568	17194	12-59630530	12-0	35-0	40-7	-48-34888900	-48-0	20-0	56-0	4-02	0 1	CEN
569	17242	12-59641100	12-0	39-0	34-6	-48-76777700	-48-0	46-0	4-0	2-38	0 5	CEN
570	17280	PORRIMA12-68474990	12-0	38-0	53-1	-11-25777777	-11-0	15-0	28-0	2-91	29 8	VIR
571	17282	12-67738880	12-0	40-0	38-6	-48-62111100	-48-0	37-0	16-0	4-68	0	CEN
572	17339	12-72597210	12-0	43-0	33-5	-60-78944400	-60-0	47-0	22-0	4-65	0 1	CRU
573	17348	12-73524980	12-0	44-0	6-9	-67-91694300	-67-0	55-0	1-0	3-26	0 8	MUS
574	17374	12-76102750	12-0	45-0	39-7	-59-49777700	-59-0	29-0	52-0	1-50	0 8	CRU
575	17473	12-85205540	12-0	51-0	7-4	-48-75305400	-48-0	46-0	11-0	4-35	0	CEN
576	17499	12-85816640	12-0	51-0	29-4	-39-98888900	-39-0	59-0	20-0	4-34	0	CEN
577	17518	12-87491650	12-0	52-0	20-7	-56-14944400	-56-0	8-0	58-0	1-68	77 8	MYA

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

576	17512		12-07530870	12-0	52-0	31-4	-56-98033300	-56-0	59-0	18-0	4-26	O M	CRU
577	17543	AUVA	12-0730550	12-0	53-0	50-3	3-58722220	3-0	35-0	14-0	3-66	43 D	VIR
578	17557	CHARA	12-9065540	12-0	54-0	23-4	38-50694000	30-0	30-0	25-0	2-90	12 A	CYN
581	17672		12-9972490	12-0	59-0	50-1	-71-36083300	-71-0	39-0	39-0	3-63	0 D	MUS
582	17687	VINDIEMATRIX	13-00722210	13-0	0	26-0	11-1489450	11-0	8-0	49-0	2-95	47 E	VIR
583	17773		13-08094430	13-0	4-0	51-4	-49-71916000	-49-0	43-0	9-0	4-90	0 C	CEM
584	17828		13-1358330	13-0	8-0	8-1	-5-35249990	-5-0	21-0	9-0	4-44	51 J	VR
585	17833	DIADEM	13-1380320	13-0	8-0	17-1	17-71380900	17-0	42-0	50-0	4-50	42 A	CDR
586	17874		13-17066950	13-0	10-0	14-4	28-05500000	28-0	3-0	18-0	4-32	43 B	COM
587	18000		13-26624970	13-0	15-0	58-5	40-75328000	40-0	45-0	23-0	4-66	20	CYN
588	18012		13-28355550	13-0	17-0	8	-22-98750000	-22-0	59-0	15-0	3-33	46 6	MVA
589	18039		13-3103880	13-0	18-0	37-4	-38-52833300	-38-0	31-0	42-0	2-91	0 I	CEM
590	18087		13-3392210	13-0	20-0	21-2	-60-80555000	-60-0	48-0	20-0	4-62	0	CEM
591	18107		13-36041090	13-0	21-0	30-2	-64-35333200	-64-0	21-0	12-0	4-50	0	CEM
592	18133	MIZAM	13-37533320	13-0	22-0	31-2	55-10749900	55-0	6-0	27-0	1-21	79 Z	UMA
593	18144	SPLICA	13-38908330	13-0	23-0	20-7	-10-9716600	-10-0	58-0	45-0	4-02	67 A	VIR
594	18155	ALCOR	13-3971100	13-0	23-0	49-6	55-17000000	55-0	10-0	12-0	4-02	80	UMA
595	18239		13-46325000	13-0	27-0	47-7	-39-22722200	-39-0	6-0	4-0	3-00V	0	MVA
596	18254		13-48344430	13-0	29-0	4-4	-9-4777777	-9-0	13-0	38-0	3-96	0	CEM
597	18351	HEZE	13-5484440	13-0	32-0	54-4	49-19416600	49-0	4-0	4-0	3-44	79 Z	CYN
598	18356		13-5504440	13-0	33-0	1-6	-53-28916600	-53-0	11-0	39-0	4-63	24	CYN
599	18450		13-62761100	13-0	37-0	39-4	54-85833300	54-0	17-0	21-0	2-56	0 E	CEM
600	18504		13-6584100	13-0	39-0	24-7	-32-86749000	-32-0	51-0	30-0	4-75	83	UMA
601	18593		13-7281940	13-0	43-0	41-5	-51-25805500	-51-0	52-0	3-0	4-26	1	CEM
602	18607		13-74047200	13-0	44-0	25-7	17-63027800	17-0	37-0	49-0	4-51	0	CEM
603	18637		13-75997220	13-0	45-0	35-9	49-48749900	49-0	29-0	15-0	1-91	85 M	UMA
604	18643	ALKAID	13-7693880	13-0	46-0	9-8	-41-51416600	-41-0	30-0	51-0	3-53	0 M	CEM
605	18665	BENETNASH	13-7899440	13-0	47-0	23-8	-34-27646600	-34-0	16-0	36-0	4-40	2	CEM
606	18666		13-79016670	13-0	47-0	24-6	-42-29899000	-42-0	18-0	18-0	3-32	0 M	CEM
607	18667		13-79163890	13-0	47-0	29-9	15-97083300	15-0	58-0	15-0	4-28	5 U	BOO
608	18674		13-79647210	13-0	47-0	47-3	-32-82138900	-32-0	49-0	17-0	4-72	3	CEM
609	18724		13-8297210	13-0	49-0	47-9	18-57250000	18-0	39-0	21-0	2-80	8 M	BOO
610	18805	MUFRID	13-8836110	13-0	53-0	1-0	-47-11694000	-47-0	7-0	1-0	3-06	0 X	CEM
611	18809		13-88908330	13-0	53-0	20-7	-63-5161100	-63-0	30-0	58-0	4-68	294	CEM
612	18845		13-91824990	13-0	55-0	5-7	-41-93055500	-41-0	55-0	50-0	4-05	0 Y	CEM
613	18874		13-9355550	13-0	56-0	8-0	-44-63361100	-44-0	38-0	1-0	4-17	0 U	CEM
614	18883		13-9417740	13-0	56-0	30-4	-45-43472200	-45-0	26-0	5-0	4-39	0 U	CEM
615	18939		13-99216650	13-0	59-0	31-8	1-71305555	1-0	42-0	47-0	4-34	93 Y	VIR
616	18945		13-99722200	13-0	59-0	51-8	-60-20537700	-60-0	12-0	19-0	8-6	0 8	CEM
617	18971		14-02227770	14-0	1-0	20-2	64-54249900	64-0	32-0	33-0	3-64	11 A	DRA
618	19019	THUBAN	14-05733320	14-0	3-0	26-4	-41-01277700	-41-0	0	46-0	4-54	0 X	CEM
619	19017		14-06500000	14-0	3-0	54-0	-26-51472200	-26-0	30-0	53-0	3-48	49 P	MVA
620	19029		14-07286090	14-0	4-0	22-3	-36-19061100	-36-0	11-0	55-0	2-26	5 J	CEM
621	19033	MENKENT	14-07691660	14-0	4-0	36-9	-10-1166650	-10-0	6-0	42-0	4-31	98 K	VIR
622	19168		14-18374990	14-0	11-0	1-5	51-95305500	51-0	57-0	11-0	4-60	16 A	BOO
623	19207		14-20383320	14-0	12-0	13-8	19-36388800	19-0	21-0	50-0	2-4	16 A	BOO
624	19242	ARCTURUS	14-2343880	14-0	14-0	3-8	-5-83416660	-5-0	50-0	3-0	4-16	99 I	VIR
625	19244		14-23627760	14-0	14-0	10-6	46-24833200	46-0	14-0	54-0	4-26	19 L	BOO
626	19273		14-25088870	14-0	15-0	3-2	-45-89749900	-45-0	53-0	51-0	4-10	0 I	LUP
627	19304		14-28586100	14-0	17-0	9-1	-13-21083340	-13-0	12-0	39-0	4-60	100 L	VIR
628	19311		14-28686110	14-0	17-0	12-7	-56-22638800	-56-0	13-0	35-0	4-41	0 U	CEM
629	19318		14-29774980	14-0	17-0	51-9	-37-72527700	-37-0	43-0	31-0	4-17	0 Y	CEM
630	19337		14-30699990	14-0	18-0	25-2	-39-35305600	-39-0	21-0	11-0	4-55	0	CEM
631	19377		14-3786100	14-0	20-0	52-3	-83-50999000	-83-0	30-0	36-0	4-14	0 7	LUP
632	19399		14-3514650	14-0	21-0	5-1	-45-08416600	-45-0	3-0	51-0	4-65	0 7	LUP
633	19453		14-39799990	14-0	23-0	52-8	-45-2222100	-45-0	1-0	20-0	4-49	0 Y	LUP
634	19454		14-39863890	14-0	23-0	55-1	52-01194400	52-0	1-0	43-0	4-06	23 J	BOO
635	19467		14-40088330	14-0	24-0	0-3							

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

636	19548	14.45961090	14.0	27.0	34.4	75.05130900	75.0	51.0	4.37	5	UMI
637	19549	14.50408310	14.0	30.0	14.7	-50.30305500	-50.0	11.0	4.60	0	LUP
638	19577	14.50536100	14.0	30.0	19.3	30.52416800	30.0	31.0	3.78	25	R
639	19607	14.51113060	14.0	30.0	40.1	38.46055500	38.0	27.0	3.00	28	R
640	19459	14.52538320	14.0	33.0	9.3	29.89630900	29.0	53.0	4.48	28	S
641	19656	14.55458310	14.0	33.0	16.5	-42.00500000	-42.0	1.0	4.65	0	M
642	19678	14.57199990	14.0	38.0	31.2	-49.27444400	-49.0	18.0	4.14	0	R
643	19728	14.62013070	14.0	37.0	12.5	-60.69222200	-60.0	41.0	3.20	0	A
644	19777	14.65791660	14.0	39.0	28.5	13.87750000	13.0	39.0	3.86	30	Z
645	19774	14.65906100	14.0	39.0	35.5	-47.23916800	-47.0	14.0	2.89	0	A
646	19772	14.66091060	14.0	39.0	39.3	-64.82416800	-64.0	49.0	3.41	0	A
647	19779	14.66297210	14.0	39.0	46.7	-37.64444400	-37.0	38.0	4.09	0	A
648	19816	14.68666100	14.0	41.0	12.7	-55.50722200	-55.0	30.0	3.95	107	M
649	19820	14.69180550	14.0	41.0	30.5	-35.02416800	-35.0	1.0	4.13	371	CEM
650	19834	14.72374990	14.0	43.0	25.5	-78.09833300	-78.0	54.0	3.81	0	A
651	19856	14.72430540	14.0	43.0	27.5	27.22083300	27.0	13.0	2.70	36	E
652	19858	14.72677770	14.0	43.0	36.4	17.11138900	17.0	4.0	4.69	35	0
653	19884	14.74127750	14.0	44.0	28.6	2.03916860	2.0	2.0	3.76	109	VIR
654	19954	14.80377760	14.0	48.0	13.6	-27.81583300	-27.0	48.0	4.63	58	MYA
655	19975	14.81563080	14.0	48.0	56.3	-15.89749900	-15.0	53.0	4.90	9	A
656	19977	14.82241660	14.0	49.0	20.7	-43.43166800	-43.0	25.0	4.49	0	LUP
657	19991	14.82952760	14.0	49.0	46.3	19.24527700	19.0	14.0	4.64	37	C
658	20039	14.84644430	14.0	50.0	47.2	74.29861100	74.0	17.0	2.24	7	B
659	20115	14.92252770	14.0	55.0	21.1	-42.20500000	-42.0	12.0	4.59	16	L
660	20128	14.93716640	14.0	56.0	13.8	-42.99444400	-42.0	59.0	2.81	0	LUP
661	20146	14.97791860	14.0	58.0	52.5	-41.98500000	-41.0	57.0	3.35	0	K
662	20226	15.01044440	15.0	60.0	37.6	40.52749900	40.0	31.0	3.63	42	B
663	20237	15.01883330	15.0	61.0	7.8	2.22749990	2.0	13.0	4.62	110	VIR
664	20253	15.03361110	15.0	62.0	1.0	-25.14583300	-25.0	8.0	3.41	20	S
665	20271	15.04541670	15.0	62.0	43.5	-46.91555500	-46.0	54.0	4.02	0	P
666	20285	15.04908320	15.0	62.0	56.7	27.08305500	27.0	4.0	4.67	43	Y
667	20356	15.10791640	15.0	64.0	28.5	-45.14666800	-45.0	48.0	4.39	0	L
668	20409	15.15816660	15.0	64.0	29.4	-48.60638800	-48.0	36.0	4.14	0	K
669	20418	15.16263870	15.0	64.0	45.5	-51.96749900	-51.0	58.0	3.85	0	LUP
670	20433	15.17036110	15.0	64.0	13.3	-19.64055500	-19.0	39.0	4.66	24	I
671	20523	15.23483310	15.0	64.0	54.4	33.44444400	33.0	26.0	3.54	49	D
672	20507	15.24594430	15.0	64.0	45.4	-58.47222200	-58.0	40.0	4.16	0	B
673	20539	15.25199980	15.0	65.0	7.2	-9.25500000	-9.0	18.0	2.74	27	B
674	20538	15.26024980	15.0	65.0	36.9	-68.55222100	-68.0	33.0	3.06	0	G
675	20550	15.26158320	15.0	65.0	41.7	-30.02138900	-30.0	1.0	4.43	2	LUP
676	20556	15.26811090	15.0	66.0	5.2	-47.74777700	-47.0	44.0	4.34	0	M
677	20620	15.31788870	15.0	69.0	4.4	-40.52222100	-40.0	31.0	3.93	0	LUP
678	20643	15.32630530	15.0	69.0	34.7	-36.13583300	-36.0	8.0	3.59	0	Y
679	20659	15.33624980	15.0	70.0	17.7	-44.56499900	-44.0	33.0	3.74	0	LUP
680	20663	15.34288870	15.0	70.0	34.4	-59.19638900	-59.0	11.0	4.54	0	CIR
681	20682	15.34613880	15.0	70.0	46.1	71.95681000	71.0	57.0	3.14	13	G
682	20676	15.34852770	15.0	70.0	54.7	-38.73444400	-38.0	44.0	4.69	0	Y
683	20714	15.38430540	15.0	73.0	3.5	-38.61111000	-38.0	36.0	4.68	0	K
684	20724	15.38611100	15.0	73.0	10.0	37.49888800	37.0	29.0	4.47	51	M
685	20747	15.40222100	15.0	74.0	8.0	59.08805500	59.0	5.0	3.47	12	I
686	20795	15.43974980	15.0	76.0	33.1	29.22527700	29.0	13.0	3.72	3	B
687	20926	15.52527770	15.0	82.0	48.0	-41.05055500	-41.0	28.0	4.17	4	J
688	20926	15.54666670	15.0	82.0	48.0	-41.05055500	-41.0	28.0	2.95	0	G
689	20942	15.55213880	15.0	83.0	7.7	10.65472200	10.0	39.0	4.23	13	D
690	20947	15.55341660	15.0	83.0	12.3	26.83138900	26.0	49.0	2.31	5	A
691	20932	15.55822210	15.0	83.0	29.6	-68.20166500	-68.0	12.0	4.0	0	E
692	20949	15.55941660	15.0	83.0	33.9	-14.67416860	-14.0	40.0	4.02	38	B
693	20977	15.58155550	15.0	84.0	53.6	-28.02055500	-28.0	14.0	3.78	39	U

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

694 21001	15.59480530	15.0	35.0	41.3	-42.45388900	14.0	27.0	14.0	4.27	0 W	LUP
695 21019	15.60833320	15.0	36.0	30.0	-29.66416600	39.0	51.0	3.80	3.80	40 W	L18
696 21042	15.62561090	15.0	37.0	32.2	-34.29888700	17.0	56.0	4.63	4.63	3 V	LUP
697 21070	15.64622210	15.0	38.0	46.4	-44.54694400	32.0	49.0	4.69	4.69	0	LUP
698 21102	15.66647220	15.0	39.0	59.3	19.78194400	46.0	55.0	4.49	4.49	21 I	5ER
699 21130	15.68766100	15.0	41.0	16.3	26.40527700	24.0	19.0	3.93	3.93	8 G	5ER
700 21158	15.70927600	15.0	42.0	32.5	6.53444400	32.0	4.0	2.75	2.75	24 A	5ER
701 21194	15.74283320	15.0	44.0	34.2	15.53000000	18.0	31.0	3.74	3.74	28 B	5ER
702 21201	15.74569430	15.0	44.0	44.5	7.46166600	7.0	27.0	4.42	4.42	27 L	5ER
703 21243	15.75447200	15.0	45.0	14.1	77.90305500	77.0	54.0	4.34	4.34	16 U	5ER
704 21255	15.76605550	15.0	47.0	9.8	18.24833300	18.0	19.0	4.28	4.28	35 K	5ER
705 21269	15.77650000	15.0	47.0	47.4	-3.32444400	-3.0	28.0	3.63	3.63	32 M	5ER
706 21276	15.78028330	15.0	48.0	7.5	26.17416600	26.0	10.0	4.73	4.73	10 D	CRB
707 21281	15.81213880	15.0	48.0	43.7	-33.52222100	-33.0	31.0	4.11	4.11	5 X	LUP
708 21288	15.81780540	15.0	49.0	4.1	4.58166670	4.0	54.0	3.75	3.75	37 E	5ER
709 21340	15.85722200	15.0	51.0	27.8	42.54861000	42.0	32.0	4.61	4.61	1 X	5ER
710 21329	15.85841660	15.0	51.0	30.3	-25.22416600	-25.0	13.0	4.66	4.66	2	SCO
711 21342	15.86380540	15.0	51.0	49.7	16.62805500	16.0	37.0	4.34	4.34	46 J	L18
712 21332	15.86733310	15.0	52.0	2.4	-63.32472100	-63.0	19.0	3.04	3.04	0 B	TRA
713 21398	15.91197220	15.0	54.0	43.1	-29.11333300	-29.0	6.0	4.02	4.02	5 R	SCO
714 21408	15.91391650	15.0	54.0	50.1	15.77444430	15.0	46.0	3.86	3.86	41 E	5ER
715 21440	15.93561100	15.0	56.0	8.2	26.97805500	26.0	58.0	4.22	4.22	13 E	CRB
716 21439	15.93708320	15.0	56.0	13.5	-14.18000000	-14.0	10.0	4.68	4.68	48	L18
717 21447	15.94549980	15.0	56.0	43.8	-26.01472100	-26.0	3.0	3.00	3.00	6 P	SCO
718 21478	15.94325000	15.0	57.0	47.7	-38.29833300	-38.0	17.0	3.84	3.84	0 M	LUP
719 21489	15.97099990	15.0	58.0	15.6	-22.52361100	-22.0	31.0	2.54	2.54	7 D	SCO
720 21539	16.01052700	16.0	1.0	37.9	-49.13388900	-49.0	8.0	2.0	4.74	0 M	NOR
721 21572	16.02050000	16.0	1.0	13.8	58.65805500	58.0	39.0	4.11	4.11	13 J	ORA
722 21580	16.02844400	16.0	1.0	22.4	46.13305500	46.0	7.0	4.64	4.64	6 U	5ER
723 21593	16.04066600	16.0	1.0	42.4	-11.27005560	-11.0	16.0	4.16	4.16	0 C	SCO
724 21609	ELACHAB16.05663800	16.0	3.0	23.9	-19.71111100	-19.0	42.0	2.90	2.90	8 M	LUP
725 21625	16.07147200	16.0	4.0	17.3	-36.70811100	-36.0	42.0	31.0	4.33	0 J	LUP
726 21639	16.07924900	16.0	4.0	45.3	-20.57583300	-20.0	34.0	4.13	4.13	9 W	SCO
727 21659	16.08913800	16.0	5.0	20.9	-20.77585500	-20.0	46.0	4.58	4.58	10 B	SCO
728 21736	16.11275000	16.0	7.0	39.9	45.02555500	45.0	1.0	32.0	4.26	11 V	5ER
729 21773	16.16593300	16.0	9.0	57.4	-19.37111000	-19.0	22.0	14.0	4.70	14 M	SCO
730 21778	16.16902700	16.0	10.0	8.5	-27.63722200	-27.0	50.0	4.70	4.70	13	SCO
731 21819	16.20916000	16.0	12.0	14.1	-63.59861000	-63.0	35.0	4.03	4.03	0 D	TRA
732 21838	16.20847100	16.0	12.0	30.5	-3.60555550	-3.0	36.0	3.03	3.03	1 D	OPH
733 21920	16.27444400	16.0	16.0	28.0	-4.60861100	-4.0	36.0	3.34	3.34	2 E	OPH
734 21933	16.28686000	16.0	17.0	12.7	-50.07166600	-50.0	4.0	18.0	4.14	0 6	NOR
735 21987	16.31144400	16.0	18.0	41.2	46.39583300	46.0	23.0	3.91	3.91	22 Y	NOR
736 21982	16.31761000	16.0	19.0	3.4	-25.51055600	-25.0	30.0	3.80	3.80	20 S	SCO
737 22012	16.33958300	16.0	20.0	22.5	19.23416600	19.0	14.0	3.0	3.79	20 E	5ER
738 22020	16.34552700	16.0	20.0	43.9	30.97222100	30.0	58.0	4.72	4.72	19 C	CRB
739 22042	16.36752700	16.0	22.0	3.1	-19.95694400	-19.0	57.0	4.59	4.59	14 Y	OPH
740 22101	16.39186100	16.0	23.0	30.7	61.59305500	61.0	35.0	2.89	2.89	14 M	ORA
741 22090	16.39663800	16.0	23.0	47.9	14.11250000	14.0	6.0	4.53	4.53	24 W	5ER
742 22134	16.43177700	16.0	25.0	54.4	-8.29500000	-8.0	17.0	4.20	4.20	3 U	OPH
743 22157	ANTARES VESPERTIL16.45427700	16.0	27.0	15.4	-26.35611100	-26.0	21.0	2.81	3.22	21 A	SCO 10
744 22142	16.46702700	16.0	28.0	1.3	-78.82222200	-78.0	49.0	2.00	2.01	0 6	5ER
745 22193	KORNEPHOROS RUTIL16.47855500	16.0	28.0	42.8	21.56472200	21.0	33.0	5.30	2.81	27 B	5ER
746 22195	16.48403300	16.0	29.0	5.4	-34.62972200	-34.0	37.0	4.33	4.33	8	SCO
747 22200	16.48552700	16.0	29.0	7.9	-16.53805500	-16.0	32.0	4.40	4.40	0 V	OPH
748 22203	16.48577700	16.0	29.0	8.8	2.05916660	2.0	3.0	3.85	3.85	10 L	OPH
749 22221	16.50094400	16.0	30.0	3.4	-21.39305500	-21.0	23.0	4.57	4.57	19 W	OPH
750 22264	16.54955500	16.0	32.0	58.4	42.50833300	42.0	30.0	4.25	4.25	35 S	5ER
751 22303	16.56166600	16.0	33.0	42.0	-28.14500000	-28.0	8.0	2.91	2.91	23 Y	SCO

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

Star ID	Star Name	17.0	47.0	28.5	-37.0	2.0	3.0	3.55	0	SCD
810	24186	17.79125000	17.0	28.5	-37.03416400	2.0	3.0	3.55	0	SCD
811	24344	17.68202700	17.0	55.3	56.87749900	52.0	39.0	3.90	32 C	ORA
812	24415	17.91752700	17.0	55.0	37.25416700	15.0	15.0	3.99	91 J	HER
813	24432	ELTANIN	17.0	47.5	51.99222200	29.0	32.0	2.42	33 G	HER
814	24446	17.92986000	17.0	55.0	29.25055500	29.0	15.0	3.82	92 C	HER
815	24468	17.94005500	17.0	57.0	-9.77083300	-9.0	16.0	3.50	64 M	OPH
816	24478	17.95163800	17.0	57.0	30.19111100	30.0	11.0	4.76	94 N	HER
817	24502	17.95224900	17.0	58.0	16.75166600	16.0	45.0	4.71	93 Z	HER
818	24503	17.97494400	17.0	58.0	-3.68944400	-3.0	41.0	4.60	57 Z	HER
819	24509	17.97719400	17.0	58.0	2.93166640	2.0	55.0	3.92	67	OPH
820	24534	17.98149900	17.0	53.4	1.30444443	1.0	18.0	4.44	68	OPH
821	24534	17.99961000	17.0	58.4	-29.58333300	-29.0	35.0	4.00V	0	S6R
822	24632	NUSHABAI	18.0	47.0	-30.42638800	-30.0	25.0	3.07	10 G	S6R
823	24641	18.06416000	18.0	33.5	2.50611100	2.0	30.0	4.07	70	OPH
824	24635	18.06508300	18.0	41.1	-50.09611000	-50.0	46.0	3.90	0 J	ARA
825	24645	18.09382300	18.0	54.3	-63.67249900	-63.0	90.0	4.44	0 P	PAV
826	24693	18.09680500	18.0	5.0	8.72808550	8.0	33.0	4.73	71	OPH
827	24695	18.09400500	18.0	37.8	9.55749990	9.0	33.0	3.73	72	OPH
828	24694	18.09774900	18.0	51.9	-28.46277700	-28.0	46.0	4.66	0	S6R
829	24711	18.10291600	18.0	4.0	28.75638800	28.0	45.0	3.83	103 G	HER
830	24740	18.12100000	18.0	10.5	20.75638800	20.0	45.0	4.32	102	HER
831	24767	18.14383300	18.0	7.0	40.80777700	40.0	57.0	4.00	0 E	TEL
832	24856	18.19447100	18.0	8.0	-45.96249900	-45.0	57.0	4.00V	13 M	S6R
833	24944	18.25427700	18.0	37.8	-21.06972200	-21.0	4.0	3.16	0 M	S6R
834	24941	18.28436000	18.0	15.4	72.71805500	72.0	19.0	4.24	43 V	ORA
835	25032	18.31055500	18.0	18.1	34.04778000	34.0	2.0	3.69	44 X	ORA
836	25034	18.31255500	18.0	18.1	-36.77416600	-36.0	27.0	4.69	0	S6R
837	25046	18.32494900	18.0	40.1	-27.05694900	-27.0	3.0	4.69	0	S6R
838	25045	18.33336100	18.0	29.8	-29.84499900	-29.0	50.0	2.84	0	S6R
839	25114	18.43016600	18.0	1.1	-2.90944440	-2.0	34.0	3.42	58 M	SER
840	25122	18.43533200	18.0	21.0	-41.51222100	-41.0	30.0	4.25	0 C	PAV
841	25100	KAUS AUSTR.	18.0	15.4	71.31944900	71.0	19.0	4.24	43 V	ORA
842	25116	18.37003000	18.0	18.1	21.75250000	21.0	43.0	3.92	109 A	TEL
843	25154	18.40430500	18.0	22.7	-45.98972100	-45.0	29.0	3.76	0 A	TEL
844	25180	KAUS-BOR.	18.0	48.4	-25.44277800	-25.0	5.0	2.94	22 L	S6R
845	25193	18.43589300	18.0	8.1	-49.09194900	-49.0	31.0	4.73	0 G	SCT
846	25220	18.45336000	18.0	12.1	-14.58972220	-14.0	35.0	4.73	0 G	SCT
847	25313	18.51672200	18.0	3.0	-42.33722500	-42.0	20.0	4.69	0 J	CRA
848	25305	18.55027000	18.0	18.1	-8.27000000	-8.0	16.0	4.04	0 A	SCT
849	25466	VEGA	18.0	35.0	38.75000000	38.0	45.0	1.14	3 A	LYR
850	25466	18.59586100	18.0	57.3	-71.44138800	-71.0	27.0	4.10	0 Z	PAV
851	25522	18.64925000	18.0	21.4	-9.08750000	-9.0	5.0	4.70V	0 D	SCT
852	25648	18.72033300	18.0	13.2	39.57527700	39.0	31.0	4.50	5 E	LYR
853	25641	18.72450000	18.0	43.0	-27.02861100	-27.0	43.0	3.30	27 V	SAG
854	25676	18.72608300	18.0	33.9	37.56749900	37.0	34.0	4.29	6 Z	LYR
855	25698	18.73589800	18.0	9.2	20.51166600	20.0	30.0	4.26	110	HER
856	25730	18.75527700	18.0	19.0	-47.78494400	-47.0	47.0	4.47	0 B	SCT
857	25734	18.75788800	18.0	28.4	18.19411000	18.0	8.0	4.37	111	HER
858	25735	18.76022100	18.0	36.8	-57.74916660	-57.0	44.0	4.00V	0	SCT
859	25847	SHELLIAK	18.0	48.0	33.32083300	33.0	19.0	3.38	10 B	LYR
860	25823	18.681630500	18.0	48.0	-62.23027700	-62.0	13.0	4.42	0 L	PAV
861	25941	MUNKI	18.0	53.0	-26.34194400	-26.0	31.0	2.14	34 S	S6R
862	25954	18.88991600	18.0	5.7	22.59944400	22.0	35.0	4.56	113	HER
863	25959	18.88791000	18.0	16.7	36.85233300	36.0	51.0	4.50V	12 D	LYR
864	25930	18.88916600	18.0	21.0	-67.28027700	-67.0	16.0	4.00V	0 K	PAV
865	25996	18.90447100	18.0	14.1	43.89888900	43.0	53.0	4.00V	13	LYR
866	25991	ALYA	18.0	54.0	4.15666660	4.0	9.0	4.50	63 J	SER
867	26019	18.92736000	18.0	55.0	-21.15444400	-21.0	9.0	3.61	37 C	S6R

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

868	26084	SULAPHAT	18+96055500	18+0	57+0	38+0	32+64027700	32+0	38+0	25+0	3+30	14 6	LYR
869	26091		18+96722200	18+0	58+0	2+0	15+01944400	15+0	1+0	10+0	4+21	13 E	ABL
870	26141		18+99483300	18+0	59+0	48+6	-25+78972220	-5+0	47+0	23+0	4+15	12	ABL
871	26161	ASCELLA	19+00441400	19+0	0	23+1	-29+93194400	-29+0	55+0	55+0	2+71	38 Z	SGR
872	26224		19+04308300	19+0	2+0	35+1	-21+7944400	-21+0	47+0	40+0	3+90	39 O	SGR
873	26270		19+06333300	19+0	3+0	48+0	13+61000000	13+0	48+0	36+0	3+02	17 Z	ABL
874	26263		19+06675500	19+0	4+0	3+2	-37+1152700	-37+0	6+0	55+0	0 6	CRA	CRA
875	26285		19+07316600	19+0	4+0	23+9	-4+9363880	-4+0	56+0	11+0	3+55	16 L	ABL
876	26291		19+07924900	19+0	4+0	45+3	-27+7233200	-27+0	43+0	24+0	3+42	40 T	SGR
877	26322		19+09855500	19+0	5+0	54+8	-40+5527800	-40+0	33+0	10+0	4+66	0 0	CRA
878	26360		19+11822200	19+0	7+0	5+6	-37+96083300	-37+0	57+0	39+0	4+12	0 A	CRA
879	26380		19+12702700	19+0	7+0	37+3	-39+39833300	-39+0	23+0	54+0	4+16	0 B	CRA
880	26386		19+12802700	19+0	7+0	40+9	-21+08083300	-21+0	4+0	51+0	3+02	41 P	SGR
881	26520	MODUS II	19+20914400	19+0	12+0	33+0	67+59999900	67+0	36+0	7+0	3+24	57 D	ORA
882	26507		19+20914400	19+0	12+0	33+9	39+08472100	39+0	5+0	5+0	4+46	20 M	LYR
883	26569		19+24516600	19+0	14+0	42+6	21+32749900	21+0	19+0	39+0	4+60	1	VUL
884	26585		19+25252700	19+0	15+0	9+1	38+07027700	38+0	4+0	13+0	4+46	21 J	LYR
885	26638		19+27058300	19+0	14+0	14+1	73+29111100	73+0	17+0	28+0	4+63	60 Y	ORA
886	26621		19+27155500	19+0	16+0	17+4	53+30333300	53+0	18+0	12+0	3+98	1 K	CY6
887	26694		19+32738900	19+0	19+0	38+6	-17+91972200	-17+0	54+0	53+0	3+95	44 R	SGR
888	26697		19+32869400	19+0	19+0	43+3	-16+02222200	-16+0	1+0	20+0	4+58	46 U	SGR
889	26703	ARKAB-PRIOR	19+33538800	19+0	20+0	7+4	-4+52666600	-4+0	31+0	36+0	4+24	0 8	SGR
890	26735		19+34152700	19+0	20+0	29+5	65+64694300	65+0	38+0	49+0	4+63	58 P	ORA
891	26718	ARKAB-POSTERIOR	19+34488900	19+0	20+0	41+6	-48+86749900	-48+0	52+0	3+0	4+51	0 A	SGR
892	26737	ALRAMI	19+35722200	19+0	21+0	27+8	-40+88361100	-40+0	41+0	1+0	4+11	0 B	SGR
893	26816	DENEK OKAB	19+39555500	19+0	23+0	44+0	3+03361100	3+0	2+0	37+0	3+44	30 D	ABL
894	26904		19+45413800	19+0	27+0	14+9	24+59277700	24+0	35+0	34+0	4+63	6 A	VUL
895	26947		19+48038900	19+0	28+0	49+4	51+6544400	51+0	39+0	16+0	3+94	10 I	CY6
896	26953	ALBIREO	19+48847200	19+0	29+0	18+8	27+88500000	27+0	53+0	4+0	3+24	6 B	CY6
897	27030		19+53943900	19+0	32+0	22+7	7+30333300	7+0	18+0	12+0	4+65	38 M	ABL
898	27089		19+57305500	19+0	38+0	34+7	-24+98250000	-24+0	57+0	45+0	4+66	52	SGR
899	27103		19+58183300	19+0	34+0	54+6	-1+34555554	-1+0	21+0	56+0	4+28	41 I	ABL
900	27141		19+59169400	19+0	35+0	30+1	50+13916400	50+0	8+0	21+0	4+64	13 J	CY6
901	27215	SHAM	19+64216400	19+0	38+0	31+8	17+93194400	17+0	55+0	55+0	4+37	5 A	SGE
902	27234		19+65791600	19+0	39+0	28+5	17+39361100	17+0	23+0	37+0	4+45	6 B	SGE
903	27347		19+71330500	19+0	43+0	52+7	45+04444400	45+0	2+0	40+0	2+97	18 0	CY6
904	27354	REDA	19+74325000	19+0	44+0	35+7	10+52666600	10+0	31+0	36+0	2+80	50 8	ABL
905	27391		19+76377700	19+0	45+0	49+6	18+44666600	18+0	28+0	48+0	3+78	7 0	SGE
906	27471	TYL	19+80999900	19+0	48+0	41+9	70+17888900	70+0	10+0	44+0	3+99	43 C	ORA
907	27470	ALTAIR	19+81791600	19+0	49+0	41+5	8+77444400	8+0	48+0	28+0	4+89	53 A	ABL
908	27481		19+82030500	19+0	49+0	13+1	32+82444400	32+0	49+0	28+0	4+00V	0 X	ABL
909	27517		19+84083300	19+0	50+0	41+4	99+444443	99+0	54+0	52+0	3+00V	55 M	CY6
910	27544		19+86619400	19+0	51+0	58+3	23+98722200	23+0	59+0	14+0	4+50	13	VUL
911	27557		19+88083300	19+0	52+0	51+0	-41+96194400	-41+0	57+0	43+0	4+21	0 I	SGR
912	27587	ALSHAIN	19+89322200	19+0	53+0	35+6	6+31805550	6+0	19+0	8+0	3+90	40 B	ABL
913	27605		19+91336000	19+0	54+0	48+1	-27+28416600	-27+0	19+0	51+0	4+62	59	SGR
914	27642		19+91652700	19+0	54+0	59+5	34+98949400	34+0	59+0	22+0	4+03	21 M	CY6
915	27631		19+92916600	19+0	55+0	34+5	-73+00583300	-73+0	0	21+0	4+10	12 6	PAY
916	27672		19+95330500	19+0	57+0	11+9	19+39583300	19+0	23+0	45+0	3+71	12 6	SGE
917	27670		19+95749400	19+0	57+0	27+7	-35+37277700	-35+0	22+0	23+0	4+39	0 J	SGR
918	27753		19+99430500	19+0	59+0	39+5	-27+65583300	-27+0	39+0	21+0	4+74	15	VUL
919	27793		20+00847200	20+0	0	30+5	-27+80861000	-27+0	48+0	31+0	4+60	62	SGR
920	27856		20+04441600	20+0	2+0	39+9	67+77361100	67+0	48+0	25+0	4+66	47 8	ORA
921	27884		20+08847100	20+0	5+0	18+5	-66+27361100	-66+0	16+0	28+0	3+64	0 0	PAY
922	28010		20+15830500	20+0	9+0	29+9	-9+2666665	9+0	55+0	38+0	3+37	45 J	ABL
923	28044		20+16836000	20+0	10+0	6+1	77+60694400	77+0	36+0	25+0	4+40	1 K	CEP
924	28099		20+20860500	20+0	12+0	31+7	46+63444400	46+0	38+0	4+0	3+95	31 0	CY6
925	28108		20+20974900	20+0	12+0	35+1	56+45999900	56+0	27+0	38+0	4+32	33	CY6

TABLE I. - STAR IDENTIFICATION CATALOGUE - Continued

Star ID	Name	20+0	14+0	19+0	27+0	42+0	21+0	4+7J	Star ID	Name	20+0	14+0	19+0	27+0	42+0	21+0	4+7J
926	28152	20+23861000	20+0	14+0	19+0	27+0583300	27+0	42+0	21+0	4+7J	VUL	23	4.73	4.14	4.16	4.14	4.14
927	28160	20+23980500	20+0	14+0	23+3	47+60611100	47+0	36+0	22+0	4.16	CYG	32	4.14	4.16	4.16	4.16	4.16
928	28189	20+26180500	20+0	15+0	42+5	-12+61777700	-12+0	37+0	4+0	4.15	CAP	5	4.15	4.15	4.15	4.15	4.15
929	28200	20+26855500	20+0	16+0	6+8	-12+65472200	-12+0	39+0	17+0	3.77	CAP	6	3.77	3.77	3.77	3.77	3.77
930	28295	20+31741800	20+0	19+0	2+7	-14+089333300	-14+0	53+0	36+0	3.25	CAP	9	3.25	3.25	3.25	3.25	3.25
931	28338	20+34950000	20+0	20+0	58+2	40+14388800	40+0	8+0	38+0	2.32	CYG	37	2.32	2.32	2.32	2.32	2.32
932	28378	20+34950000	20+0	20+0	58+2	40+14388800	40+0	8+0	38+0	4.60	CYG	39	4.60	4.60	4.60	4.60	4.60
933	28374	20+38147200	20+0	22+0	53+3	-56+84916800	-56+0	50+0	57+0	2.12	A	0	2.12	2.12	2.12	2.12	2.12
934	28513	20+46055500	20+0	27+0	57+8	30+25033300	30+0	15+0	3+0	4.09	CYG	41	4.09	4.09	4.09	4.09	4.09
935	28541	20+48327700	20+0	28+0	59+8	62+87611100	62+0	34+0	34+0	4.28	DEL	2	4.28	4.28	4.28	4.28	4.28
936	28593	20+52566600	20+0	31+0	32+4	11+10305500	11+0	10+0	59+0	3.98	DEL	2	3.98	3.98	3.98	3.98	3.98
937	28659	20+566119400	20+0	33+0	40+3	14+55249990	14+0	33+0	9+0	4.69	DEL	4	4.69	4.69	4.69	4.69	4.69
938	28682	20+56819400	20+0	35+0	6+7	-47+41499900	-47+0	24+0	54+0	3.21	IND	0	3.21	3.21	3.21	3.21	3.21
939	28709	20+56819400	20+0	35+0	6+7	-47+41499900	-47+0	24+0	54+0	3.72	DEL	6	3.72	3.72	3.72	3.72	3.72
940	28725	20+60883300	20+0	36+0	31+8	-1+22861110	-1+0	13+0	43+0	4.51	ABL	7	4.51	4.51	4.51	4.51	4.51
941	28780	20+63352700	20+0	38+0	1+7	14+47222200	14+0	28+0	20+0	3.86	CYG	9	3.86	3.86	3.86	3.86	3.86
942	28846	20+67061100	20+0	40+0	14+2	45+15444400	45+0	9+0	16+0	1.33	DEL	50	1.33	1.33	1.33	1.33	1.33
943	28860	20+69127700	20+0	41+0	28+6	-52+04749900	-52+0	23+0	51+0	4.70	IND	0	4.70	4.70	4.70	4.70	4.70
944	28873	20+69705500	20+0	41+0	49+4	14+94777700	14+0	56+0	52+0	4.53	DEL	11	4.53	4.53	4.53	4.53	4.53
945	28882	20+69708300	20+0	41+0	49+5	-66+33083200	-66+0	19+0	51+0	3.60	PAV	0	3.60	3.60	3.60	3.60	3.60
946	28929	20+73374900	20+0	44+0	1+5	-25+39805500	-25+0	23+0	53+0	4.24	CAP	14	4.24	4.24	4.24	4.24	4.24
947	28942	20+73691600	20+0	44+0	2+9	30+59111100	30+0	35+0	28+0	4.34	CYG	52	4.34	4.34	4.34	4.34	4.34
948	28956	20+74138800	20+0	44+0	29+0	57+45341100	57+0	27+0	13+0	4.63	CEP	4	4.63	4.63	4.63	4.63	4.63
949	28962	20+74299900	20+0	44+0	34+8	61+70250000	61+0	42+0	9+0	3.59	CEP	3	3.59	3.59	3.59	3.59	3.59
950	28959	20+74455500	20+0	44+0	47+6	33+83805500	33+0	50+0	17+0	2.64	CYG	53	2.64	2.64	2.64	2.64	2.64
951	28966	20+75055500	20+0	45+0	2+0	15+99722200	15+0	59+0	50+0	4.49	DEL	12	4.49	4.49	4.49	4.49	4.49
952	28978	20+76302700	20+0	45+0	6+9	-9+62449990	-9+0	37+0	28+0	4.00	ABR	3	4.00	4.00	4.00	4.00	4.00
953	28979	20+76403300	20+0	45+0	53+4	-5+15649440	-5+0	9+0	25+0	4.47	CTE	54	4.47	4.47	4.47	4.47	4.47
954	28994	20+76738800	20+0	46+0	2+6	36+26111000	36+0	21+0	3+0	4.24	CAP	88	4.24	4.24	4.24	4.24	4.24
955	28979	20+8281400	20+0	49+0	44+1	-27+05138800	-27+0	3+0	5+0	4.68	CAP	88	4.68	4.68	4.68	4.68	4.68
956	29150	20+8667700	20+0	52+0	4+4	44+25388800	44+0	15+0	14+0	4.68	CYG	57	4.68	4.68	4.68	4.68	4.68
957	29133	20+86813800	20+0	52+0	5+3	-58+58777800	-58+0	35+0	16+0	3.72	IND	0	3.72	3.72	3.72	3.72	3.72
958	29251	20+93111100	20+0	55+0	52+0	41+03166600	41+0	1+0	54+0	4.09	CYG	58	4.09	4.09	4.09	4.09	4.09
959	29331	20+98580500	20+0	59+0	8+9	-32+39583300	-32+0	23+0	45+0	4.71	MIC	0	4.71	4.71	4.71	4.71	4.71
960	29459	21+06091400	21+0	3+0	39+3	43+78750000	43+0	47+0	23+0	4.19	CAP	62	4.19	4.19	4.19	4.19	4.19
961	29460	21+06636100	21+0	3+0	58+9	-17+37305500	-17+0	22+0	49+0	4.40	CAP	24	4.40	4.40	4.40	4.40	4.40
962	29490	21+08472100	21+0	5+0	5+0	-25+14894400	-25+0	8+0	49+0	4.40	ABR	13	4.40	4.40	4.40	4.40	4.40
963	29571	21+12813800	21+0	7+0	41+3	-11+51444400	-11+0	30+0	52+0	4.32	ABR	24	4.32	4.32	4.32	4.32	4.32
964	29661	21+19074900	21+0	11+0	26+7	30+08250000	30+0	4+0	57+0	3.40	CYG	64	3.40	3.40	3.40	3.40	3.40
965	29591	21+21291400	21+0	12+0	46+5	9+84416660	9+0	51+0	57+0	4.76	CEP	5	4.76	4.76	4.76	4.76	4.76
966	29723	21+22314300	21+0	13+0	23+5	37+89527700	37+0	53+0	43+0	3.82	CYG	65	3.82	3.82	3.82	3.82	3.82
967	29735	21+23455500	21+0	14+0	4+4	5+10222220	5+0	6+0	8+0	4.14	CEP	67	4.14	4.14	4.14	4.14	4.14
968	29784	21+26730500	21+0	16+0	2+3	39+24722100	39+0	14+0	50+0	4.28	CEP	67	4.28	4.28	4.28	4.28	4.28
969	29802	21+27461100	21+0	16+0	28+6	34+74916600	34+0	44+0	44+0	4.42	CYG	68	4.42	4.42	4.42	4.42	4.42
970	29819	21+28649400	21+0	17+0	23+9	-53+59749900	-53+0	35+0	51+0	4.60	IND	0	4.60	4.60	4.60	4.60	4.60
971	29848	21+29572200	21+0	17+0	44+6	62+43494400	62+0	26+0	13+0	4.60	CEP	5	4.60	4.60	4.60	4.60	4.60
972	29903	21+33833200	21+0	20+0	18+0	-16+98472200	-16+0	59+0	5+0	4.30	CAP	32	4.30	4.30	4.30	4.30	4.30
973	29914	21+34111100	21+0	20+0	28+0	19+65388800	19+0	37+0	14+0	4.24	PEG	1	4.24	4.24	4.24	4.24	4.24
974	29979	21+39288800	21+0	23+0	34+4	-65+52611100	-65+0	31+0	34+0	4.30	PAV	0	4.30	4.30	4.30	4.30	4.30
975	30020	21+41119400	21+0	24+0	40+3	-22+56388800	-22+0	33+0	50+0	3.86	CAP	34	3.86	3.86	3.86	3.86	3.86
976	30059	21+44549900	21+0	26+0	43+8	-21+94055500	-21+0	57+0	38+0	4.59	CAP	36	4.59	4.59	4.59	4.59	4.59
977	30118	21+47024900	21+0	28+0	12+9	70+40644400	70+0	24+0	33+0	3.32	CEP	8	3.32	3.32	3.32	3.32	3.32
978	30137	21+49527700	21+0	29+0	43+0	-5+72611100	-5+0	43+0	37+0	3.07	ABR	22	3.07	3.07	3.07	3.07	3.07
979	30207	21+54436000	21+0	32+0	39+7	45+43638800	45+0	26+0	11+0	4.22	CEP	73	4.22	4.22	4.22	4.22	4.22
980	30252	21+56534100	21+0	35+0	7+3	-19+62388800	-19+0	37+0	26+0	4.72	CAP	39	4.72	4.72	4.72	4.72	4.72
981	30289	21+62761100	21+0	37+0	39+4	-77+5722200	-77+0	32+0	50+0	3.74	IND	0	3.74	3.74	3.74	3.74	3.74
982	30320	21+63588900	21+0	38+0	9+2	-16+82138800	-16+0	49+0	17+0	3.80	CAP	40	3.80	3.80	3.80	3.80	3.80
983	30440	21+70724900	21+0	42+0	24+1	58+61888800	58+0	37+0	8+0	4.00	CEP	0	4.00	4.00	4.00	4.00	4.00

TABLE I. - STAR IDENTIFICATION CATALOGUE - Concluded

1042	32061	22-98036100	22.0	58.0	49.3	-52.94222200	-52.0	56.0	32.0	4.18	0 Z	GRU
1043	32095	23-00508300	23.0	.0	18.3	42.13749900	42.0	9.0	15.0	3.60V	1 0	AND
1044	32135	23-03455500	23.0	2.0	4.4	27.89249900	27.0	53.0	33.0	2.61	53 B	PEG
1045	32134	23-03488900	23.0	2.0	5.6	3.63133880	3.0	37.0	53.0	4.5W	4 B	PSC
1046	32149	23-05024900	23.0	3.0	.9	15.01668670	15.0	1.0	.0	2.57	54 A	PEG
1047	32184	23-08188800	23.0	4.0	58.8	-43.70999900	-43.0	42.0	36.0	4.35	0 J	GRU
1048	32196	23-08733300	23.0	5.0	14.4	9.21999990	9.0	13.0	12.0	4.69	55	PEG
1049	32237	23-11297100	23.0	6.0	46.7	75.19833200	75.0	11.0	54.0	4.56	33 P	CEP
1050	32246	23-12636100	23.0	7.0	34.9	-21.34627700	-21.0	21.0	46.0	3.80	88	ABR
1051	32270	23-15972100	23.0	8.0	26.0	-45.43666600	-45.0	26.0	12.0	4.10	0 I	GRU
1052	32316	23-18233300	23.0	10.0	56.4	49.21472100	49.0	12.0	53.0	4.62	7	AND
1053	32346	23-20847100	23.0	12.0	30.5	-6.23808550	-6.0	19.0	17.0	4.40	90 V	ABR
1054	32374	23-23430500	23.0	14.0	3.5	-9.27861110	-9.0	16.0	43.0	4.46	91 Y	ABR
1055	32415	23-25583200	23.0	15.0	21.0	3.09083330	3.0	5.0	27.0	3.85	6 G	PSC
1056	32413	23-25661000	23.0	15.0	23.8	-58.42805500	-58.0	25.0	41.0	4.10	0 6	TUC
1057	32429	23-26808300	23.0	16.0	5.1	-9.37388890	-9.0	22.0	26.0	4.56	93 Y	ABR
1058	32450	23-28227800	23.0	16.0	56.2	-32.72305500	-32.0	43.0	23.0	4.51	0 6	SCL
1059	32503	23-31502700	23.0	18.0	54.1	23.54861100	23.0	32.0	55.0	4.65	62 Y	PEG
1060	32540	23-35222100	23.0	21.0	8.0	-20.29194400	-20.0	17.0	31.0	4.20	98	ABR
1061	32585	23-39380500	23.0	23.0	37.7	23.21111000	23.0	12.0	40.0	4.57	68 U	PEG
1062	32594	23-40347200	23.0	24.0	12.5	-20.83416600	-20.0	50.0	3.0	4.52	99	ABR
1063	32647	23-43649900	23.0	26.0	11.4	6.18638890	6.0	11.0	11.0	4.45	10 J	PSC
1064	32667	23-45636000	23.0	27.0	22.9	12.56722210	12.0	34.0	2.0	4.67	70	PEG
1065	32744	23-51830500	23.0	31.0	5.9	-38.01222100	-38.0	.0	44.0	4.46	0 8	SCL
1066	32832	23-59738900	23.0	35.0	50.6	46.26833300	46.0	16.0	6.0	4.00	14 L	AND
1067	32850	23-60688800	23.0	36.0	24.8	43.07416600	43.0	4.0	27.0	4.28	17 I	AND
1068	32875	23-62155500	23.0	37.0	53.6	77.43694300	77.0	26.0	13.0	3.42	35 8	CEP
1069	32879	23-63580500	23.0	38.0	8.9	5.43638890	5.0	26.0	11.0	4.28	17 I	PSC
1070	32884	23-64461000	23.0	38.0	40.4	44.14000000	44.0	6.0	24.0	4.33	19 K	AND
1071	32917	23-67097100	23.0	40.0	15.5	1.58749999	1.0	35.0	15.0	4.61	18 L	PSC
1072	32931	23-68177700	23.0	40.0	54.4	-14.73861110	-14.0	46.0	19.0	4.62	105 B	ABR
1073	33050	23-78508300	23.0	47.0	6.3	-28.32368700	-28.0	19.0	26.0	4.64	0 0	SCL
1074	33160	23-87708300	23.0	52.0	37.5	57.30472100	57.0	16.0	17.0	4.00V	7 R	CAS
1075	33230	23-93283200	23.0	55.0	58.2	24.94694400	24.0	56.0	49.0	4.75	84 Y	PEG
1076	33282	23-95852700	23.0	57.0	30.7	6.66944440	6.0	48.0	10.0	4.03	28 W	PSC
1077	33280	23-96849900	23.0	58.0	6.6	-45.77194400	-45.0	46.0	19.0	4.71	0 2	TUC
1078	33321	23-99702700	23.0	59.0	49.3	-77.25888800	-77.0	15.0	32.0	4.73	0 J	OCT

TRANSLUNAR INJECTION
BURN

TRANSLUNAR COAST

EARTH VIEWS

MOON VIEWS

LUNAR ORBIT
INSERTION BURN

LUNAR ORBIT PHASE

TRANSEARTH INJECTION
BURN

TRANSEARTH COAST

POST TEI

MOON VIEWS

EARTH VIEWS

ENTRY PHASE

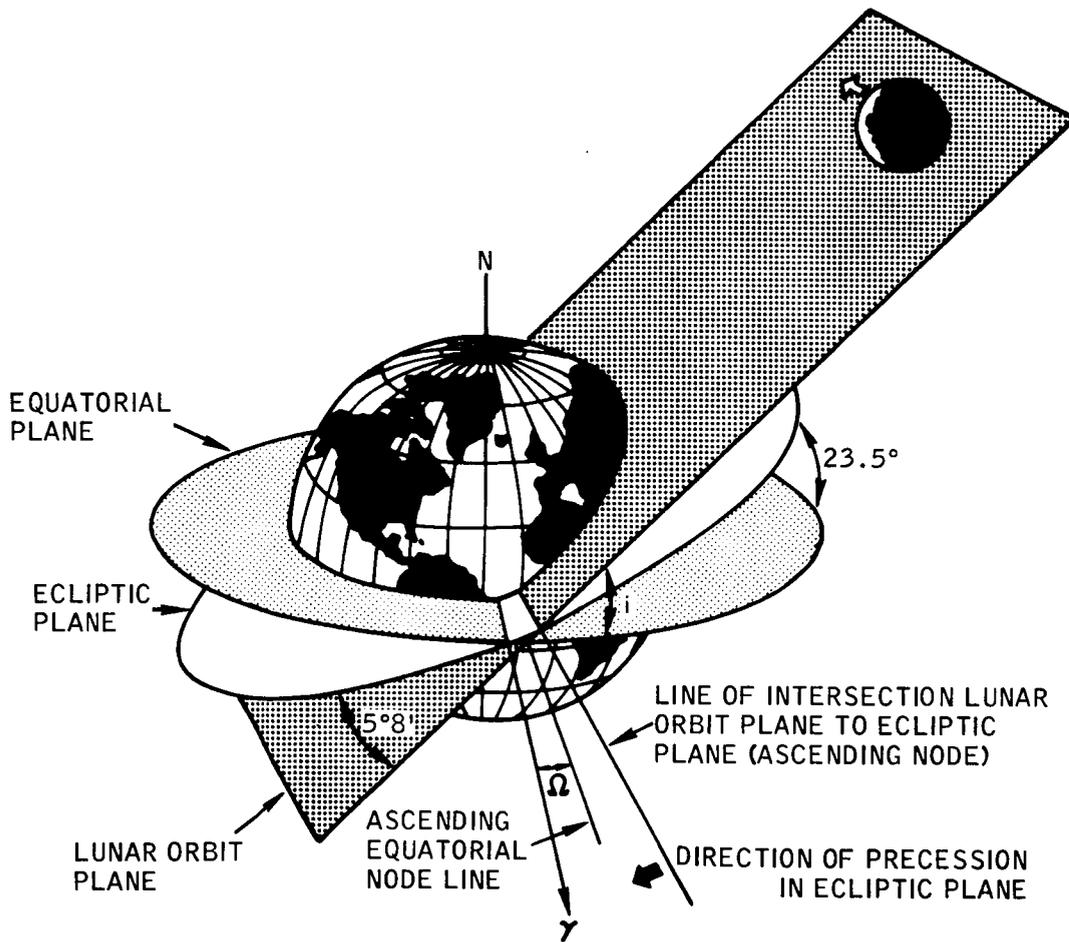


Figure 1. - Illustration of lunar orbit plane in year 1969 - inclination angle (i) $\approx 28^{\circ}$, right ascension of ascending equatorial node (Ω) $\approx 5^{\circ}$.

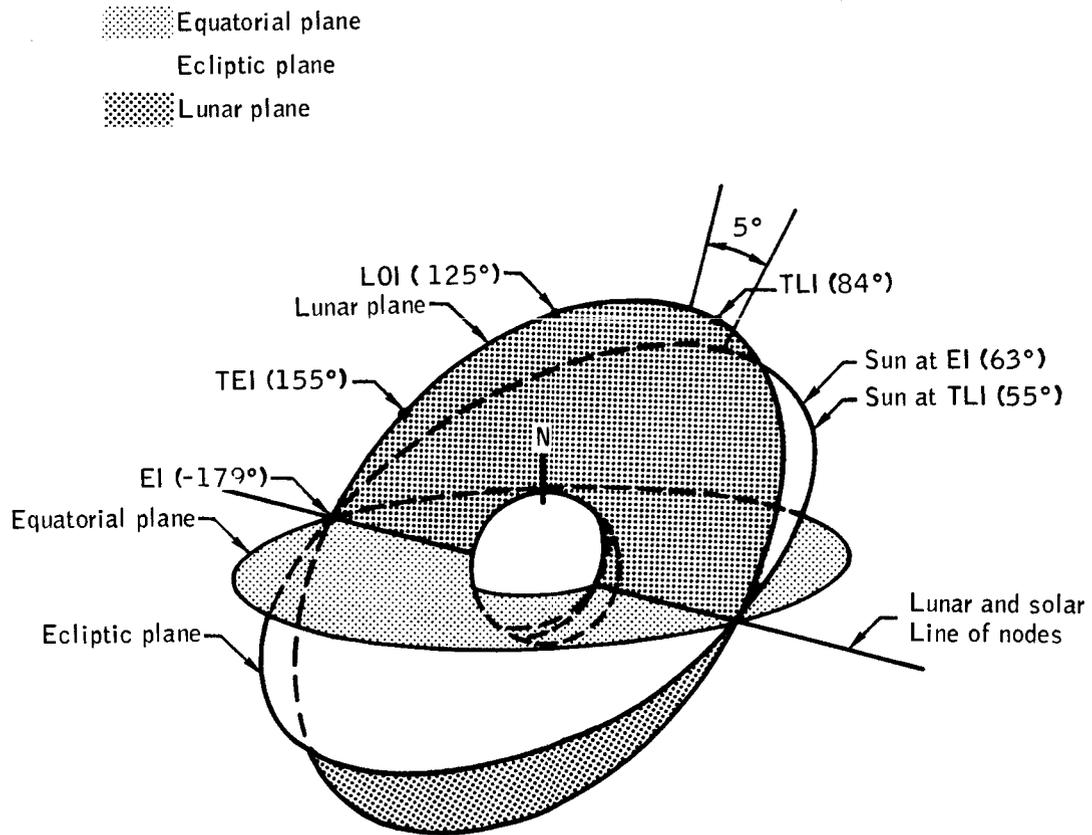


Figure 2.- Sun and moon location at major phases during Apollo 10 (Mission F).

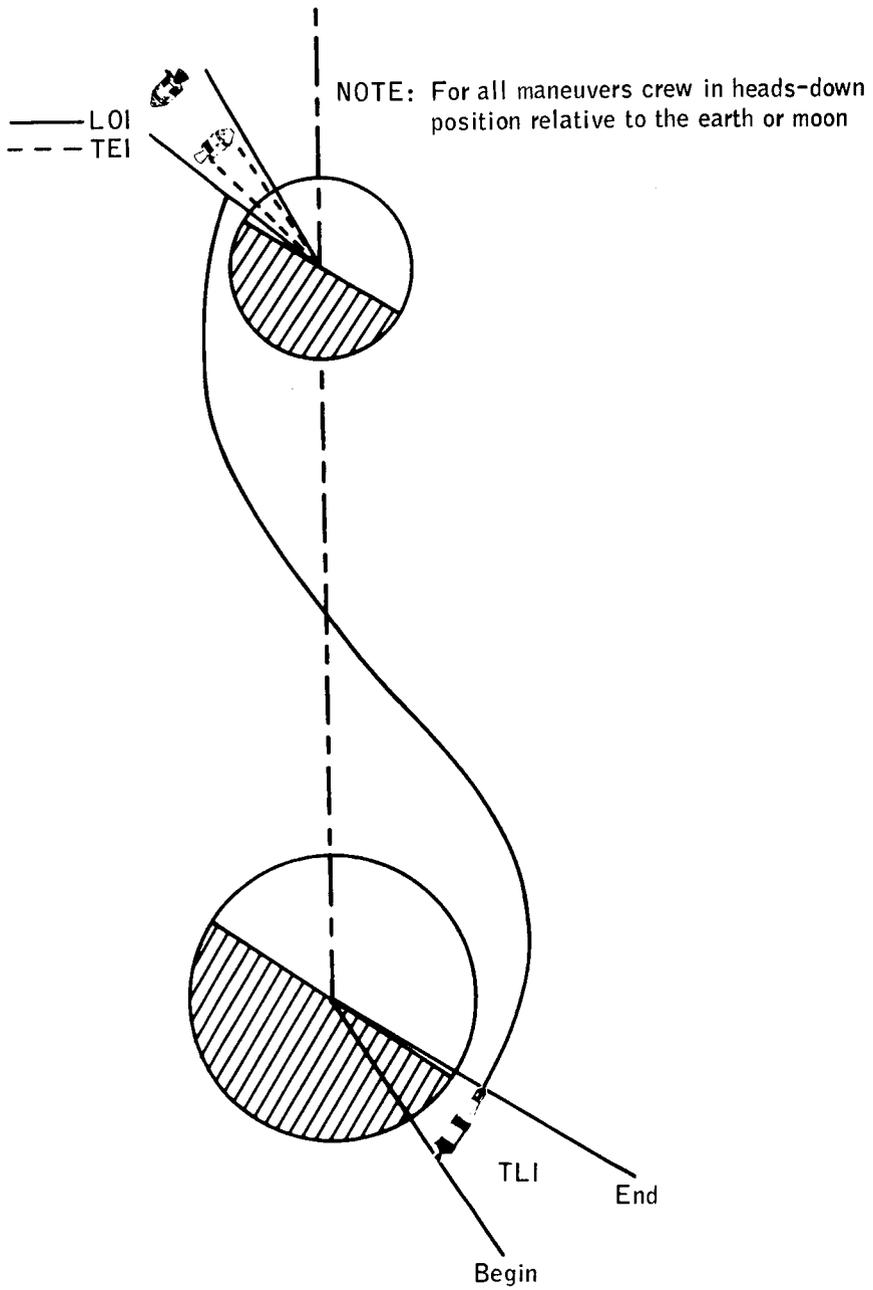


Figure 3.- A schematic of the maneuver attitudes and lighting conditions for the nominal Apollo 10 (Mission F).

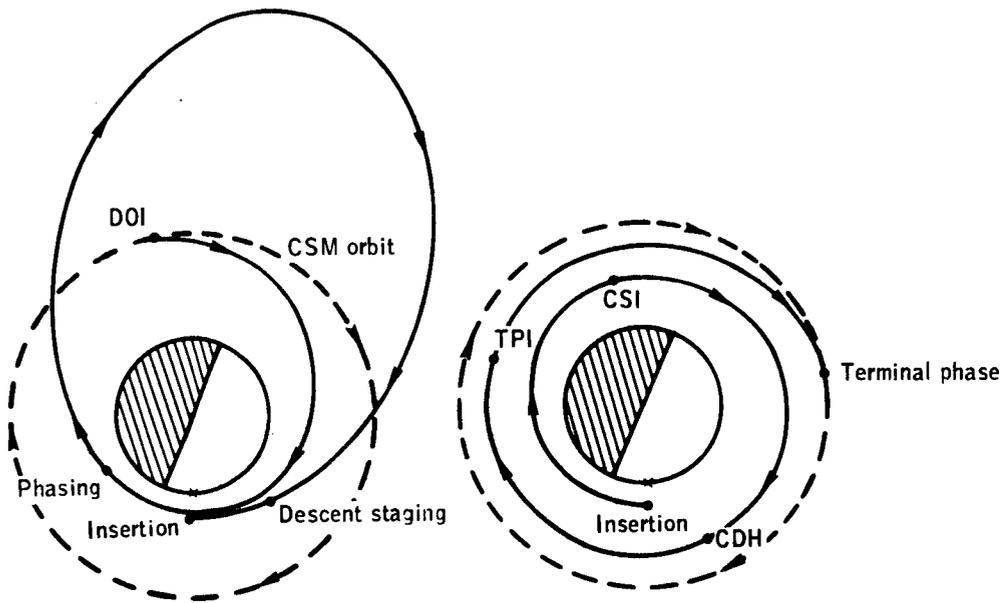


Figure 5. - F mission nominal rendezvous.

TRANSLUNAR INJECTION
BURN

SEC	4	5	7	15	22	25	41	63	75	80	984	1044	1046
X	9	20	3	-23	18	=13	8	C	0	=12	12	13	8
Y	=4	5	=8	=20	6	=13	2	3	5	0	-24	=10	=14

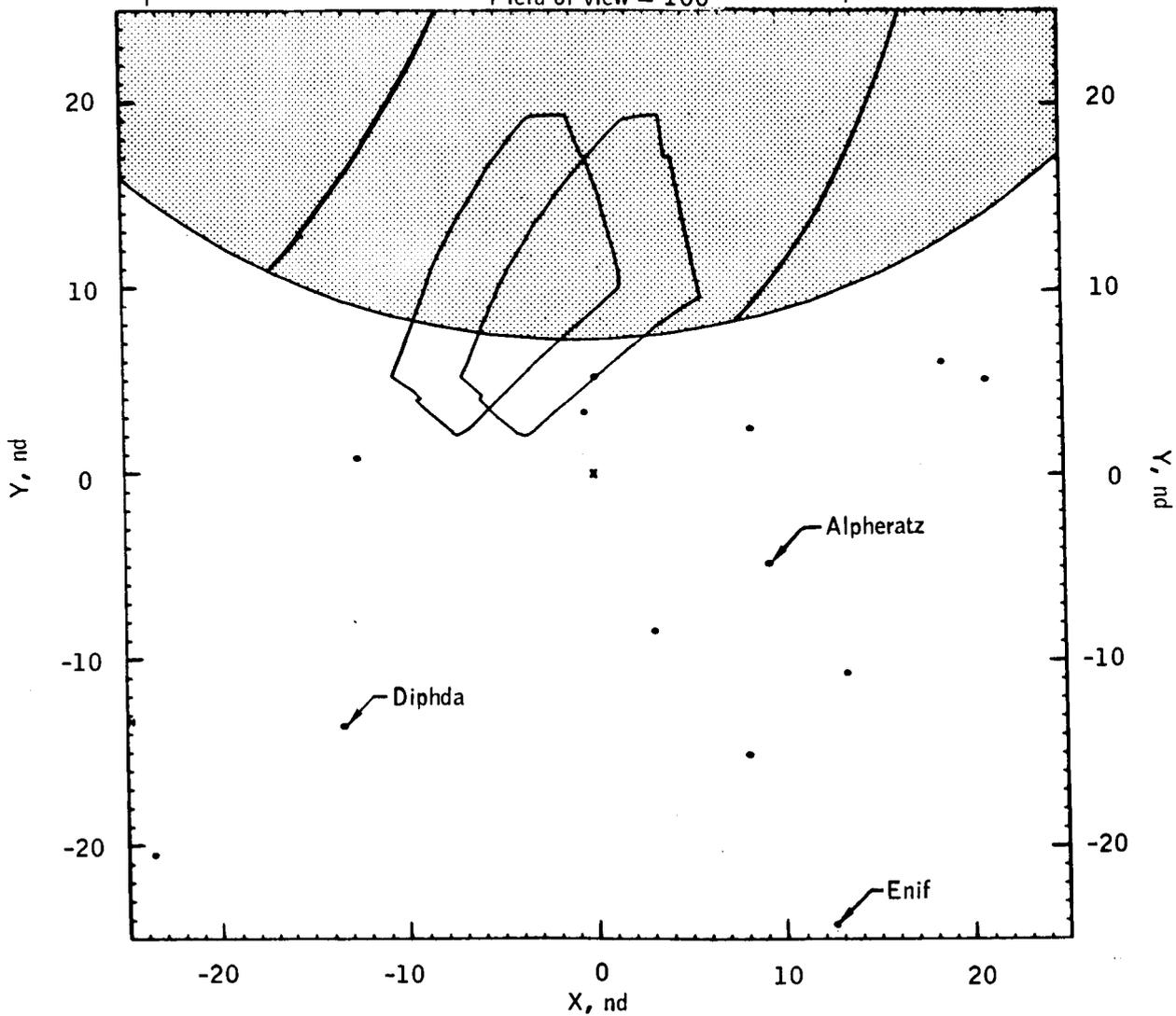
$R_E = 3547$ n. mi.

$V_i = 25\,568$ fps

$h_E = 121$ stat. mi.

$V_i = 17\,433$ mph

Field of view = 100°



(a) Begin TLI (g.e.t. = 2:33:17.7).

Figure 6. - Translunar injection burn.

SEQ	4	5	7	15	22	25	31	41	47	63	73	75	80
X	11	22	5	=23	20	-11	21	10	19	1	10	2	=10
Y	-10	0	-14	=24	1	=19	3	=3	5	-2	3	0	=4

SEQ	108	1044	1046
X	-9	15	10
Y	1	-16	-20

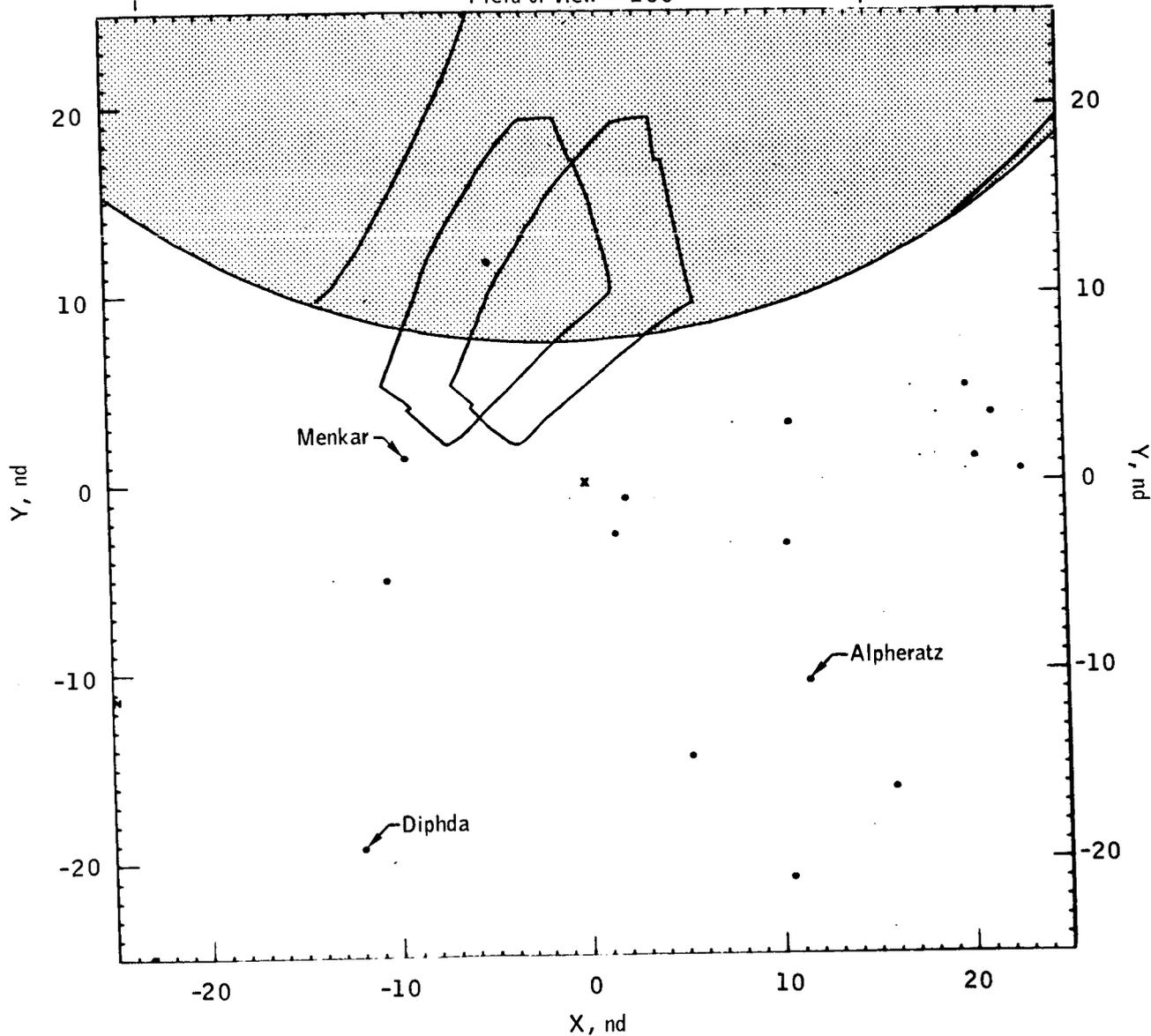
$R_E = 3552$ n. mi.

$V_i = 29\ 517$ fps

$h_E = 127$ stat. mi.

$V_i = 20\ 125$ mph

Field of view = 100°



(b) Middle of TLI (g.e.t. = 2:36:08.0).

Figure 6. - Continued.

SEQ	4	5	7	22	25	31	41	47	63	73	75	80	100
X	13	24	6	22	-11	22	12	21	3	12	3	-8	-9
Y	-14	-2	-18	=2	=22	0	=7	1	-6	=1	=5	=8	=2
SEQ	111	112	120	144	150	151	186	215	1044				
X	8	9	13	0	3	7	-4	-16	17				
Y	3	4	7	5	7	8	10	11	-20				

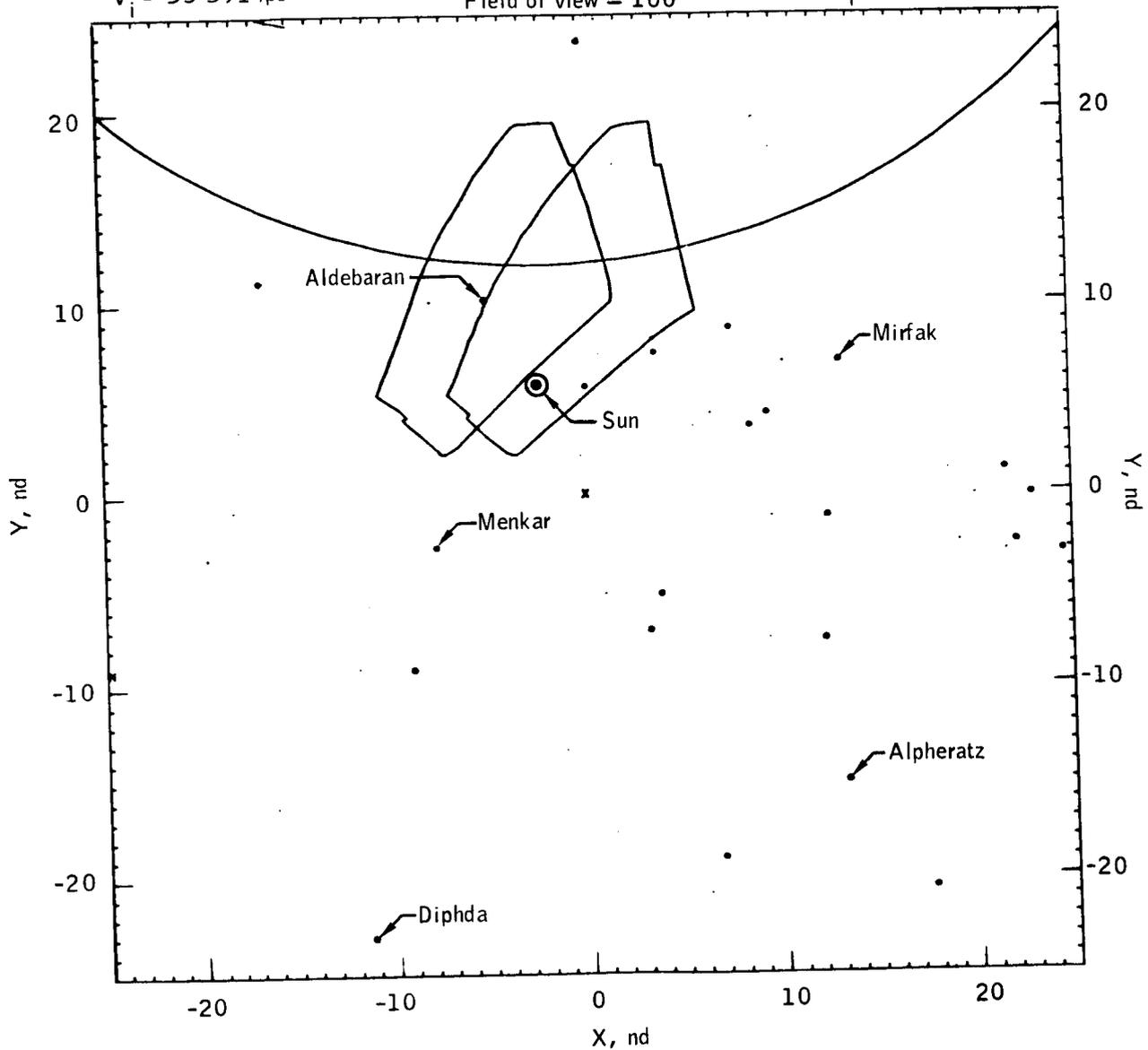
$R_E = 3613$ n. mi.

$V_i = 35\,591$ fps

$h_E = 196$ stat. mi.

$V_i = 24\,267$ mph

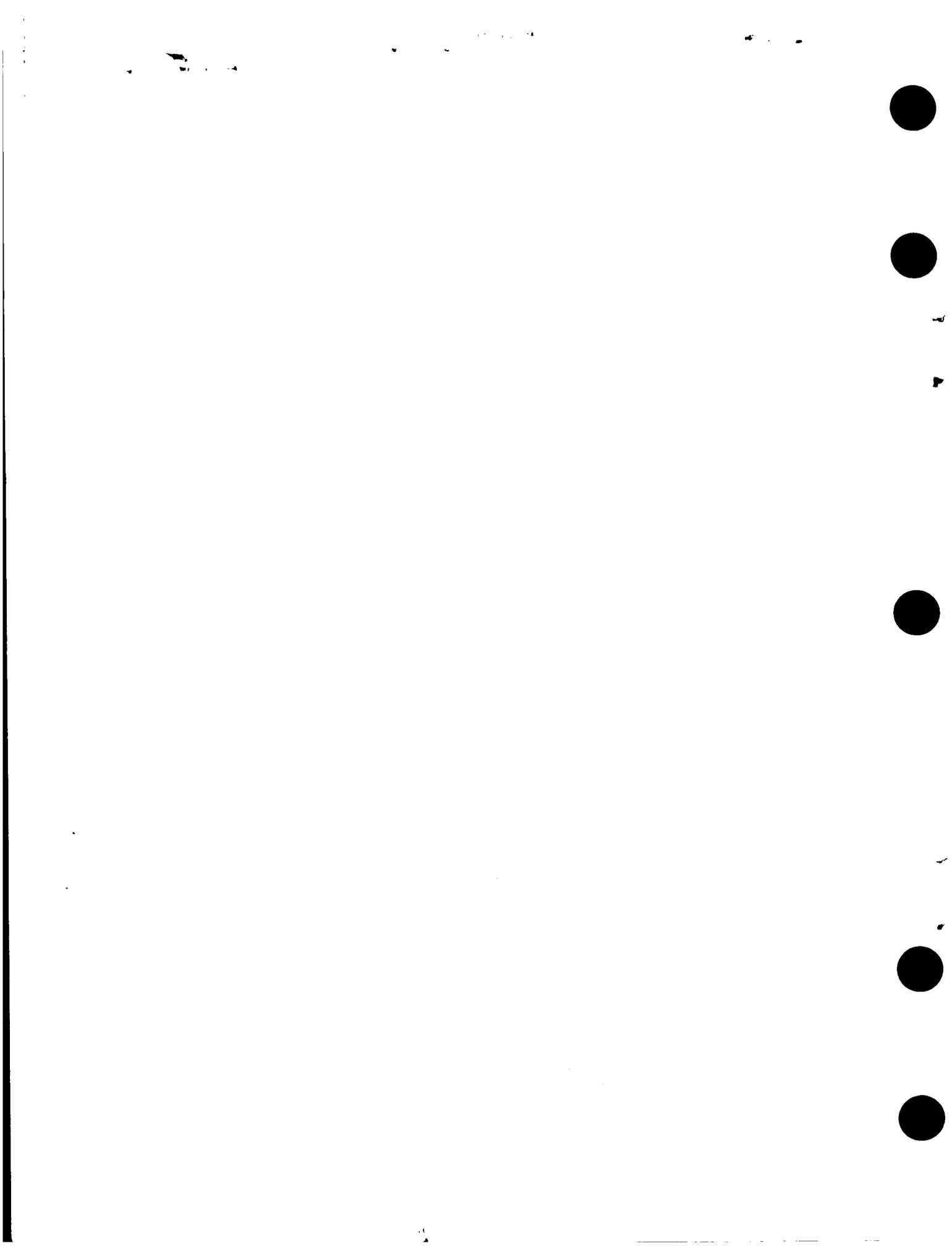
Field of view = 100°

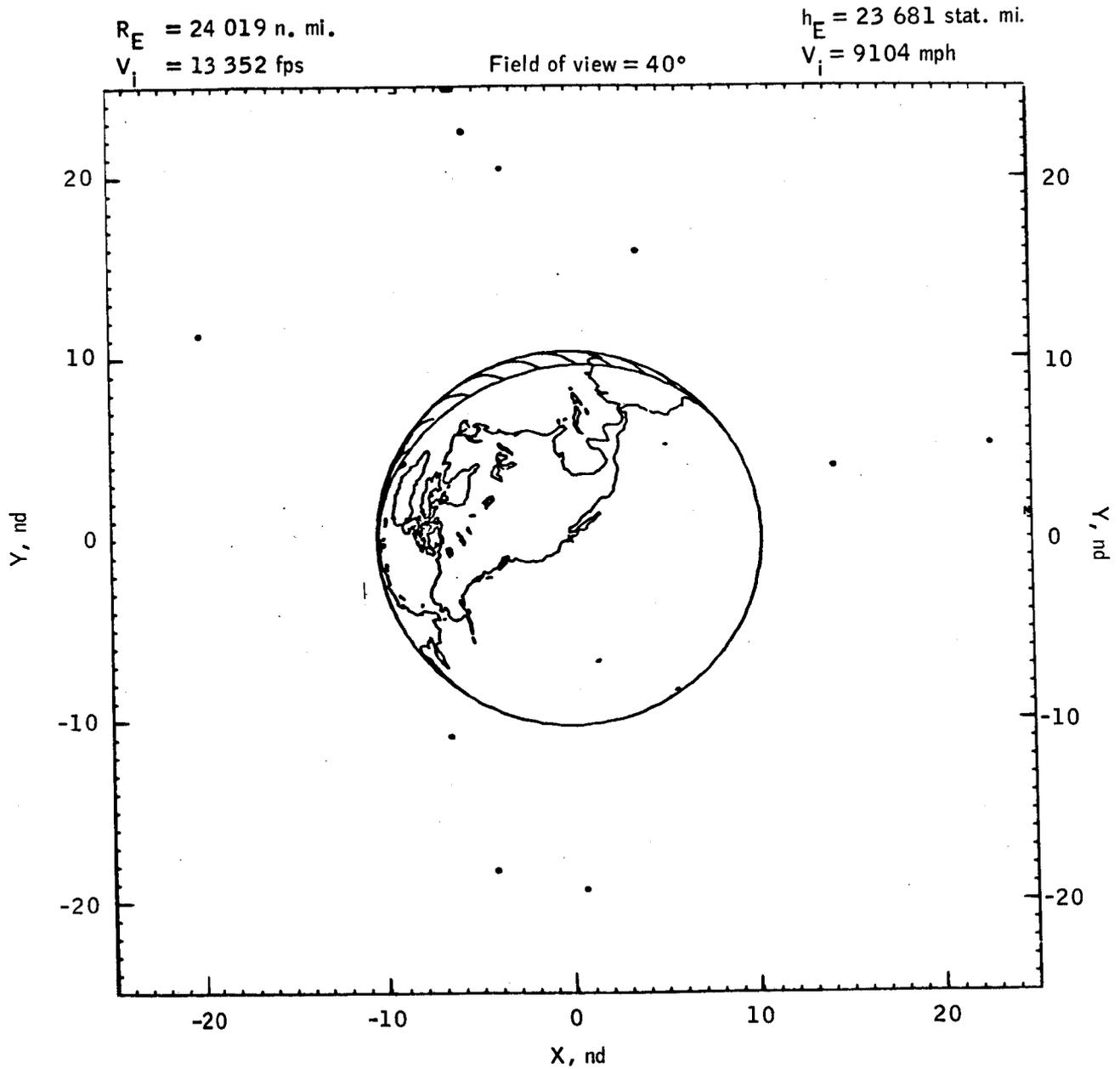


(c) End of TLI (g.e.t. = 2:38:59.5).

Figure 6. - Concluded.

TRANSLUNAR COAST





(a) G.e.t. = 5 hours.

Figure 7.- Translunar coast - constant field of view (earth).

SEQ	790	793	797	802	836	841	844
X	23	6	14	9	1	4	6
Y	25	25	24	22	12	12	9

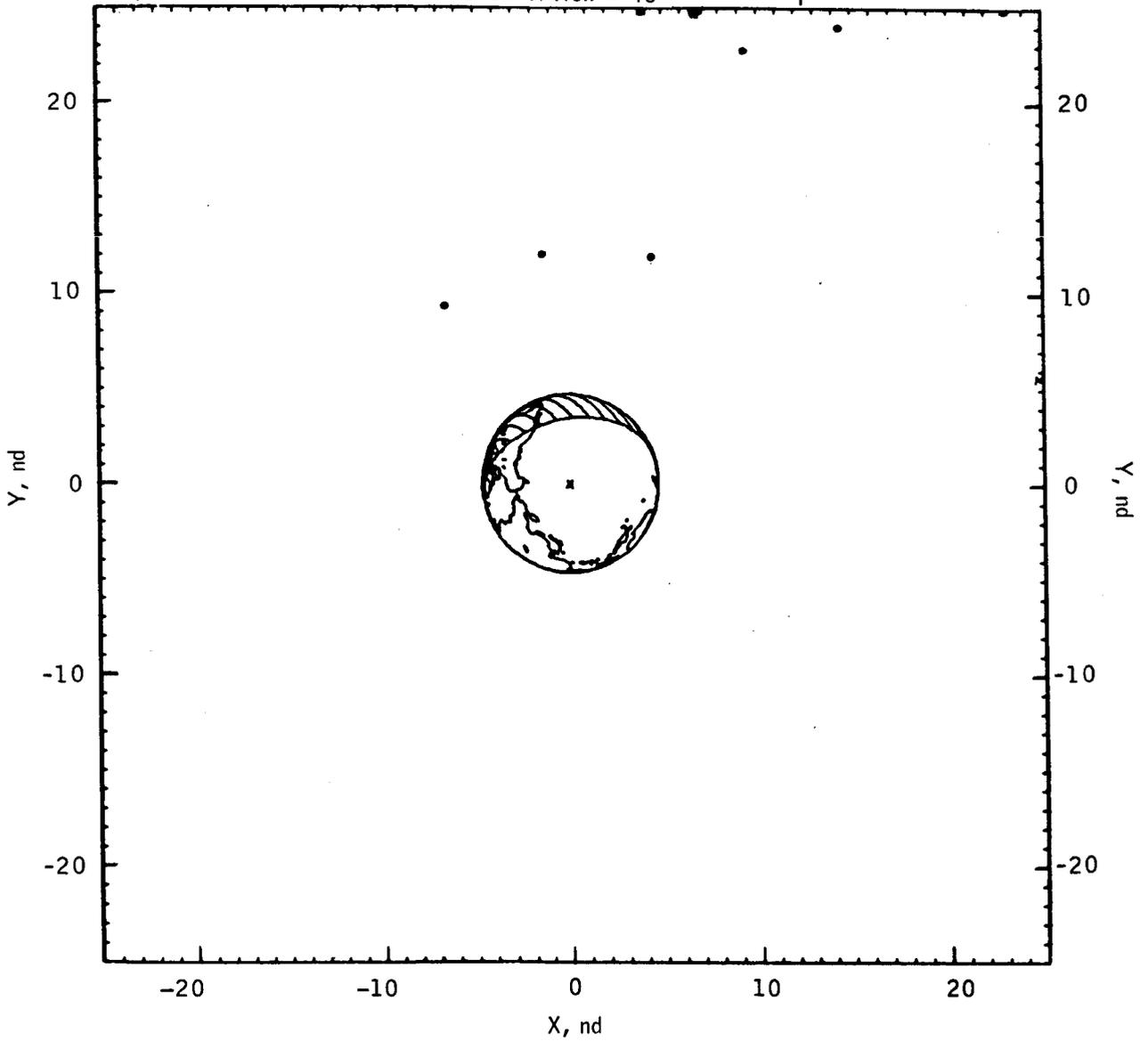
$R_E = 52\,882$ n.mi.

$V_i = 8541$ fps

$h_E = 56\,896$ stat. mi.

$V_i = 5823$ mph

Field of view = 40°



(b) G.e.t. = 10 hours.

Figure 7.- Continued.

SEQ	836	841	844	861	871
X	-1	4	-6	-4	0
Y	22	22	19	12	11

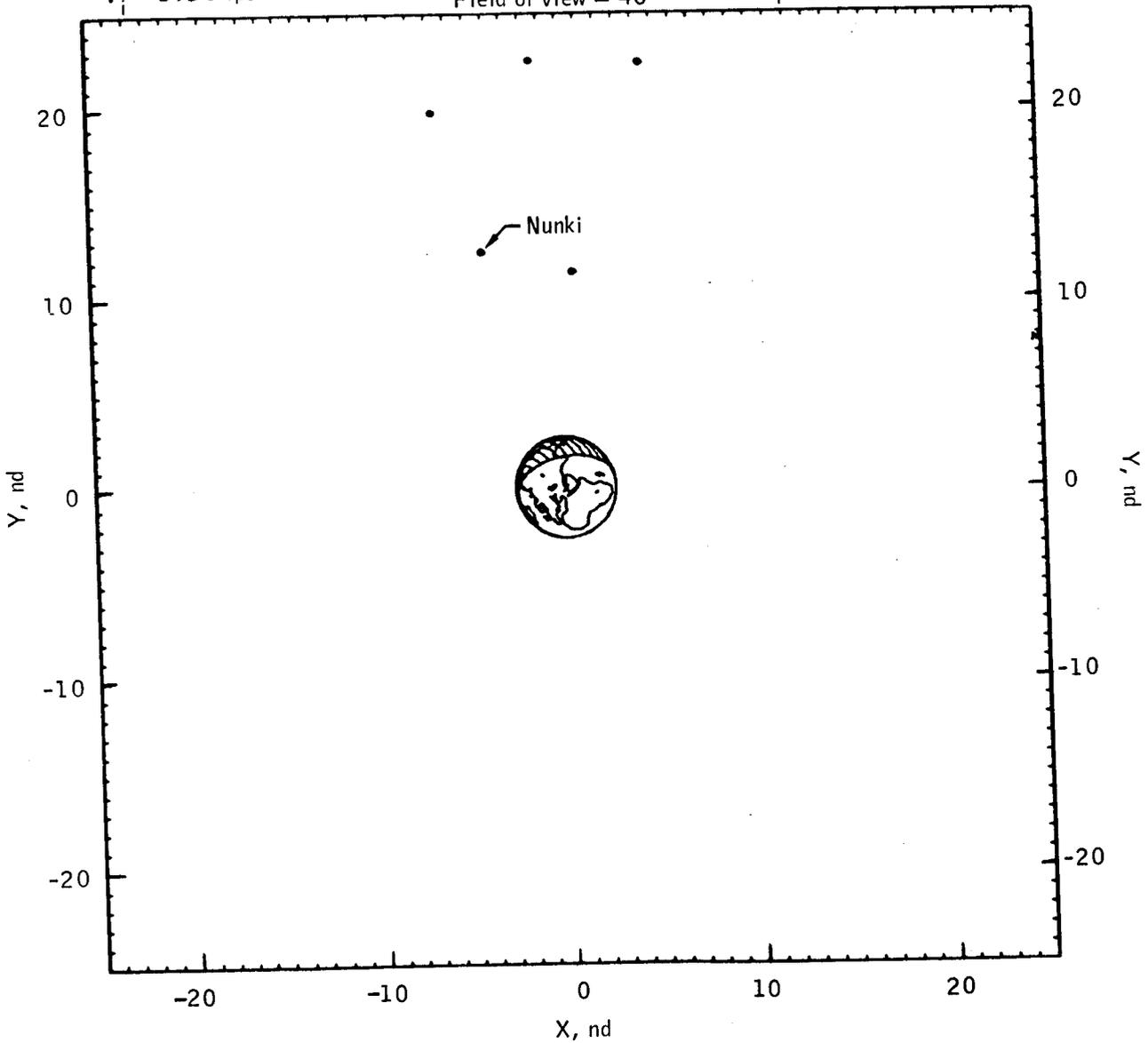
$R_E = 93\,028$ n. mi.

$h_E = 103\,440$ stat. mi.

$V_i = 5930$ fps

Field of view = 40°

$V_i = 4043$ mph



(c) G.e.t. = 20 hours.

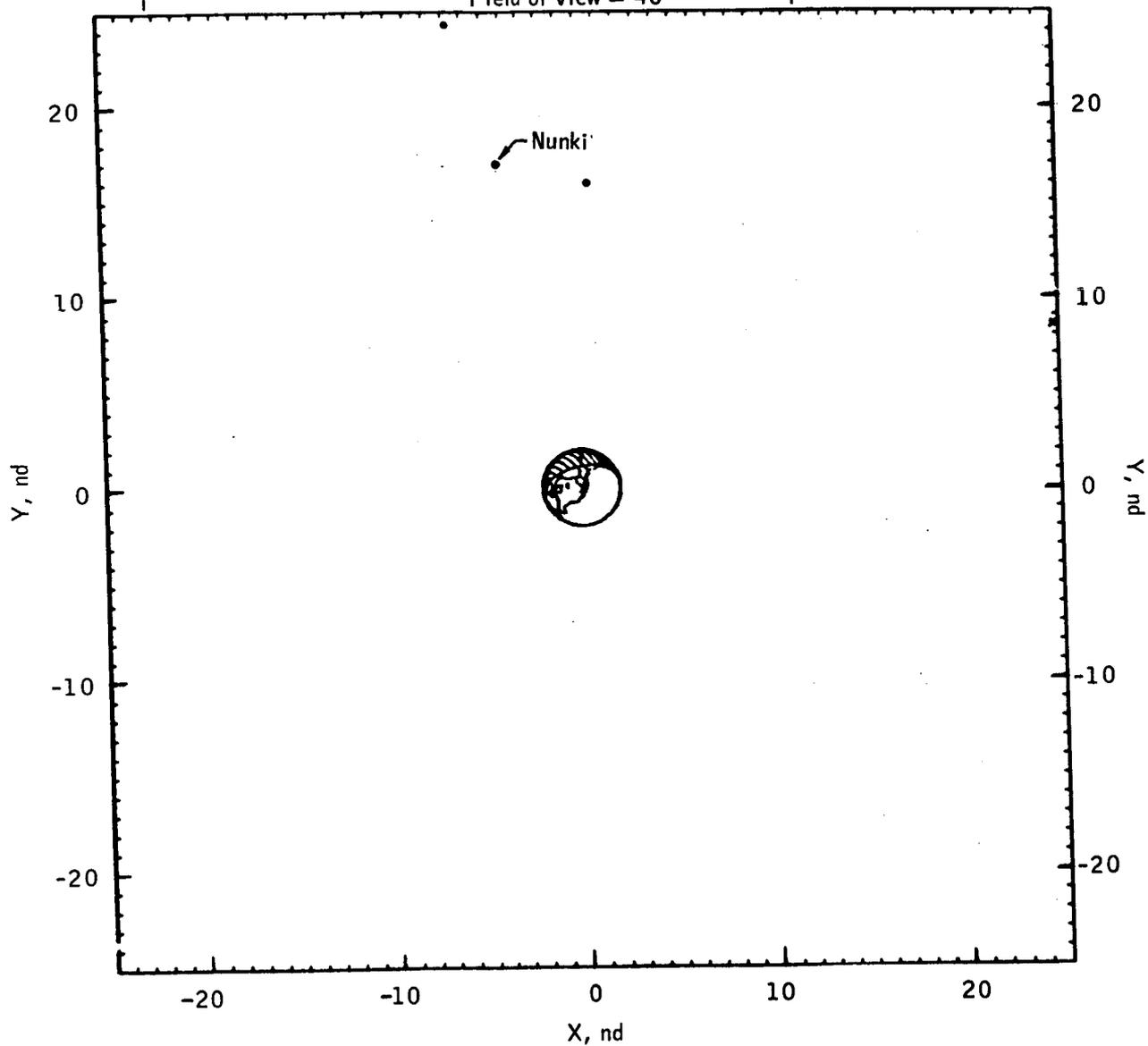
Figure 7.- Continued.

SEQ	044	061	071
X	-6	74	0
Y	24	17	16

 $R_E = 123\,687$ n. mi.

 $V_i = 4782$ fps

 $h_E = 138\,375$ stat. mi.

 $V_i = 3260$ mph
Field of view = 40° 

(d) G.e.t. = 30 hours.

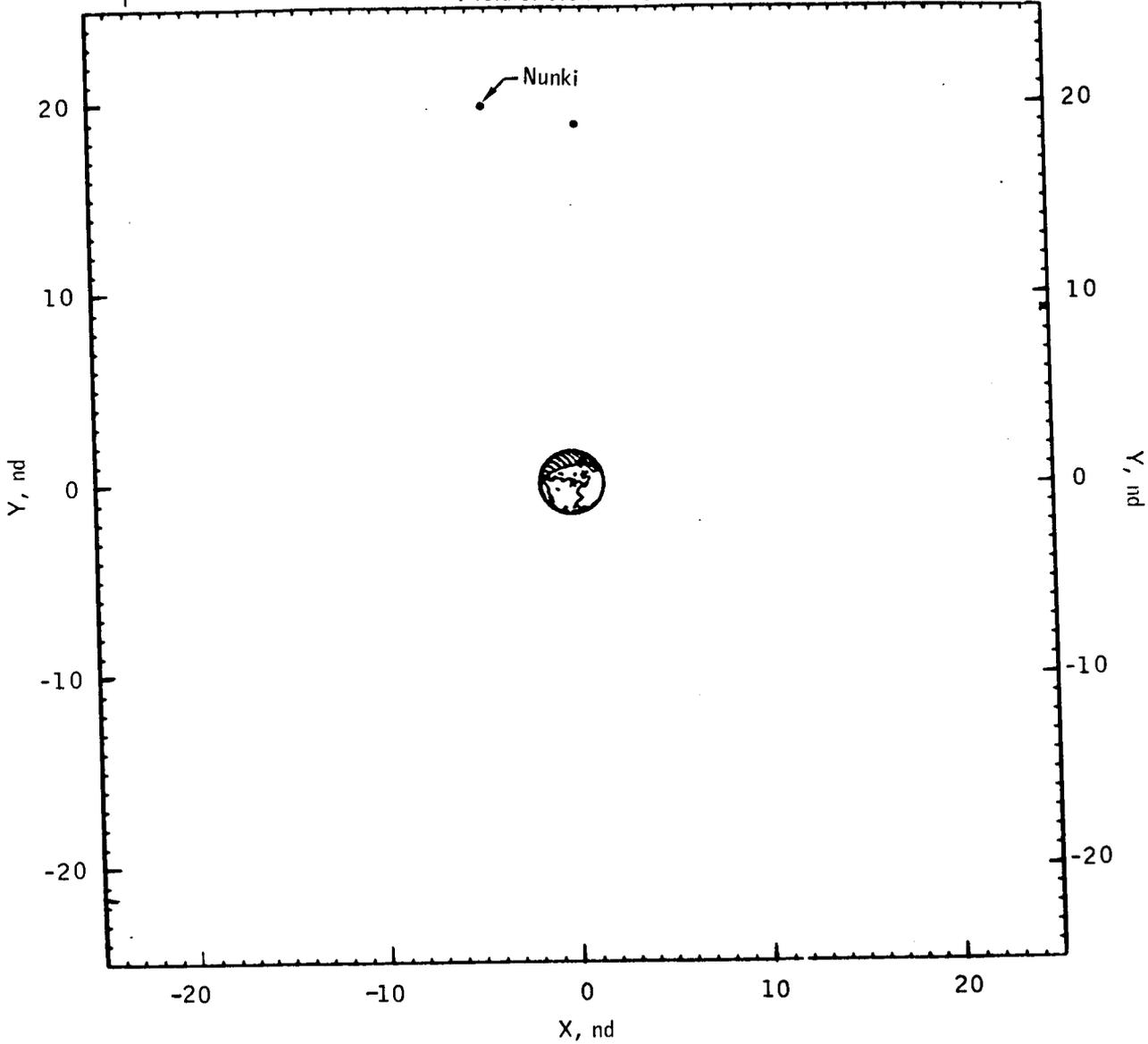
Figure 7.- Continued.

SEQ 061 071
 X -4 0
 Y 19 18

$R_E = 149\,206$ n. mi.
 $V_i = 4067$ fps

$h_E = 167\,742$ stat. mi.
 $V_i = 2773$ mph

Field of view = 40°



(e) G.e.t. = 40 hours.

Figure 7.- Continued.

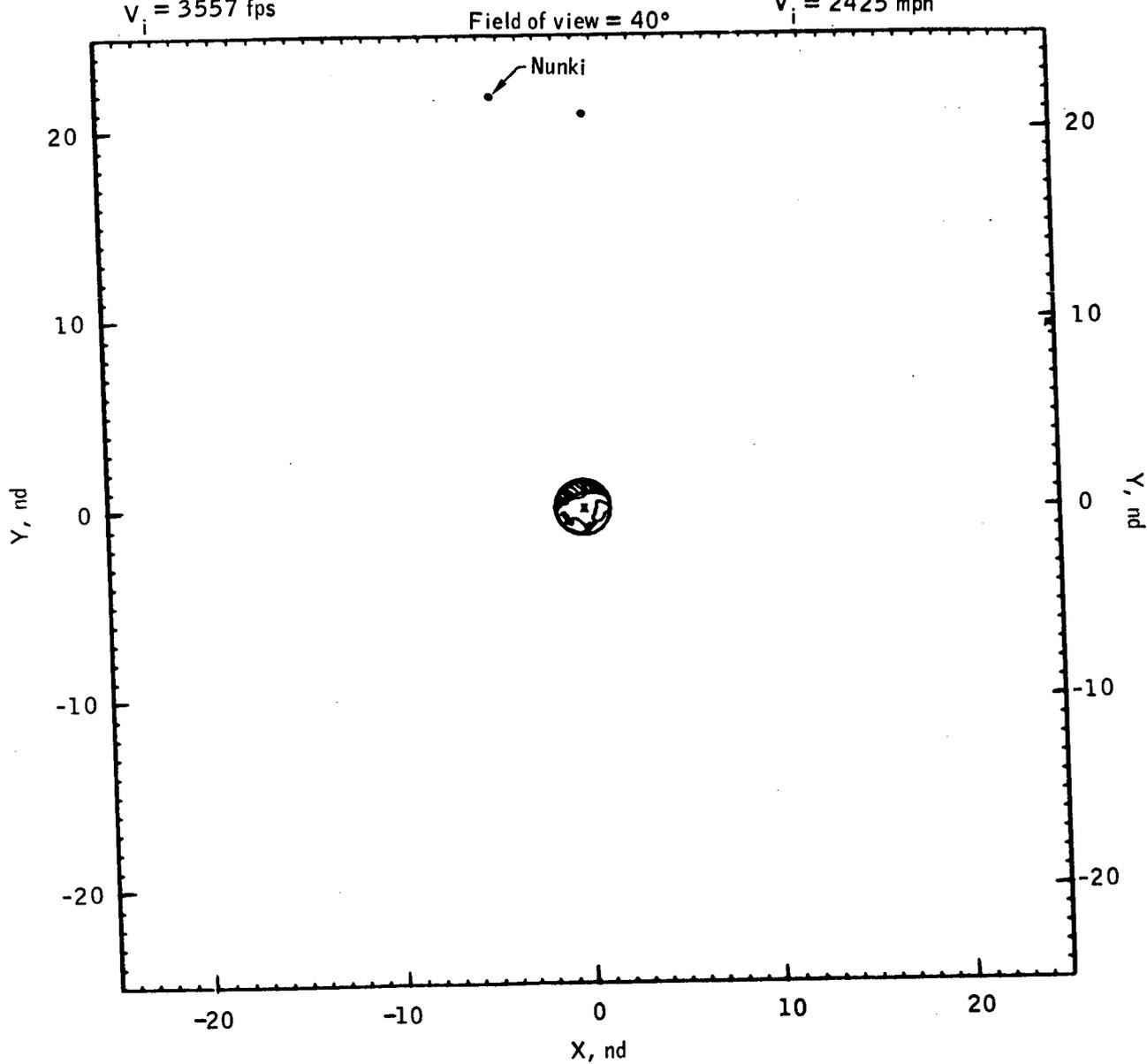
SEQ 061 071
 X 04 0
 Y 21 20

$R_E = 171\,265$ n. mi.

$V_i = 3557$ fps

$h_E = 193\,127$ stat. mi.

$V_i = 2425$ mph



(f) G.e.t. = 50 hours.

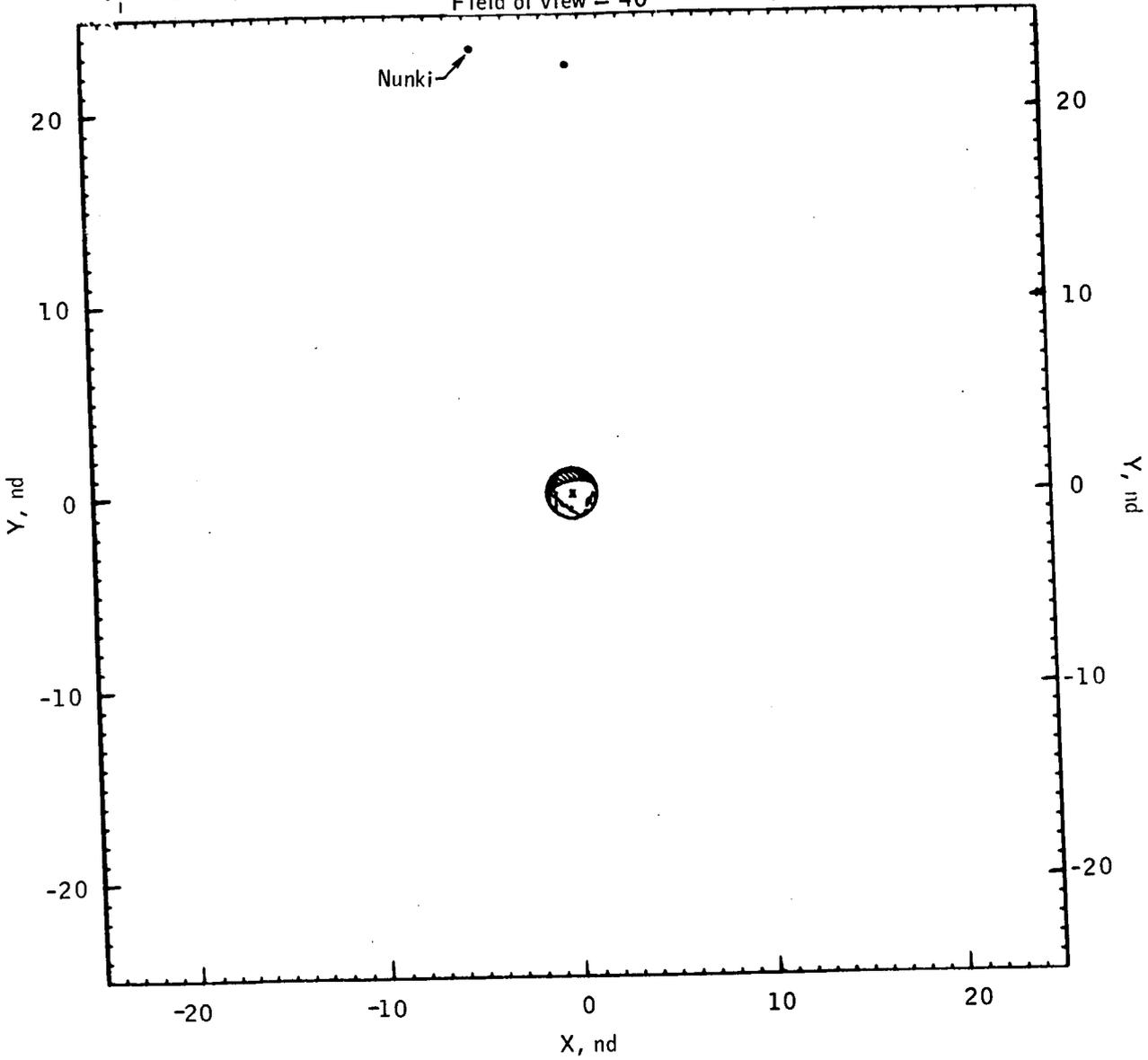
Figure 7.- Continued.

SEQ 861 871
 X -4 0
 Y 23 22

$R_E = 190\,809$ n. mi.
 $V_i = 3182$ fps

$h_E = 187\,368$ stat. mi.
 $V_i = 2170$ mph

Field of view = 40°



(g) G.e.t. = 60 hours.

Figure 7.- Continued.

SEQ	844	861	871	990
X	-22	-16	-12	16
Y	23	18	20	-21

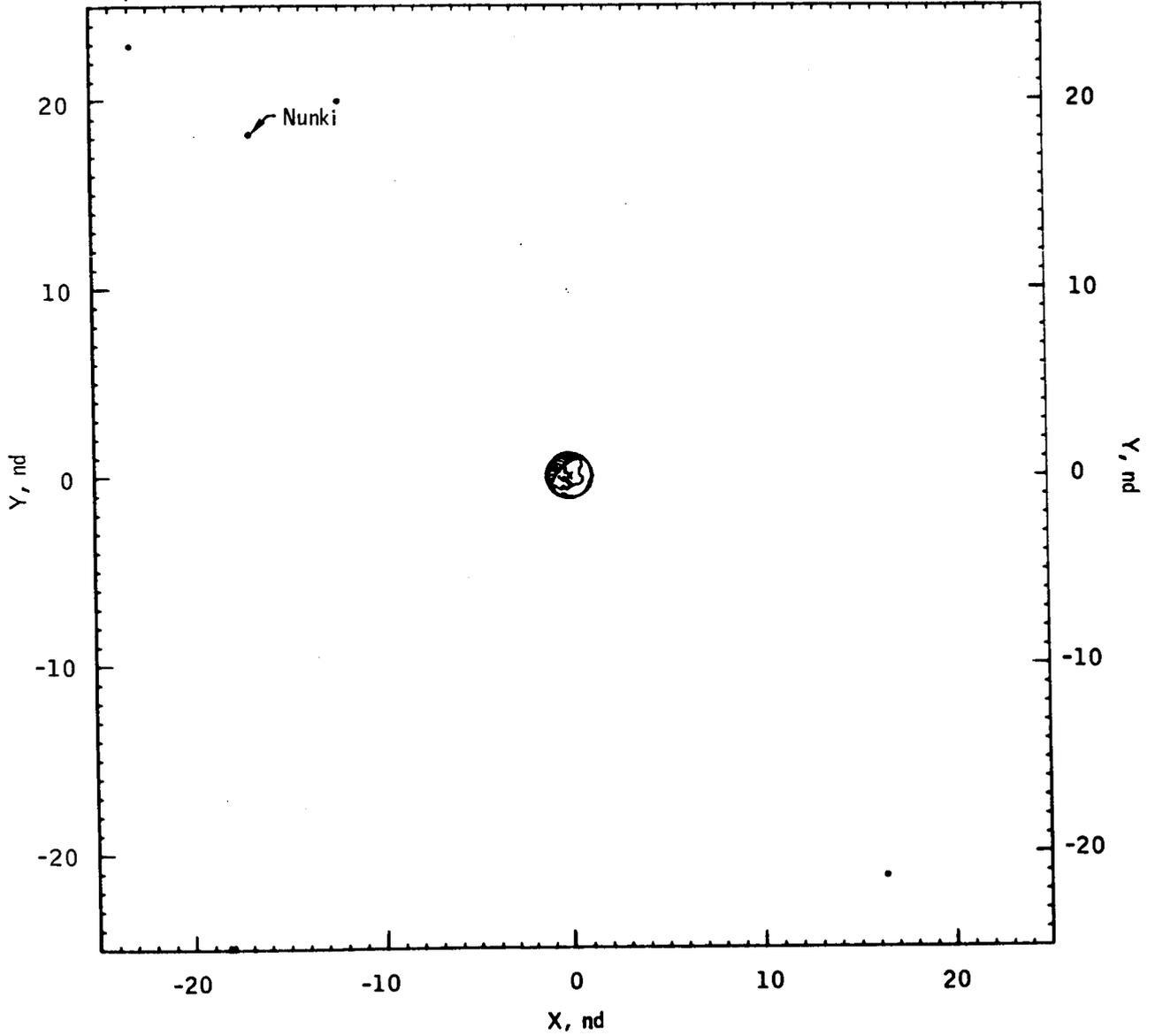
$R_M = 15\,709$ n. mi.

$V_i = 4031$ fps

$h_M = 16\,997$ stat. mi.

$V_i = 2748$ mph

Field of view = 40°



(h) G.e.t. = 70 hours.

Figure 7.- Concluded.

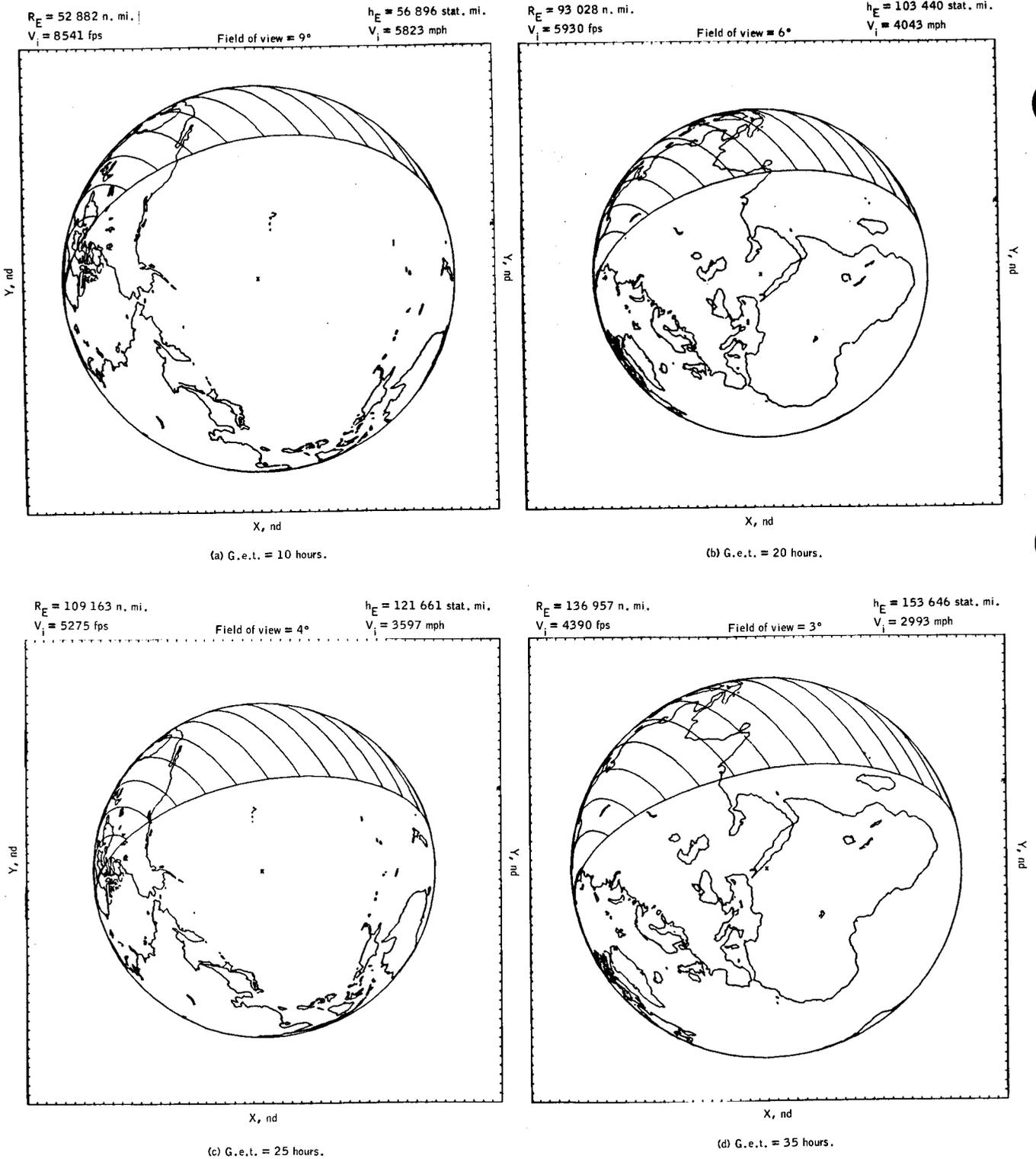
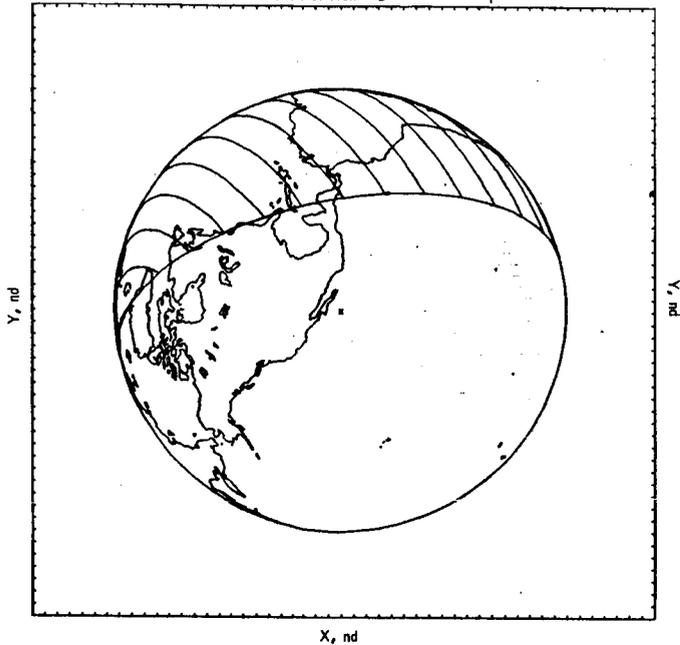


Figure 8.- Translunar coast - variable field of view (earth).

$R_E = 160\,600$ n. mi. $h_E = 180\,853$ stat. mi.
 $V_i = 3793$ fps $V_i = 2586$ mph
 Field of view = 3°

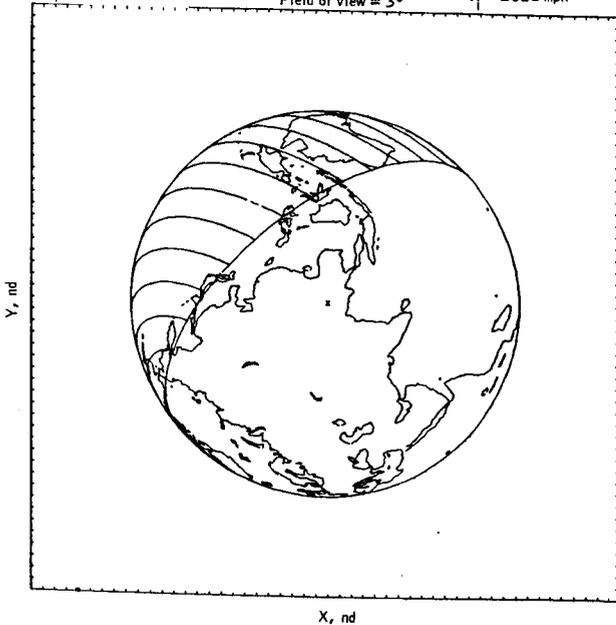


(e) G.e.t. = 45 hours.

$R_M = 27\,254$ n. mi.
 $V_i = 3844$ fps

Field of view = 3°

$h_M = 30\,284$ stat. mi.
 $V_i = 2621$ mph

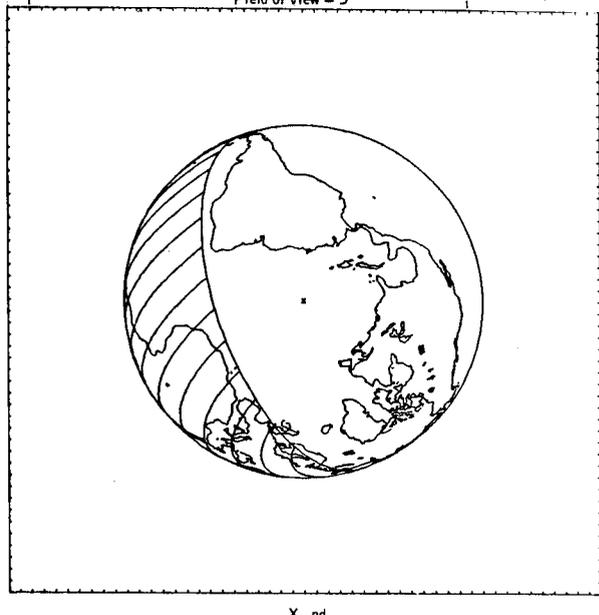


(f) G.e.t. = 65 hours.

$R_M = 3055$ n. mi.
 $V_i = 5591$ fps

Field of view = 3°

$h_M = 2436$ stat. mi.
 $V_i = 3821$ mph



(g) G.e.t. = 75 hours.

Figure 8.- Concluded.

MOON VIEWS

SEQ	150	186	205	207	222	230	231	248	265	270	271	281	301
X	21	0	11	20	21	-20	2	-7	-24	14	6	-11	-21
Y	-17	-21	-3	5	9	-17	-1	-3	-9	17	12	6	8

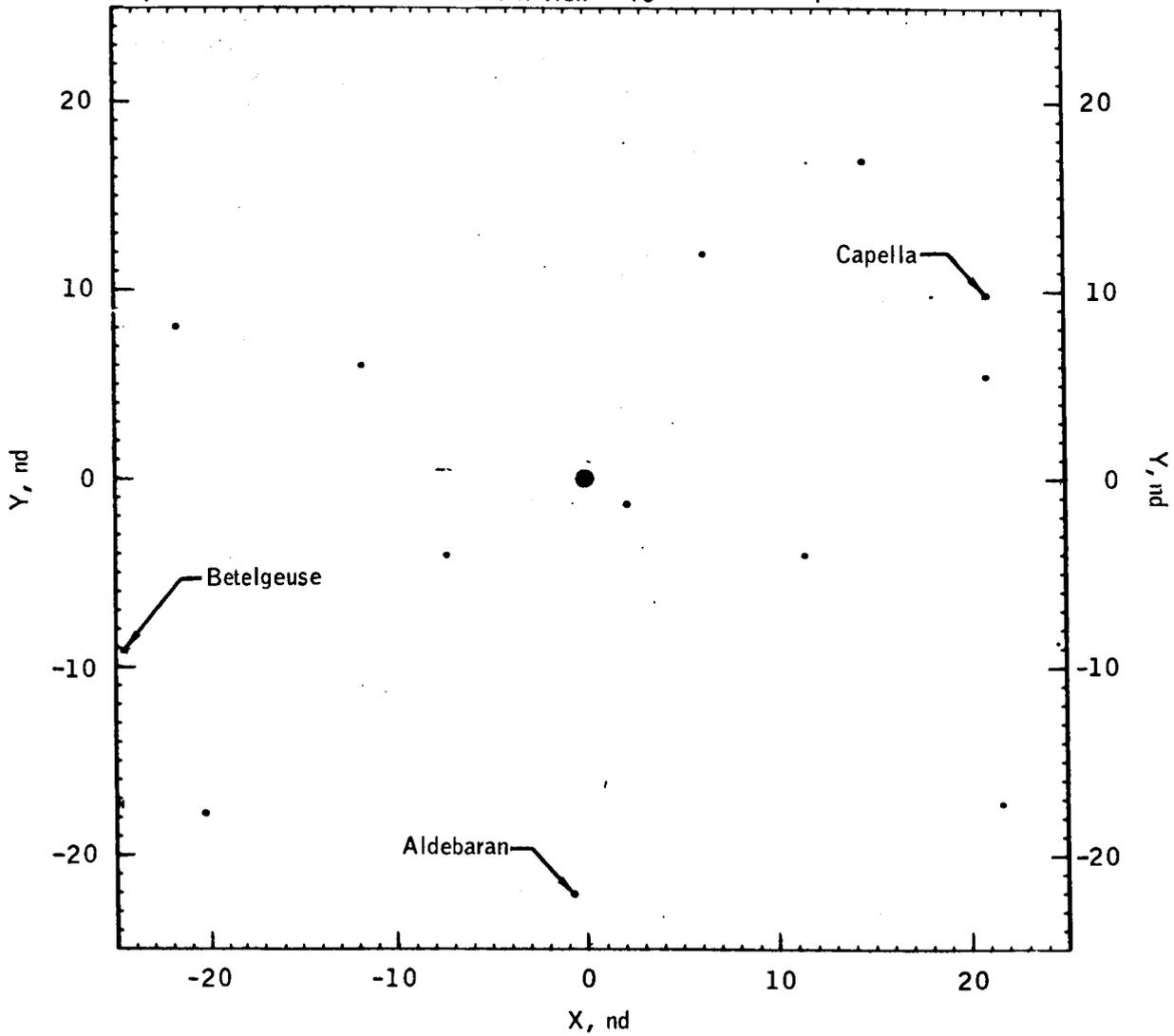
$R_E = 52\,882$ n. mi.

$h_E = 56\,896$ stat. mi.

$V_i = 8541$ fps

Field of view = 40°

$V_i = 5823$ mph



(a) G.e.t. = 10 hours.

Figure 9.- Translunar coast-constant field of view (moon).

SEQ	144	150	186	205	207	222	230	231	240	270	271	281	301
X	16	21	0	9	17	17	-20	0	-9	10	2	-14	-24
Y	-20	-11	-18	0	11	15	-17	2	-1	21	15	7	6

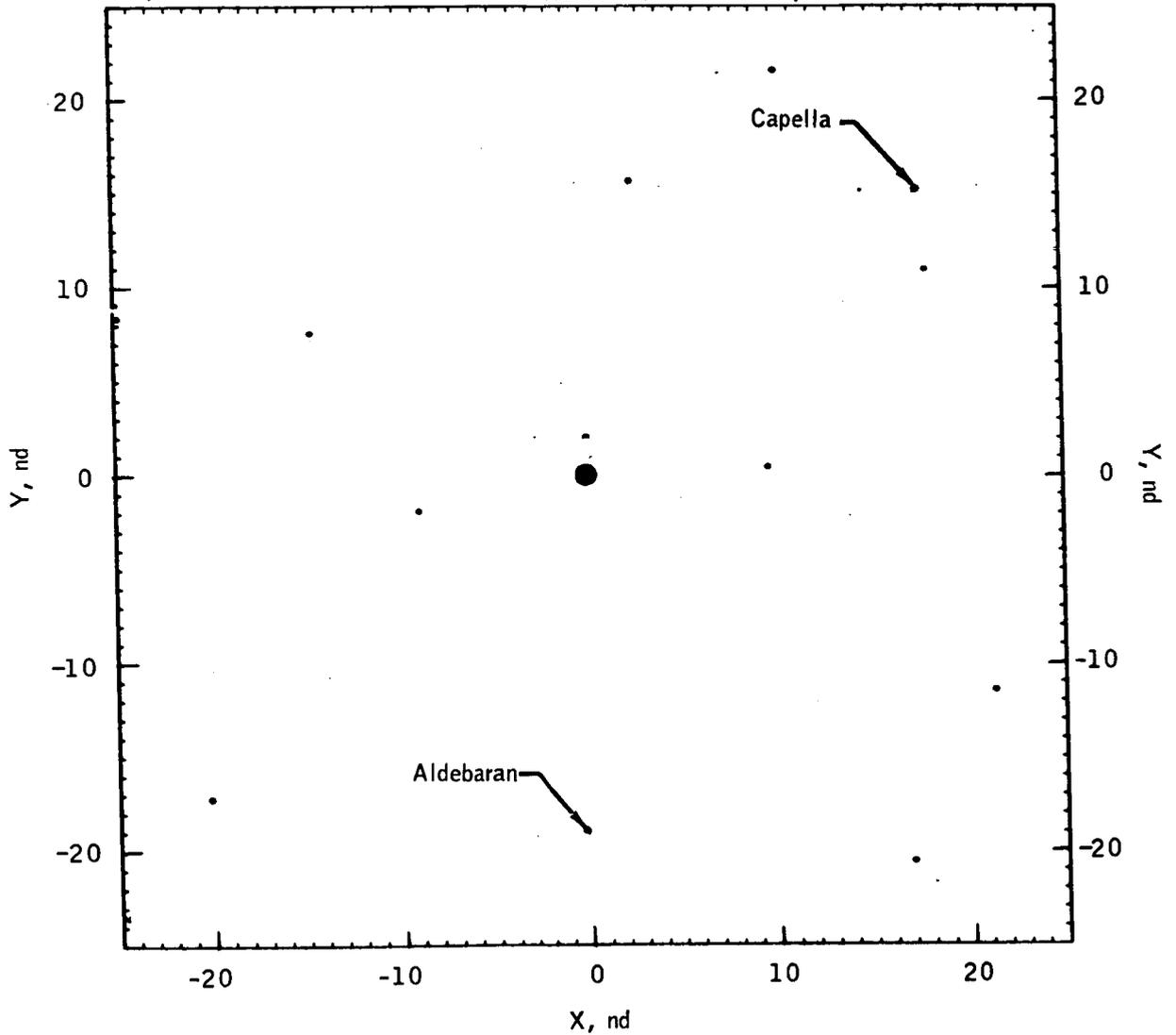
$R_E = 93\,028$ n. mi.

$h_E = 103\,440$ stat. mi.

$V_i = 5930$ fps

Field of view = 40°

$V_i = 4043$ mph



(b) G.e.t. = 20 hours.

Figure 9.- Continued.

SEQ	144	150	151	184	205	207	222	230	231	248	270	271	281
X	16	20	24	0	7	15	14	-20	-2	-10	6	0	-17
Y	-16	-7	1	-16	3	14	18	-16	4	0	24	18	8

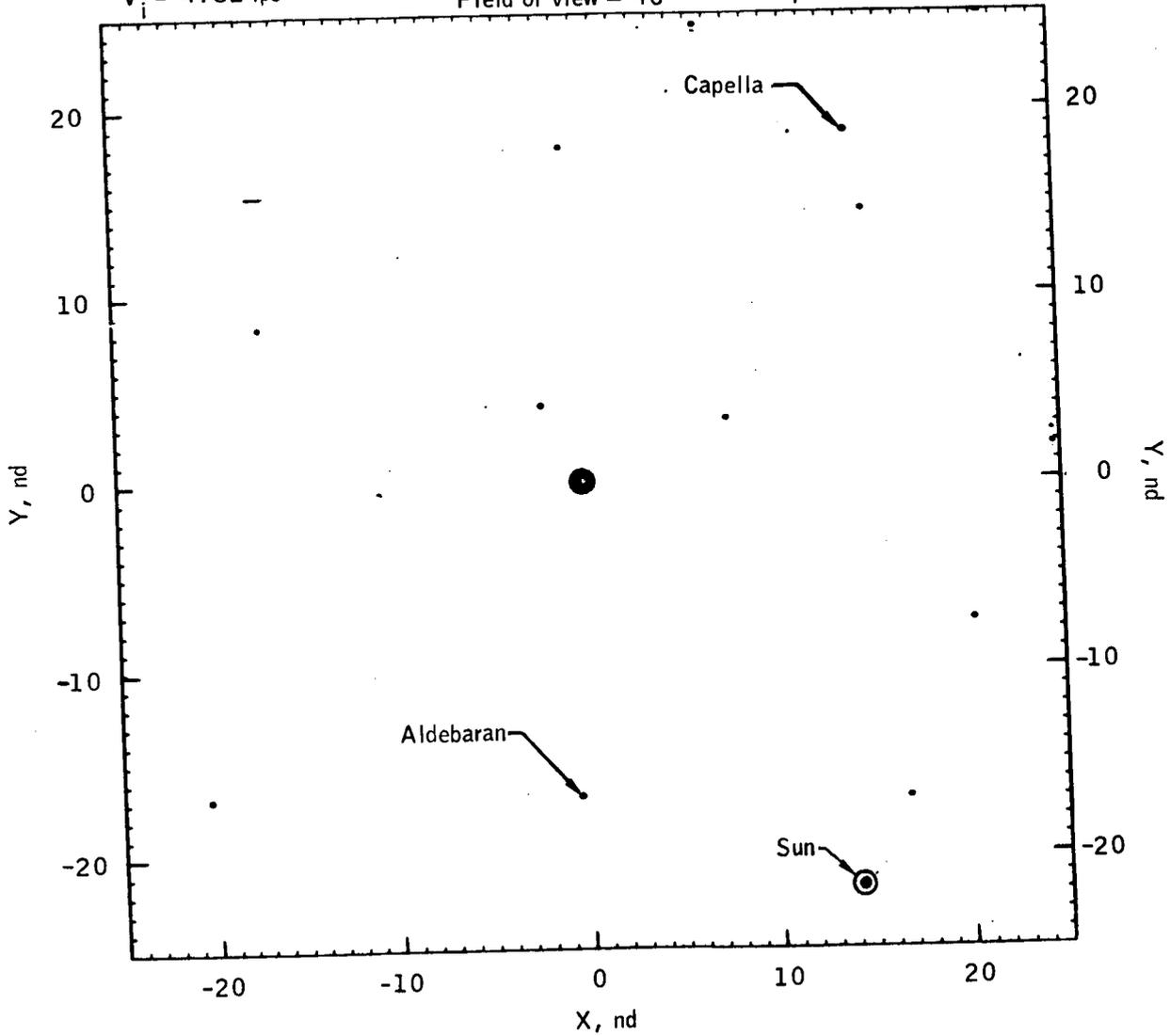
$R_E = 123\,687$ n. mi.

$V_i = 4782$ fps

Field of view = 40°

$h_E = 138\,375$ stat. mi.

$V_i = 3260$ mph



(c) G.e.t. = 30 hours.

Figure 9.- Continued.

SEQ	144	150	151	186	205	207	222	230	231	248	270	271	281
X	16	20	24	0	7	15	14	-20	-2	-10	6	0	-17
Y	-16	-7	1	-16	3	14	18	-16	4	0	24	18	0

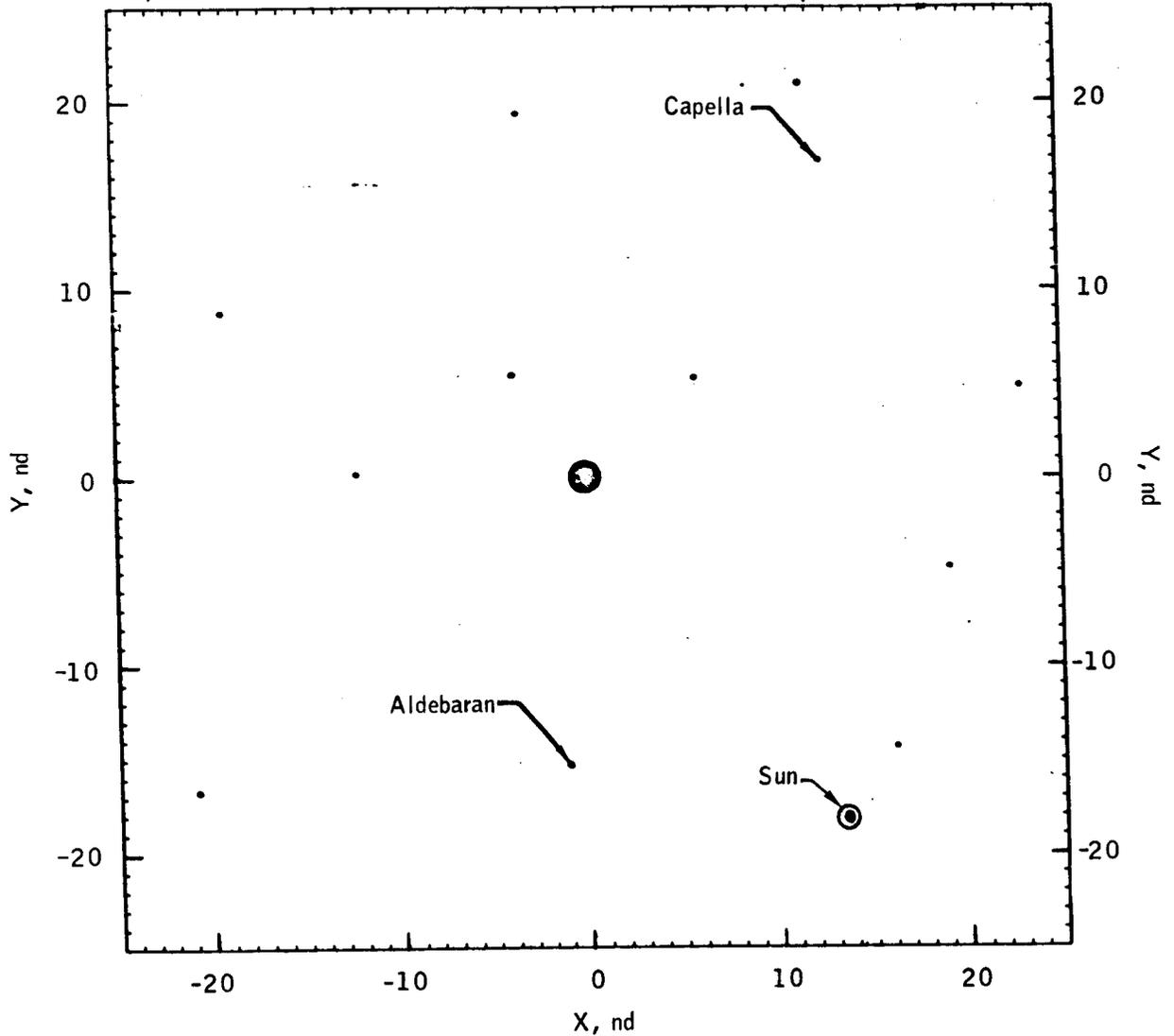
$R_E = 149\,206$ n. mi.

$h_E = 167\,742$ stat. mi.

$V_i = 4067$ fps

Field of view = 40°

$V_i = 2773$ mph



(d) G.e.t. = 40 hours.

Figure 9.- Continued.

SEQ	144	150	151	186	205	207	222	230	231	248	271	281
X	15	17	21	-1	4	10	9	-21	-5	-13	-5	-21
Y	-12	-2	6	-13	6	18	22	-16	6	1	20	9

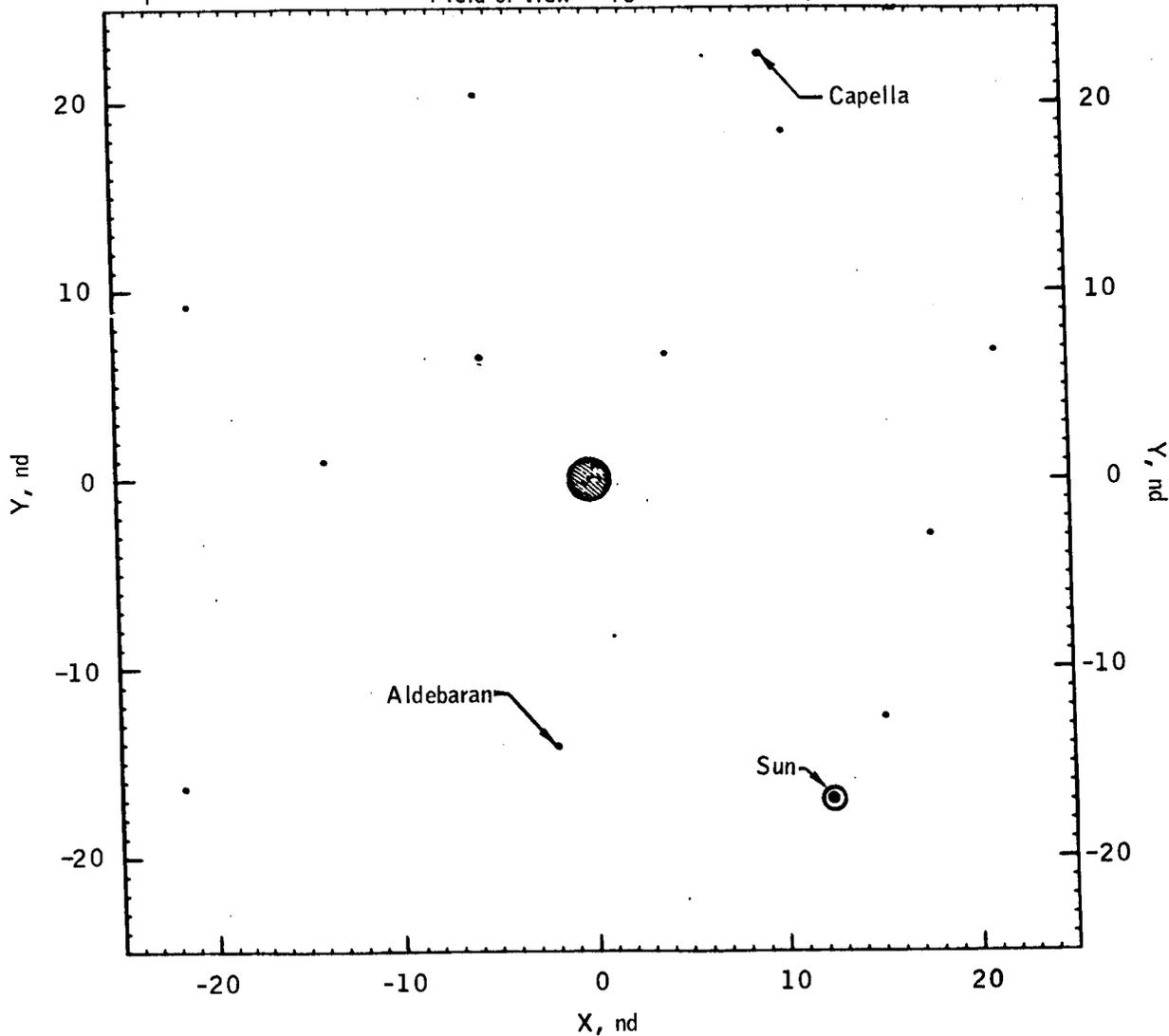
$R_E = 171\,265$ n. mi.

$h_E = 193\,127$ stat. mi.

$V_i = 3557$ fps

$V_i = 2425$ mph

Field of view = 40°



(e) G.e.t. = 50 hours.

Figure 9.- Continued.

STW	144	150	151	186	205	207	222	230	231	248	271	281
X	15	17	21	-1	4	10	9	-21	-5	-13	-5	-21
Y	-12	-2	6	-13	6	18	22	-16	6	1	20	9

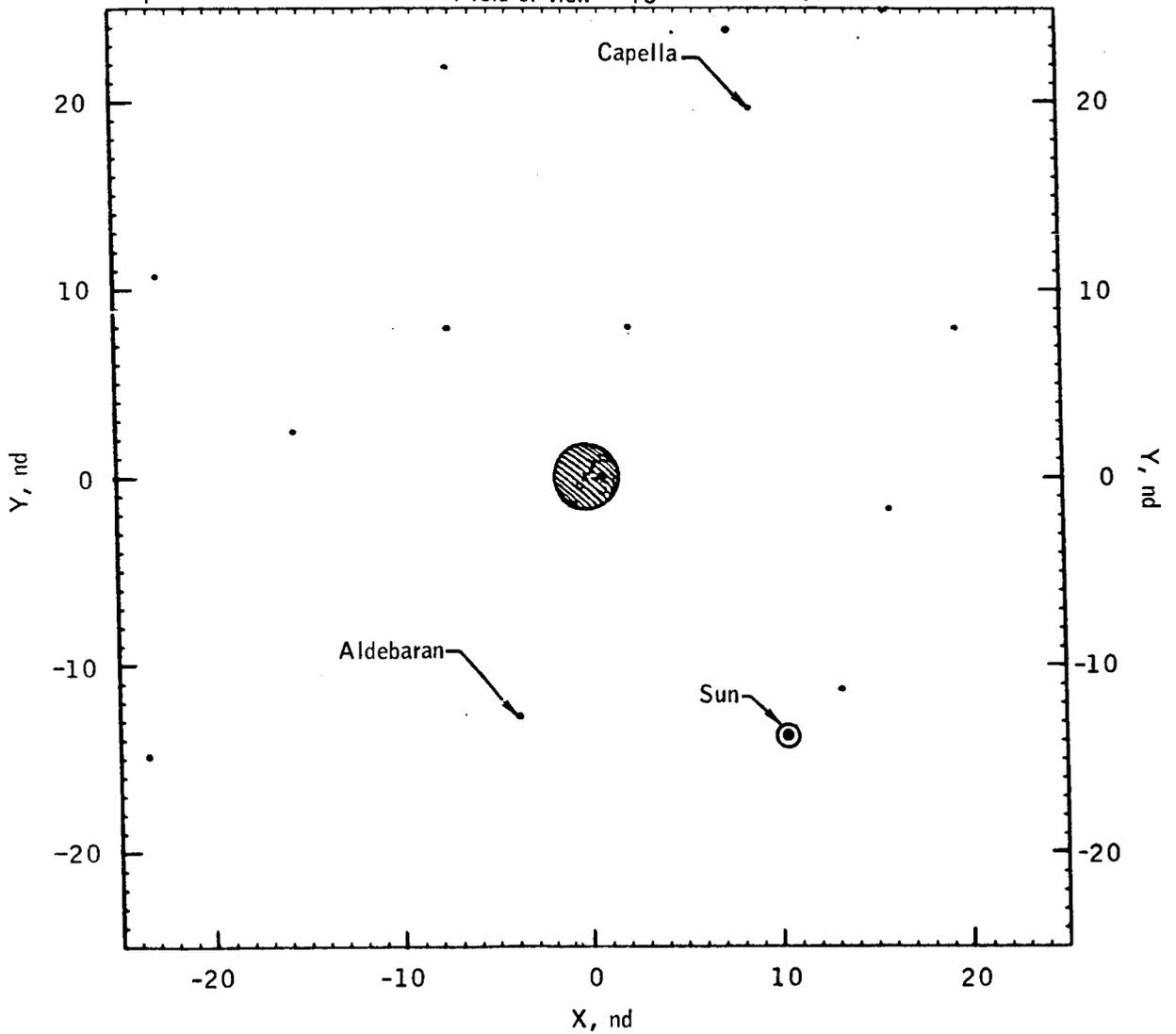
$R_E = 190\,809$ n. mi.

$h_E = 215\,619$ stat. mi.

$V_i = 3182$ fps

$V_i = 2170$ mph

Field of view = 40°



(f) G.e.t. = 60 hours.

Figure 9.- Continued.

SEC	111	112	144	150	151	186	205	207	222	231	248	270	271
X	18	21	-1	7	17	12	7	21	24	2	-7	23	13
Y	-18	-16	-11	-7	-5	2	8	10	13	16	20	22	24

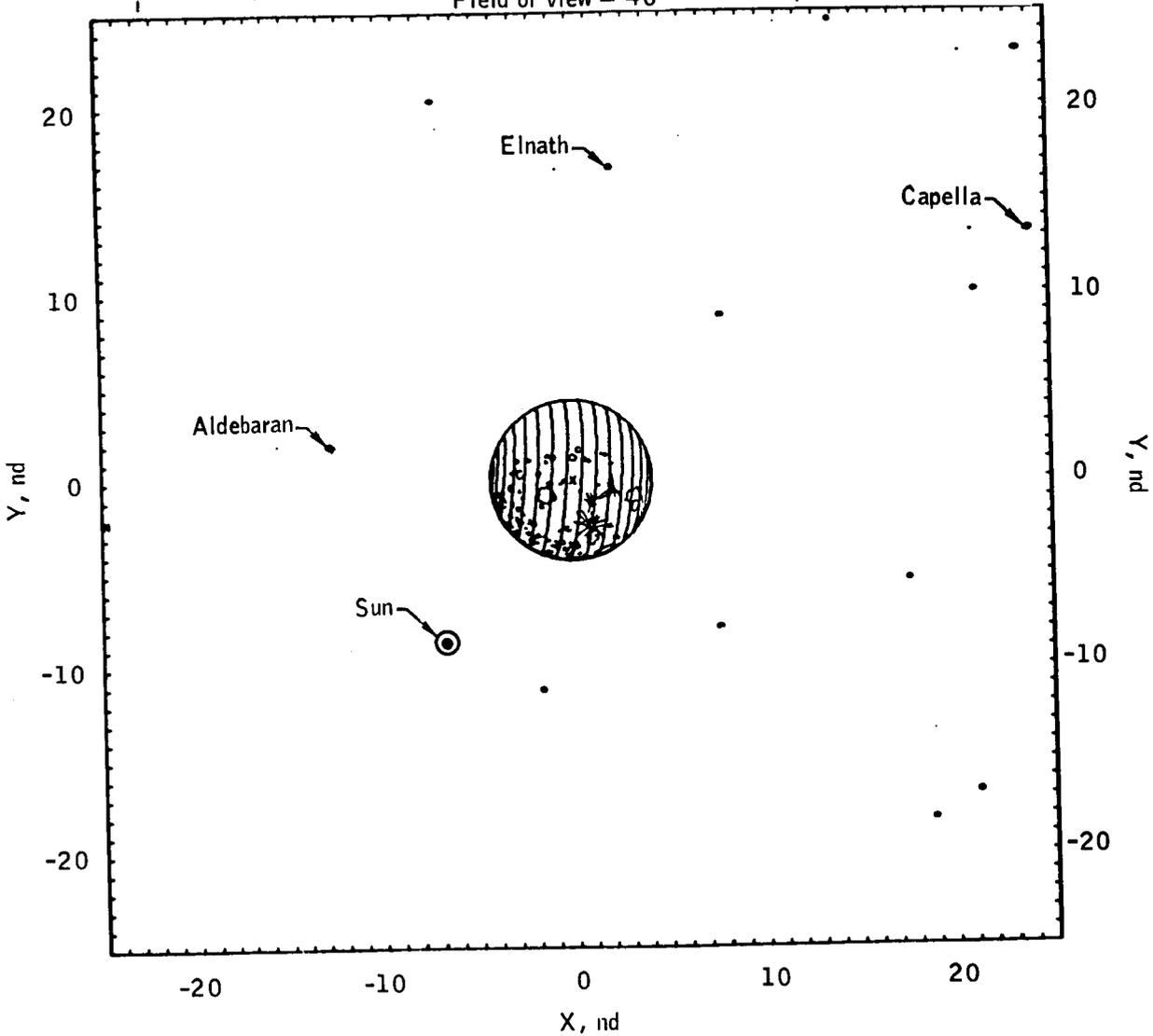
$R_M = 15\,709$ n. mi.

$V_i = 4031$ fps

$h_M = 16\,997$ stat. mi.

$V_i = 2748$ mph

Field of view = 40°



(g) G.e.t. = 70 hours.

Figure 9. - Concluded.

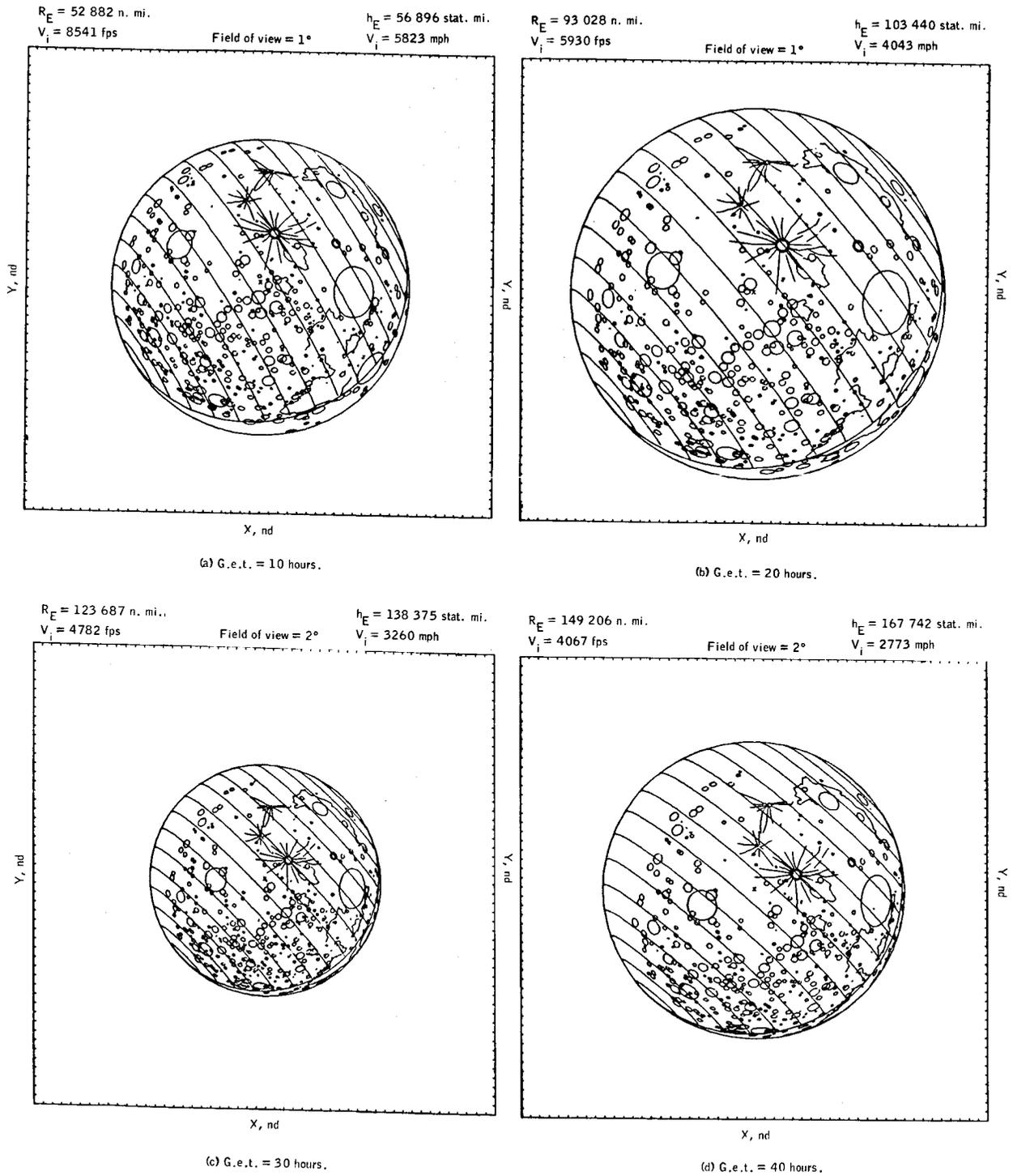
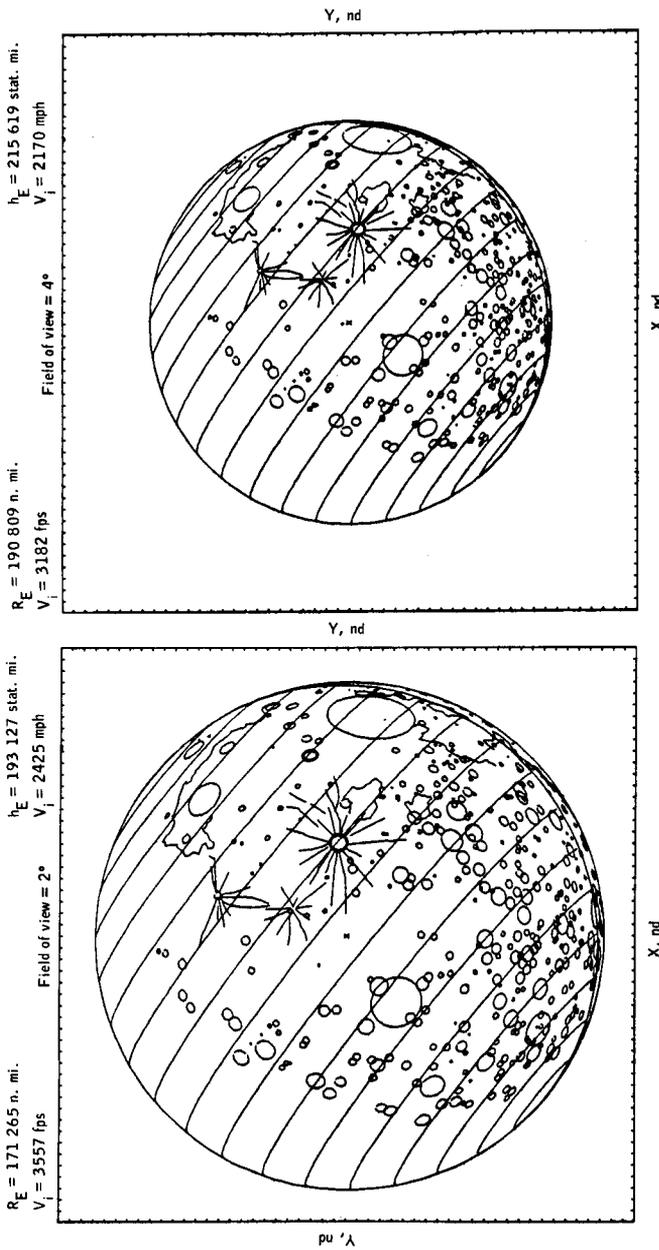


Figure 10.- Trans lunar coast - variable field of view (moon).



(f) G.e.t. = 60 hours.

Figure 10. - Concluded.

(e) G.e.t. = 50 hours.

LUNAR ORBIT
INSERTION BURN

SEQ	535	551	569	580	589	599	610	639	641	645	651
X	0	-10	-23	19	-16	-23	11	22	-16	-18	17
Y	-20	-11	0	-19	0	4	-5	-4	7	8	-1

SEQ	660	688	690	736	743	745	751	755	759
X	-16	-14	19	-5	-5	18	-6	24	-9
Y	10	13	4	17	18	11	19	10	20

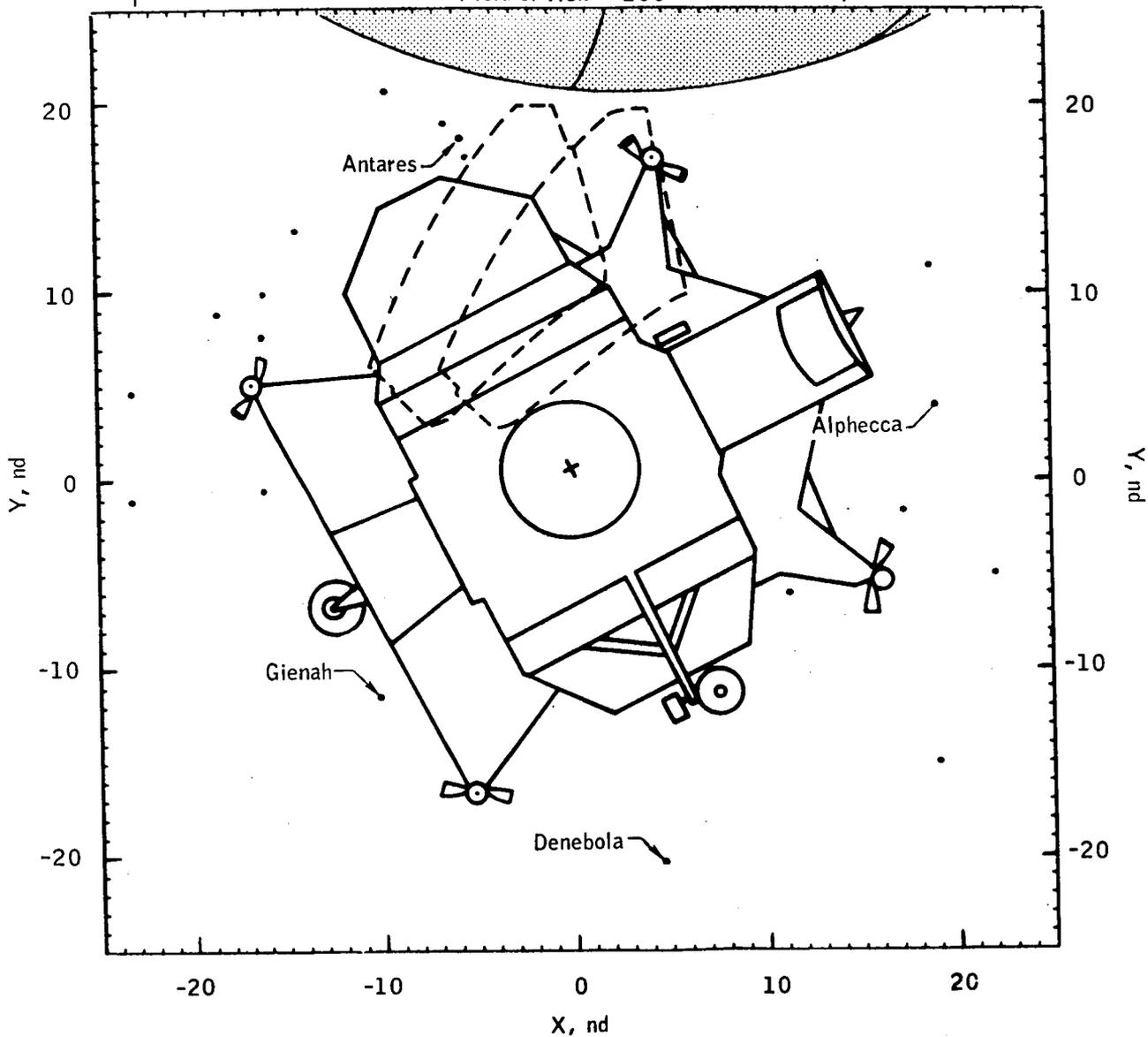
$R_M = 1028$ n. mi.

$V_i = 8251$ fps

$h_M = 102$ stat. mi.

$V_i = 5626$ mph

Field of view = 100°



(a) Begin LOI (g.e.t. = 75:45:43.2).

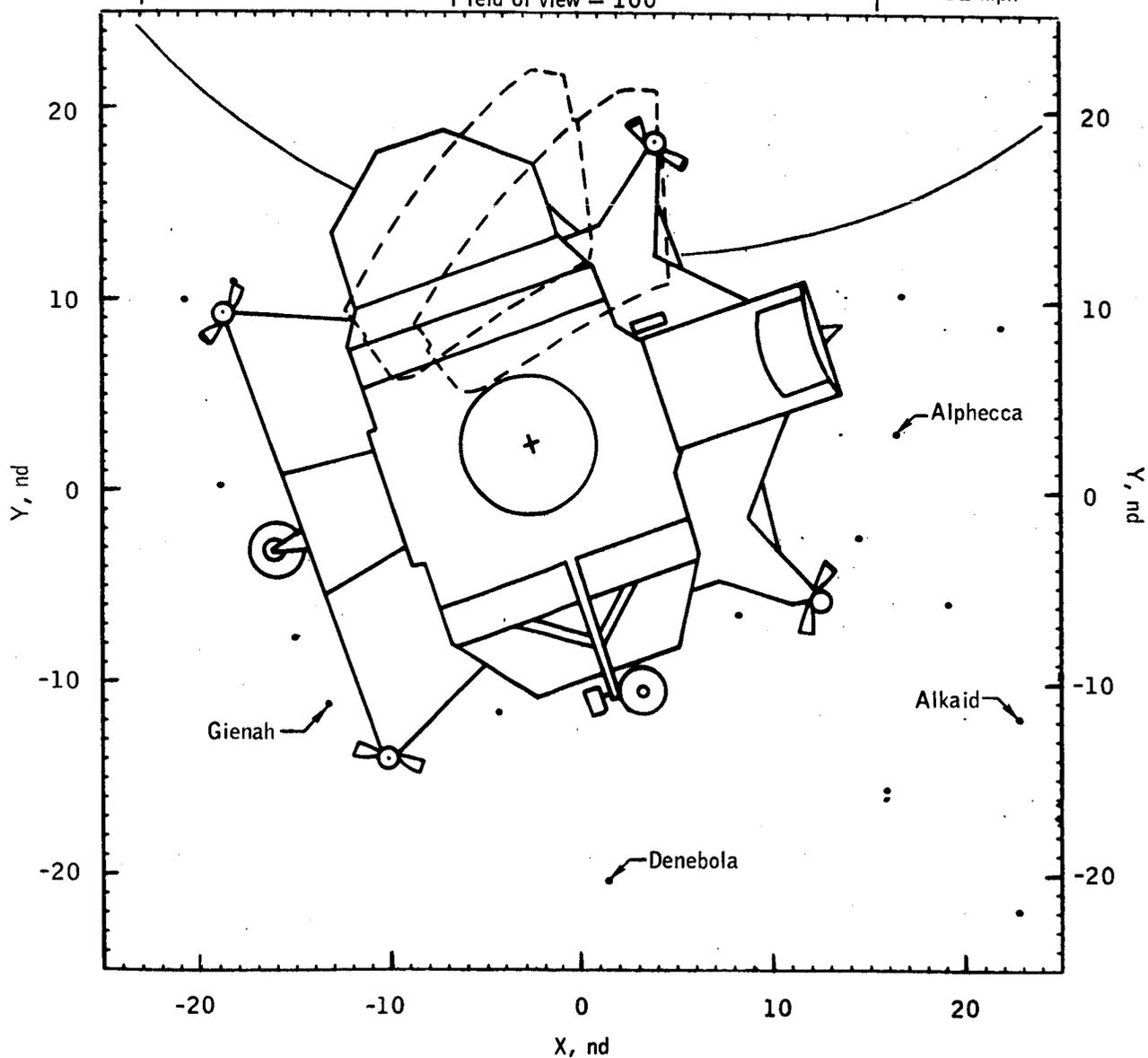
Figure 11.- Lunar orbit insertion burn.

SEG	535	540	551	566	570	577	580	589	604
X	1	22	-13	-14	-4	24	15	-18	-22
Y	-20	-21	-10	-7	-11	-16	-15	0	-11

SEG	610	639	645	651	660	695	745	789
X	8	19	-20	14	-18	16	18	21
Y	-6	-5	10	-2	11	3	18	8

 $R_M = 1001 \text{ n. mi.}$
 $V_i = 7013 \text{ fps}$
 $h_M = 71 \text{ stat. mi.}$
 $V_i = 4782 \text{ mph}$

Field of view = 100°



(b) Middle of LOI (g.e.t. = 75:48:43.2).

SEQ	535	540	551	566	577	580	582	589	592	595	604	621	639	690
X	-2	18	-17	-19	20	11	-1	-22	20	-16	18	-20	14	12
Y	-20	-22	-10	-6	-17	-15	-11	1	-15	0	-12	5	-6	2

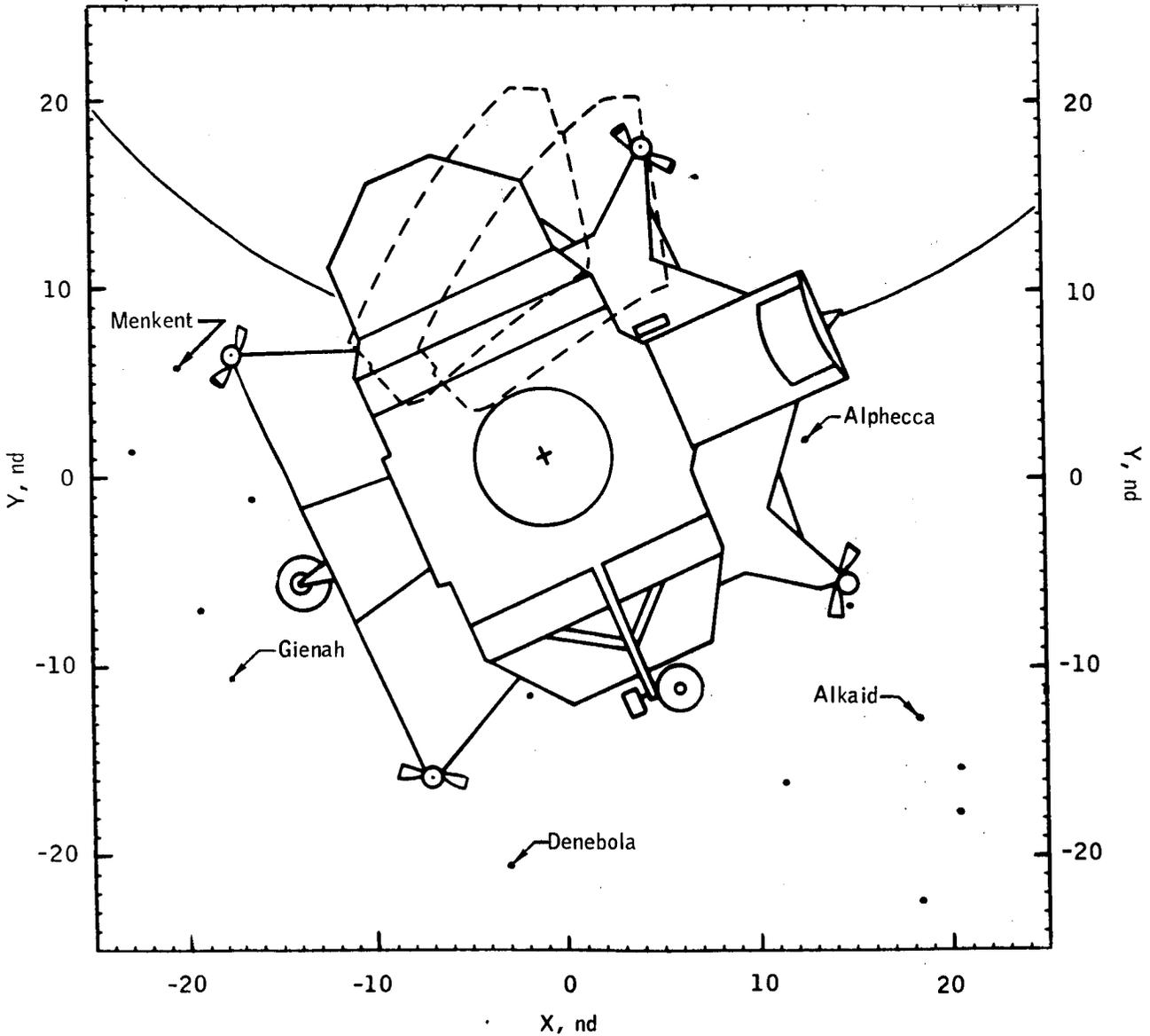
$R_M = 997$ n. mi.

$V_i = 5485$ fps

Field of view = 100°

$h_M = 67$ stat. mi.

$V_i = 3740$ mph



(c) End of LOI (g.e.t. = 75:51:44.7).

Figure 11.- Concluded.

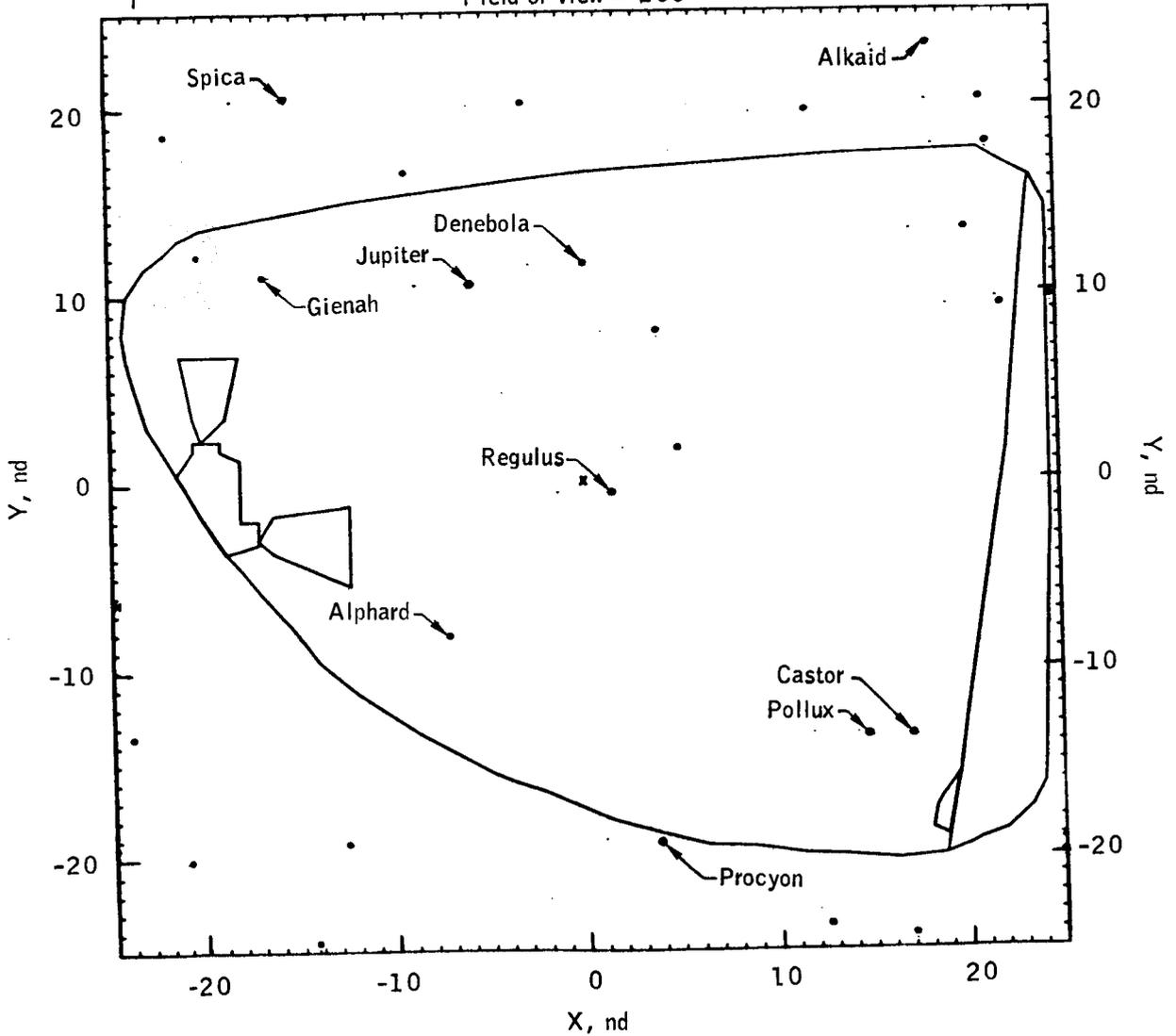
LUNAR ORBIT PHASE

SEQ	271	281	301	342	349	356	362	376	377	381	427	440	473	480
X	24	17	12	-14	17	3	14	-20	-12	-24	-23	-7	1	5
Y	-19	-24	-23	-24	-13	-19	-13	-19	-19	-19	-13	28	0	1
SEQ	507	509	515	535	540	551	566	570	577	580	582	592	593	595
X	22	24	3	0	20	-16	-20	-9	21	11	-2	21	-15	-21
Y	9	9	8	11	13	11	12	16	18	19	20	20	20	18
SEQ	604	1081												
X	18	-5												
Y	23	10												

$R_M = 996$ n. mi.
 $V_i = 5349$ fps

$h_M = 67$ stat. mi.
 $V_i = 3647$ mph

Field of view = 100°



(a) Begin DOI burn - front window (g.e.t. = 99:33:51).

Figure 12.- Lunar orbit phase.

SEQ	545	561	566	569	574	589	593	595	599	610	617	621	624	641
X	-23	-24	-9	-21	-24	-13	0	-6	-20	16	-22	-11	17	-12
Y	-15	-11	-24	-14	-10	-16	-21	-18	-9	-21	-5	-12	-18	-8
SEQ	643	645	651	655	660	673	688	690	700	717	719	724	736	743
X	-21	-15	21	0	-12	4	-10	22	12	-2	-1	0	-2	-2
Y	-3	-6	-15	-11	-6	-8	-2	-9	-6	-2	-2	-2	0	1
SEQ	745	751	753	757	759	770	781	789	790	793	795	797	802	803
X	21	-3	5	-23	-6	3	-16	-7	-13	-7	17	-10	-8	13
Y	-2	2	1	4	3	5	7	8	7	8	6	8	9	8
SEQ	836	841	844	861	871	933	1000							
X	-3	-6	-1	-2	-4	-20	-1							
Y	13	13	14	17	17	19	3							

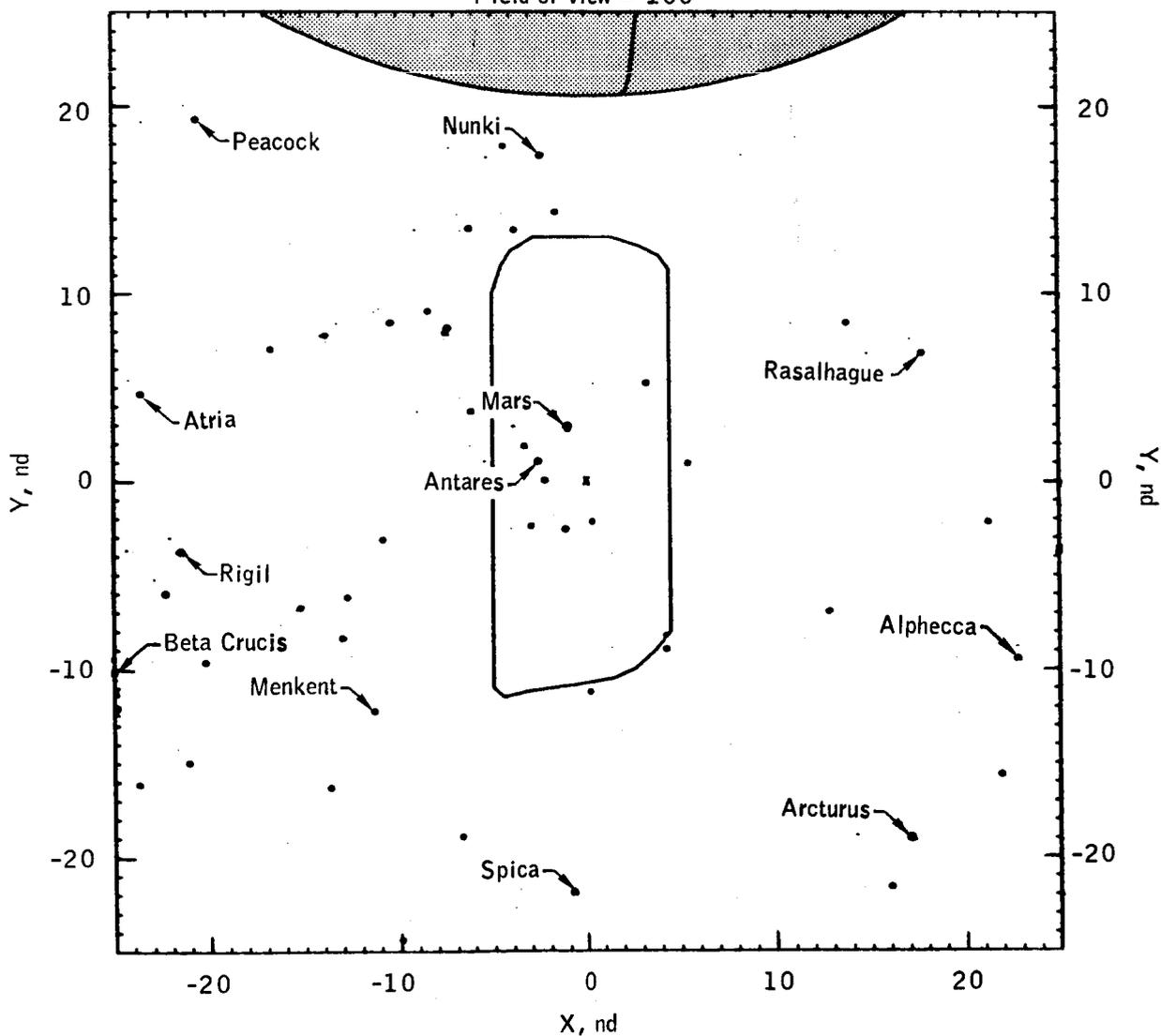
$R_M = 996$ n. mi.

$h_M = 67$ stat. mi.

$V_i = 5349$ fps

$V_i = 3647$ mph

Field of view = 100°



(b) Begin DOI burn - docking window (g.e.t. = 99:33:51).

SEQ	271	271	301	342	349	356	362	376	377	381	427	440	473	480	507
X	24	17	12	14	17	13	14	-20	-12	-24	-23	-7	1	5	22
Y	-19	-24	-23	-24	-13	-19	-13	-19	-19	-19	-13	-8	0	1	9
SEQ	509	515	535	540	551	566	570	577	580	582	592	593	595	604	1081
X	24	3	0	20	-16	-20	-9	21	11	-2	21	-15	-21	18	5
Y	9	4	11	13	11	12	16	18	19	20	20	20	18	23	10

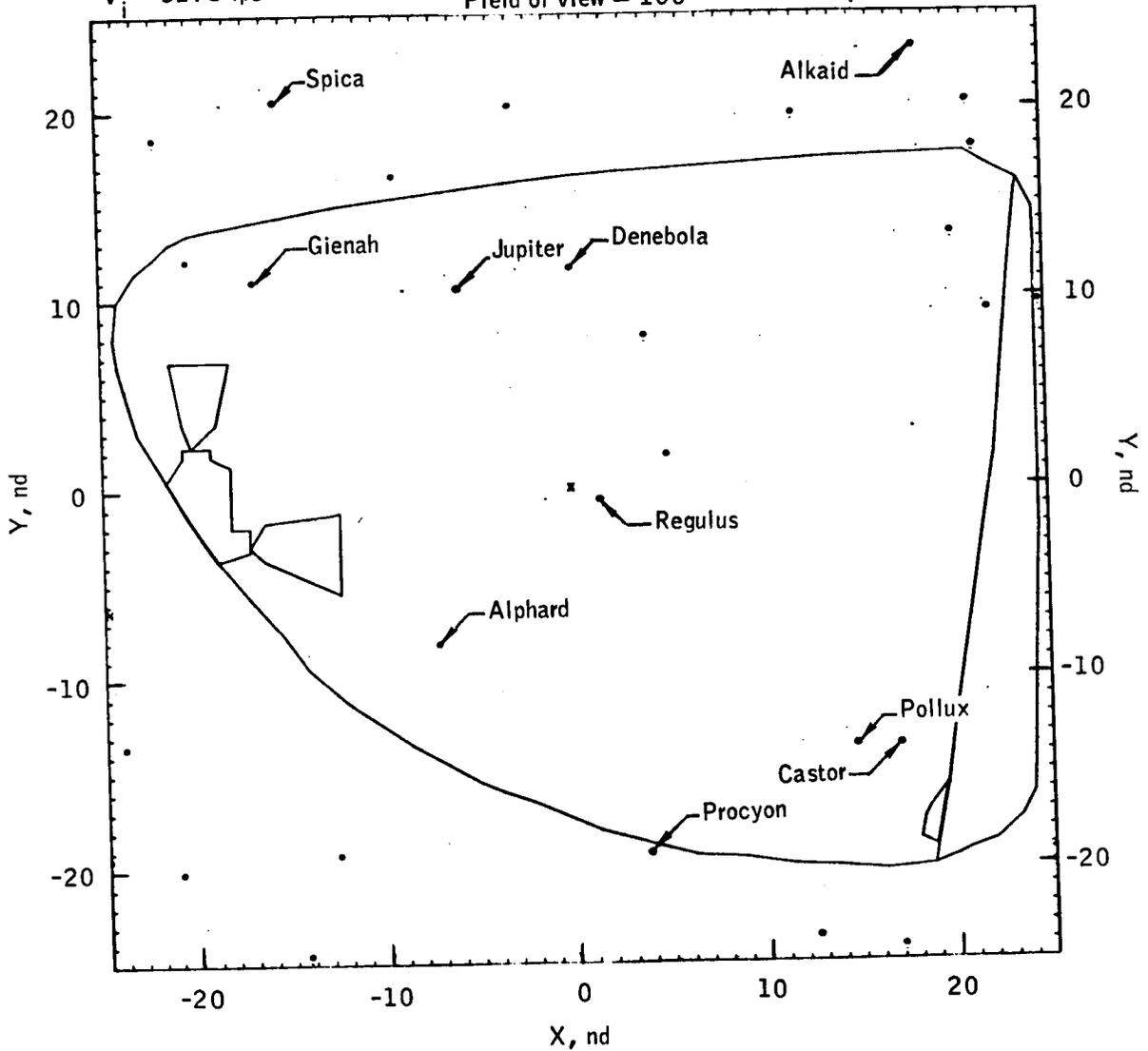
$R_M = 996$ n. mi.

$h_M = 67$ stat. mi.

$V_i = 5278$ fps

Field of view = 100°

$V_i = 3599$ mph



(c) End DOI burn - Front window (g.e.t. = 99:34:26).

Figure 12.- Continued.

SEQ	545	561	566	569	574	589	593	595	599	610	617	621	624	641	643
X	-23	-24	-9	-21	-24	-13	0	-6	-20	16	-22	-11	17	-12	-21
Y	-15	-11	-24	-14	-10	-16	-21	-18	-9	-21	-9	-12	-18	-8	-3
SEQ	645	651	655	660	673	688	690	700	717	719	724	736	743	745	751
X	-15	21	0	-12	4	-10	22	12	-2	-1	0	-2	2	21	-3
Y	-6	-15	-11	-6	-8	-2	-9	-6	-2	-2	-2	0	1	2	2
SEQ	753	757	759	770	781	789	790	793	795	797	802	803	836	841	844
X	5	-23	-6	3	-16	-7	-13	-7	17	-10	-8	13	-3	-6	-1
Y	1	4	3	5	7	8	7	8	6	8	9	8	13	13	14
SEQ	861	871	1080												
X	-2	-4	-1												
Y	17	17	3												

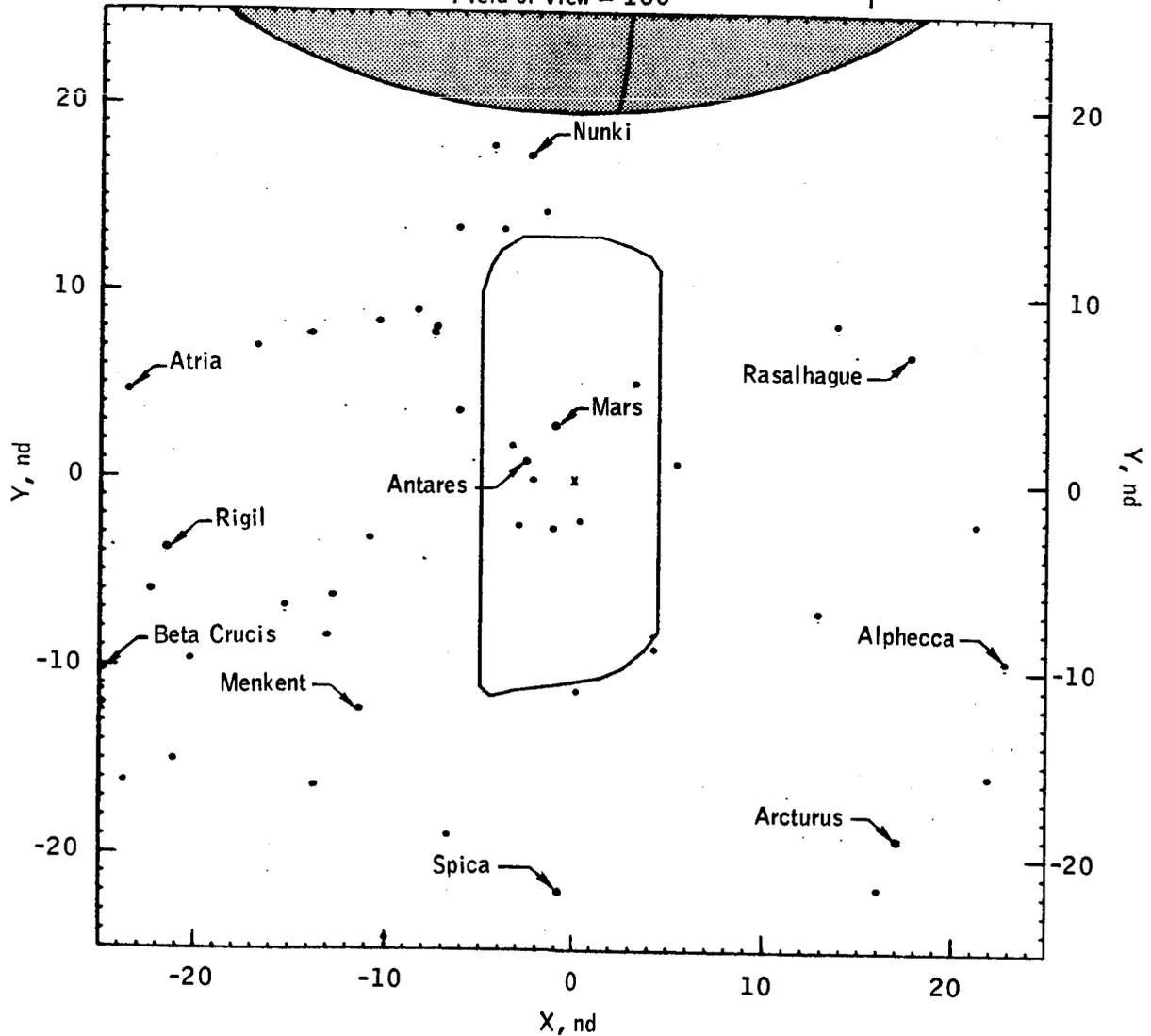
$R_M = 996$ n. mi.

$V_i = 5278$ fps

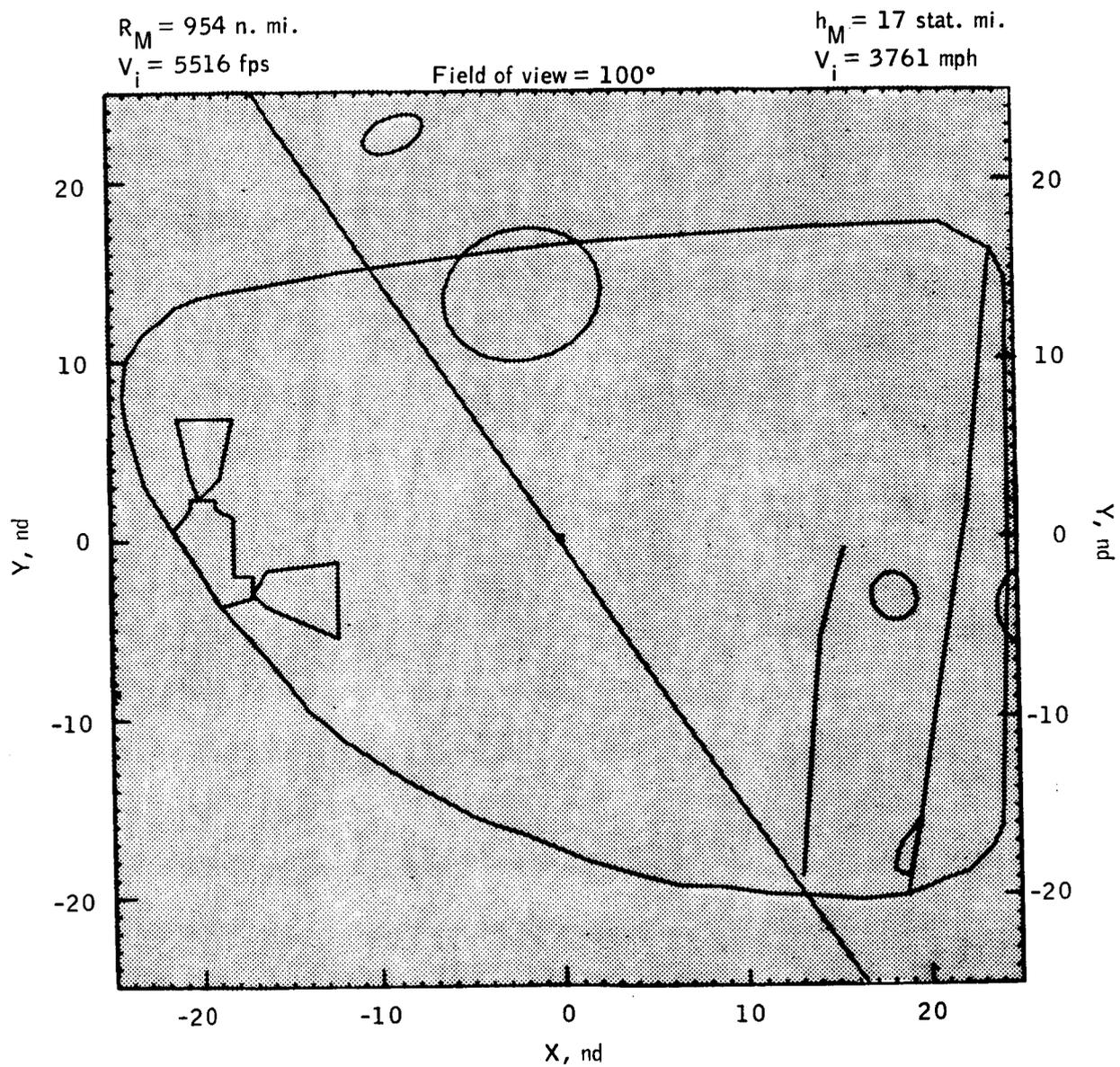
$h_M = 67$ stat. mi.

$V_i = 3599$ mph

Field of view = 100°



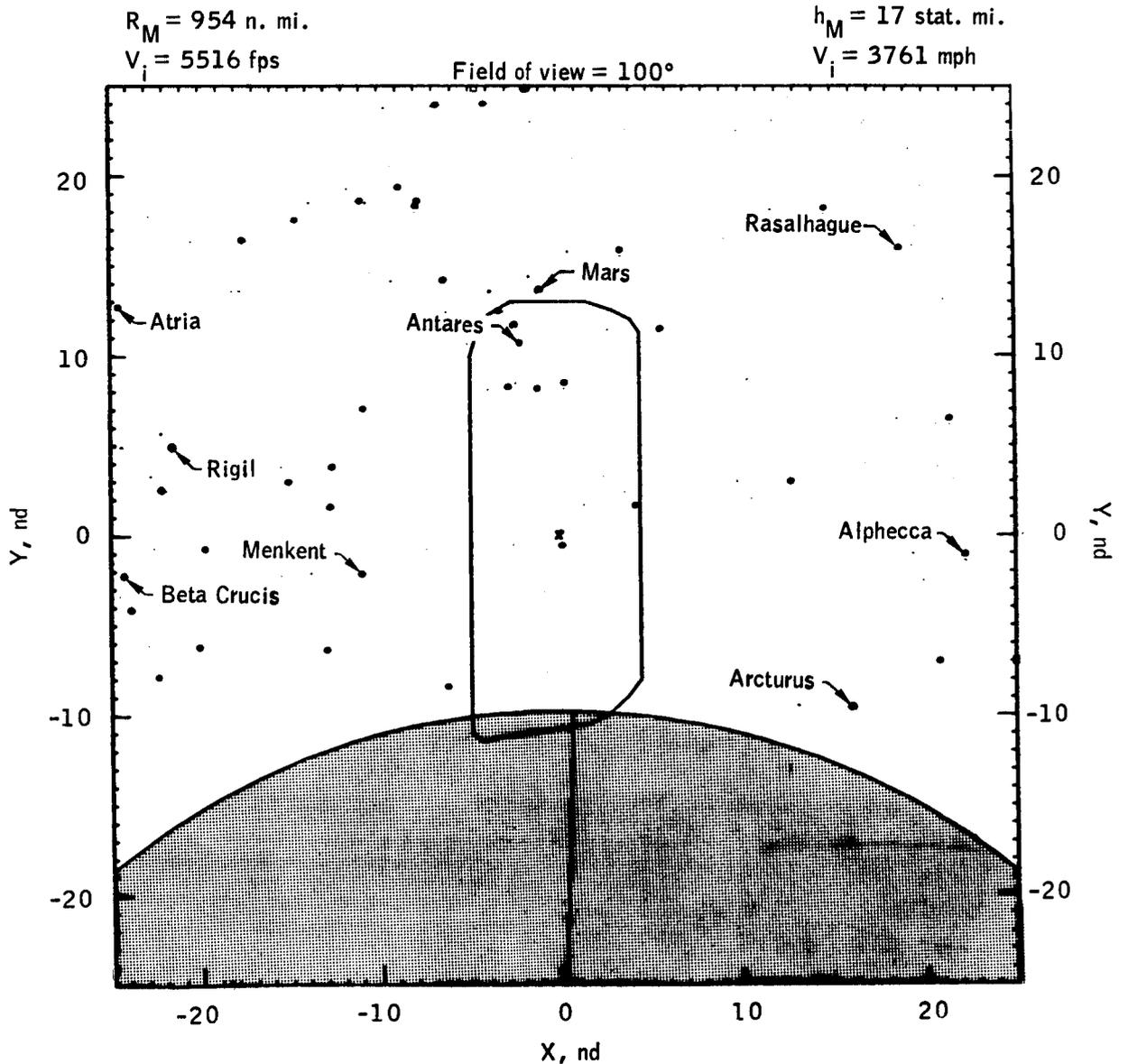
(d) End DOI burn - docking window (g.e.t. = 99:34:26).



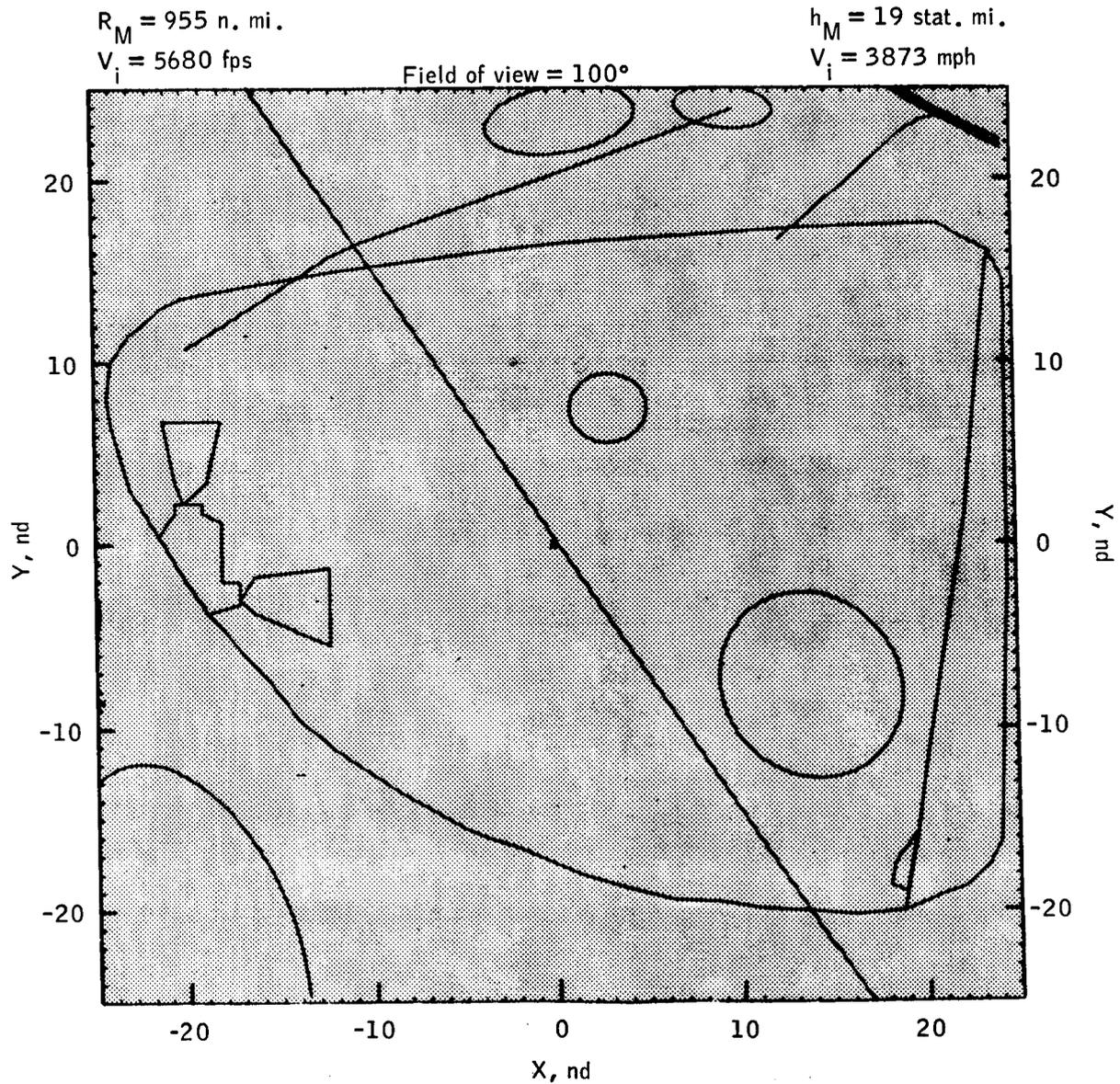
(e) Begin phasing burn - front window (g.e.t. = 100:64:21).

Figure 12.- Continued.

SEQ	545	561	569	574	589	595	599	617	621	624	641	643	645	651
X	-22	-23	-20	-24	-12	-6	-19	-22	-10	15	-12	-21	-15	20
Y	-7	-3	-6	-2	-6	-8	0	2	-1	-9	1	5	3	-6
SEQ	655	660	673	688	690	700	717	719	724	736	743	745	751	753
X	0	-12	4	-10	22	12	-2	-1	0	-2	-2	21	-3	5
Y	0	3	1	7	0	3	8	8	8	10	11	6	12	11
SEQ	757	759	770	781	789	790	793	795	797	802	803	836	841	844
X	-24	-6	3	-17	-7	-14	-7	18	-10	-8	14	-4	-6	-1
Y	12	14	16	16	18	17	18	16	18	19	18	24	24	25
SEQ	1080													
X	-1													
Y	13													



(f) Begin phasing burn - docking window (g.e.t. = 100:46:21).



(g) End phasing burn - front window (g.e.t. = 100:47:03).

Figure 12.- Continued.

SEQ	545	561	569	574	589	595	599	617	621	624	641	643	645
X	-22	-23	-20	-24	-12	-6	-19	-22	-10	15	-12	-21	-15
Y	7	-3	6	-2	6	-8	0	2	-1	-9	1	5	3
SEQ	651	655	660	673	688	690	700	717	719	724	736	743	745
X	20	0	-12	4	-10	22	12	-2	-1	0	-2	-2	21
Y	-6	0	3	1	7	0	3	8	8	8	11	11	6
SEQ	751	753	757	759	770	781	786	790	793	795	797	802	803
X	-3	5	-24	-6	3	-17	-7	-14	-7	18	-10	-8	14
Y	12	11	12	14	16	16	18	17	18	16	18	19	18
SEQ	836	841	844	1080									
X	-4	-6	-1	-1									
Y	24	24	25	13									

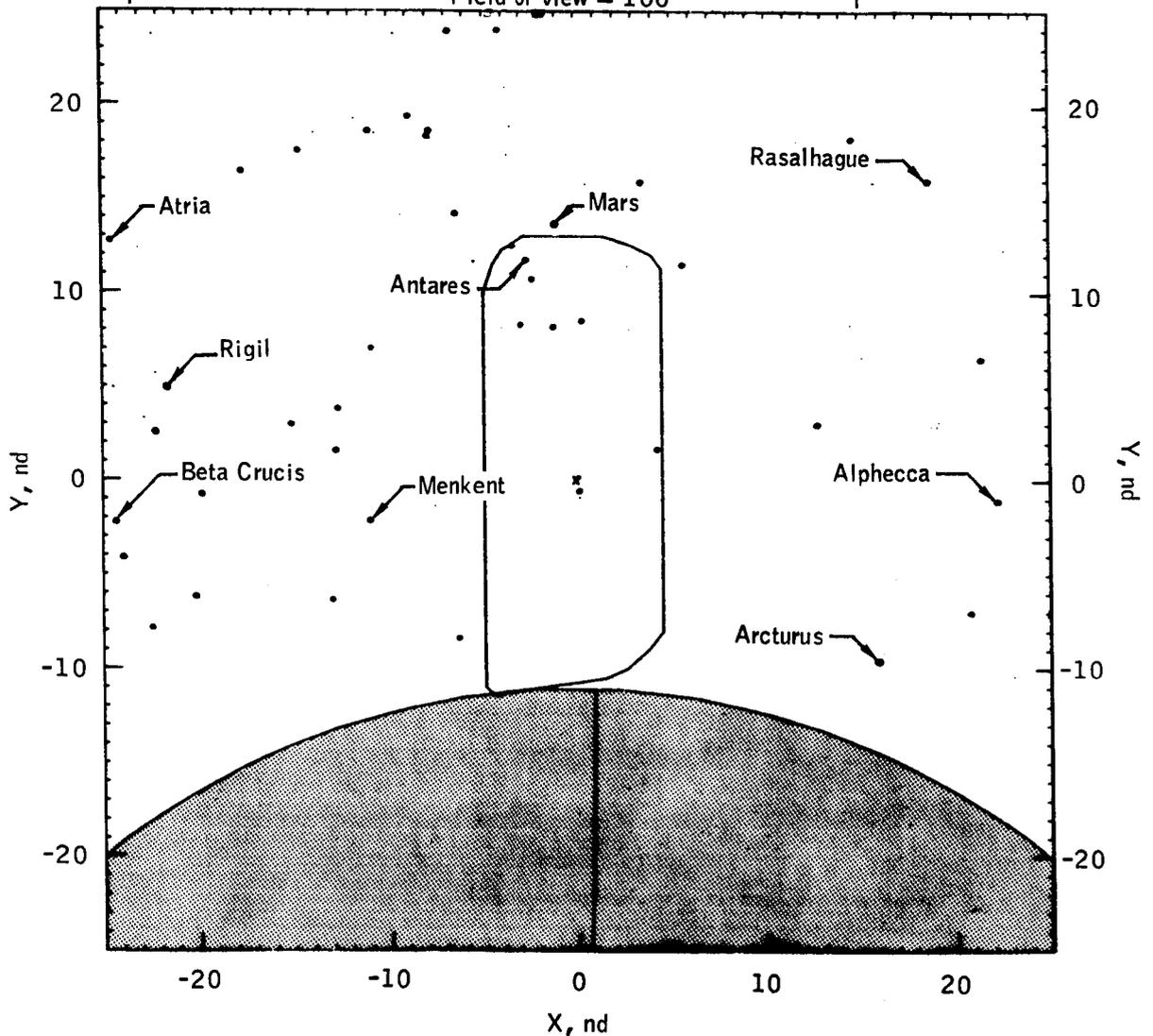
$R_M = 955$ n. mi.

$h_M = 19$ stat. mi.

$V_i = 5680$ fps

$V_i = 3873$ mph

Field of view = 100°



(h) End phasing burn - docking window (g.e.t. = 100:47:03).

SEC 349 362
 X 21 19
 Y -18 -19

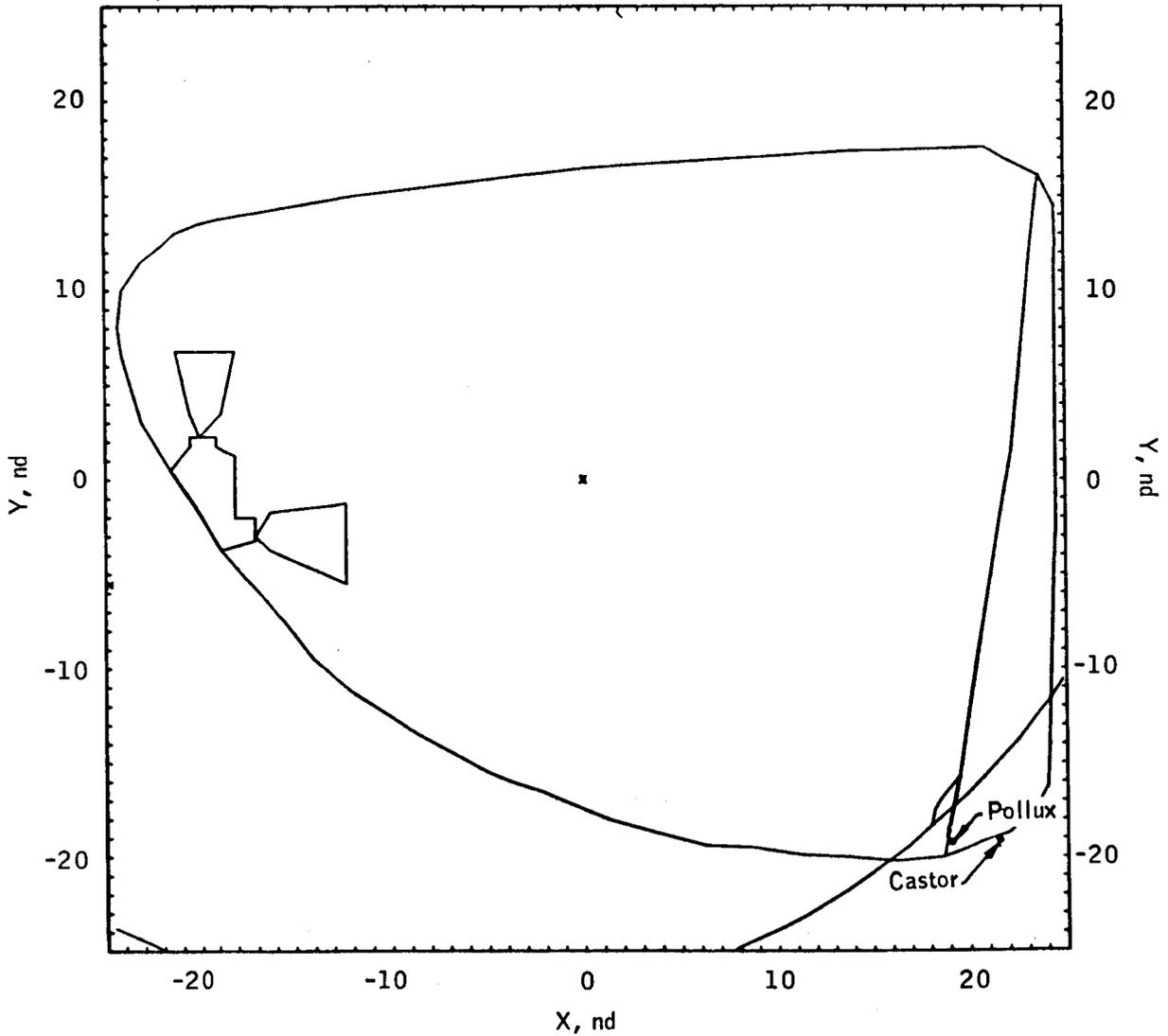
$R_M = 964$ n. mi.

$V_i = 5631$ fps

$h_M = 29$ stat. mi.

$V_i = 3839$ mph

Field of view = 100°



(i) Descent stage jettison (end burn)- front window (g.e.t. = 102:33:28).

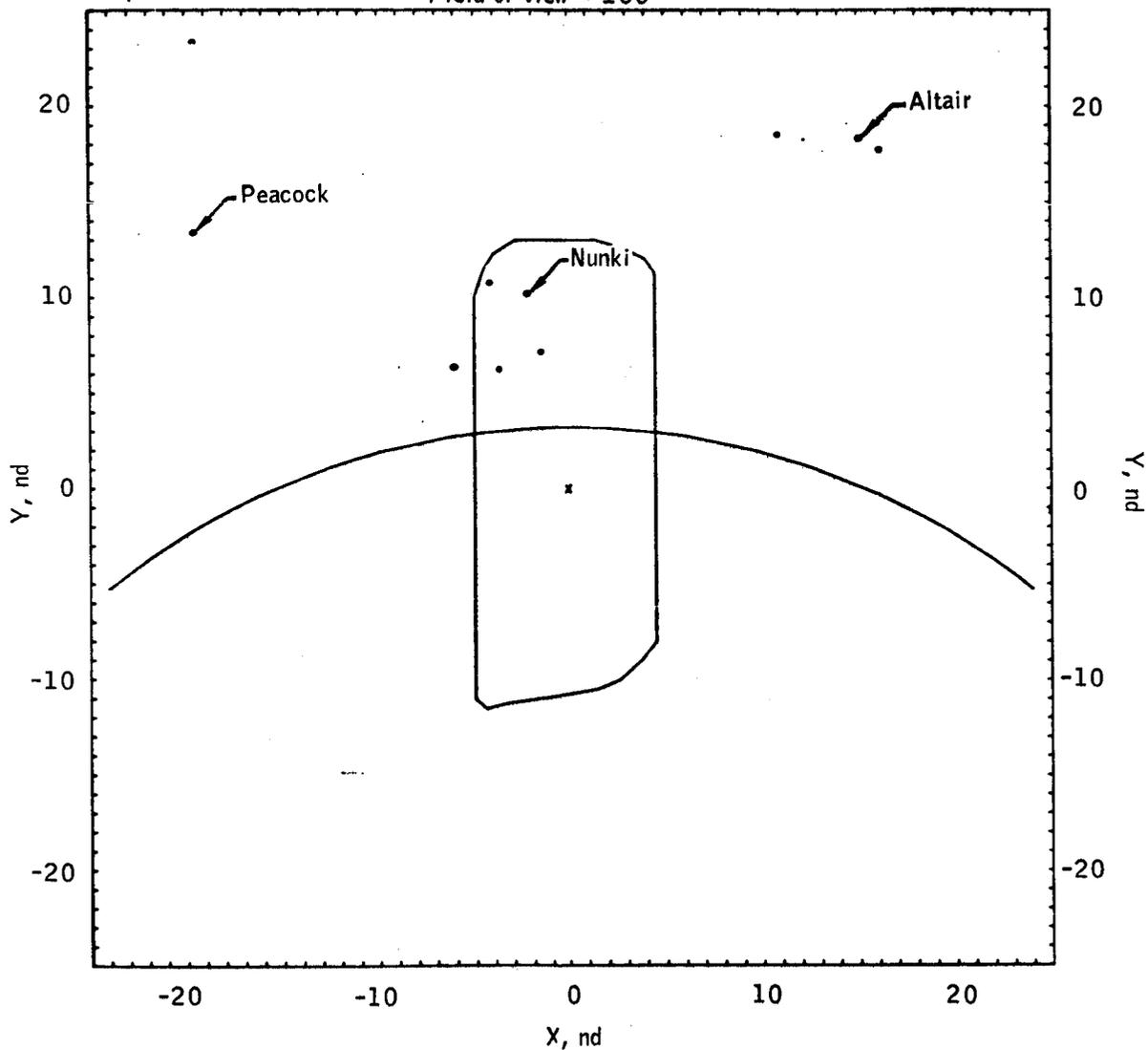
Figure 12. - Continued.

SEC	834	841	844	861	871	904	907	909	913	1001
X	-3	-6	-1	-2	-4	16	15	10	-19	-19
Y	6	6	7	10	10	17	18	18	13	23

$R_M = 964$ n. mi.
 $V_i = 5631$ fps

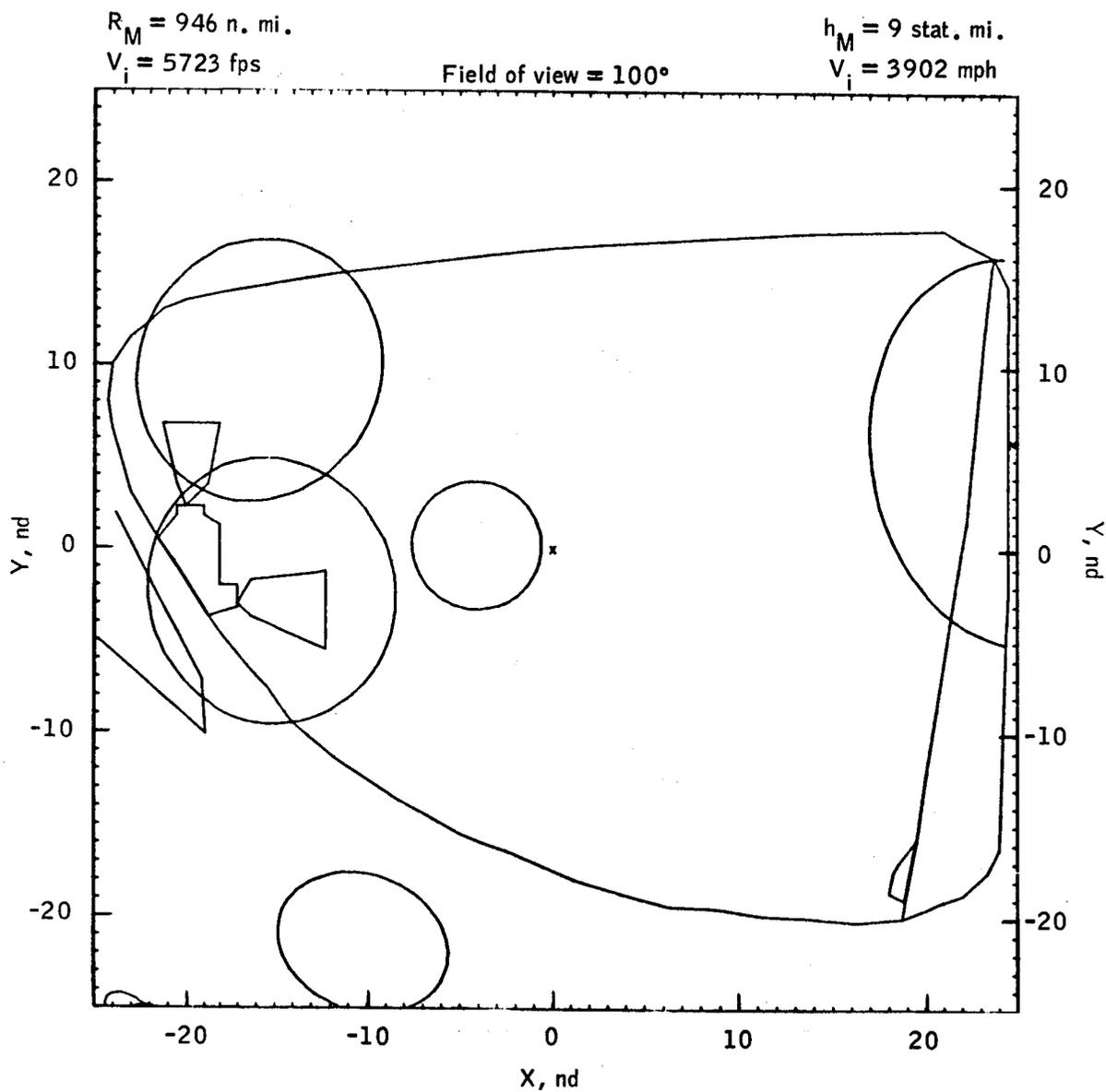
$h_M = 29$ stat. mi.
 $V_i = 3839$ mph

Field of view = 100°



(j) Descent stage jettison (end burn)- docking window (g.e.t. =102:33:28).

Figure 12. - Continued.



(k) Begin insertion burn - front window (g.e.t. = 102:43:18).

Figure 12.- Continued.

SEQ	4	22	31	41	47	63	73	75	80	108	111	112
X	-14	-23	-24	-13	-23	-4	-14	-5	8	6	-10	-11
Y	23	10	8	16	7	15	9	13	16	10	5	4

SEQ	120	144	150	151	186	205	215	221	1079	1082
X	-15	-2	-5	-9	2	-5	13	15	0	1
Y	1	2	1	0	-2	-5	-5	-5	22	15

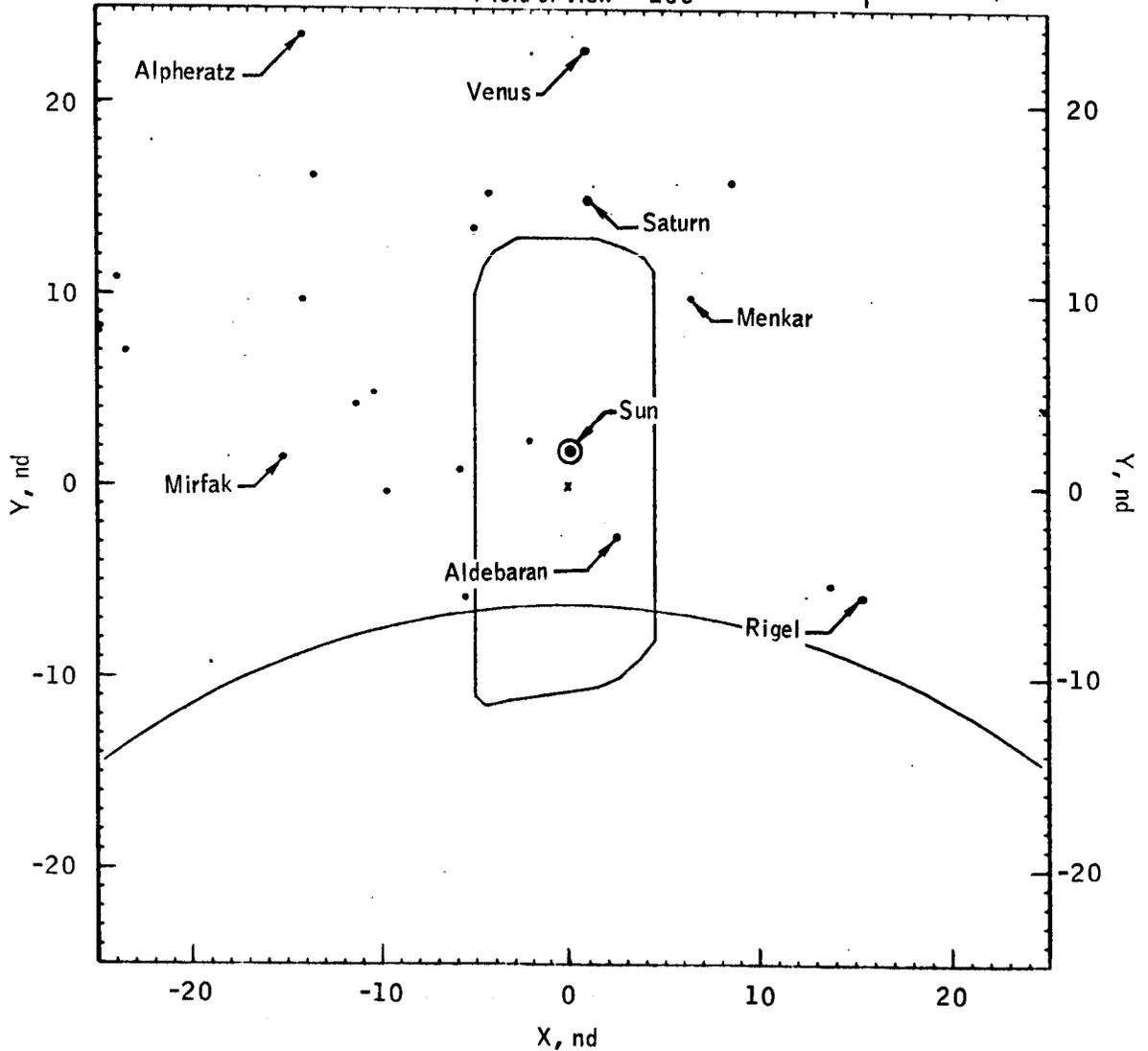
$R_M = 946$ n. mi.

$V_i = 5723$ fps

$h_M = 9$ stat. mi.

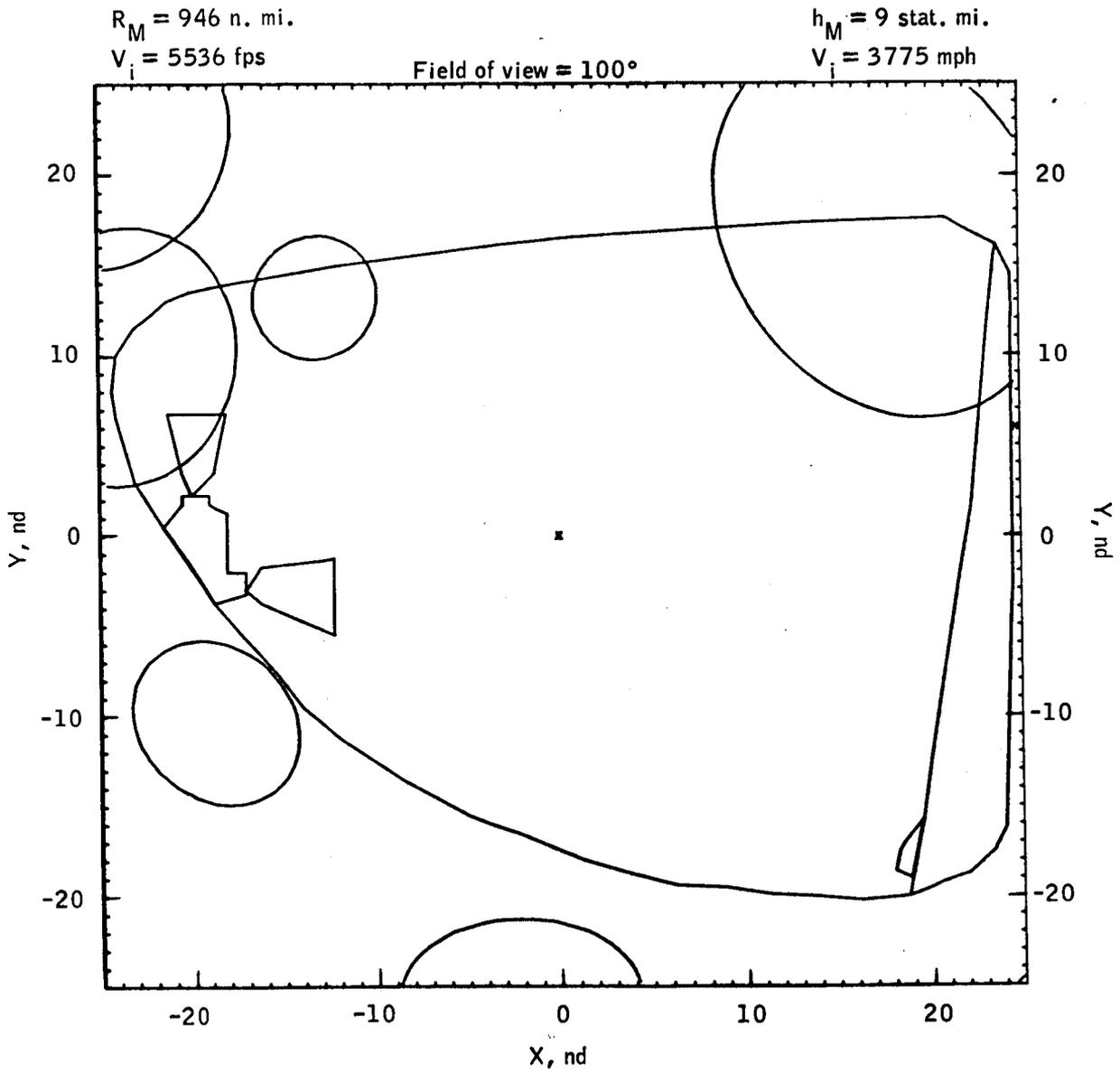
$V_i = 3902$ mph

Field of view = 100°



(I) Begin insertion burn - docking window (g.e.t. = 102:43:18).

Figure 12.- Continued.



(m) End insertion burn - front window (g.e.t. = 102:43:33).

Figure 12.- Continued.

SEQ	4	22	31	41	47	63	73	75	80	108	111	112
X	-14	-23	-24	-13	-23	-4	-14	-5	8	6	-10	-11
Y	23	10	8	16	7	15	9	13	16	10	5	4

SEQ	120	144	150	151	186	215	221	1079	1082
X	-15	-2	-5	-9	2	13	15	0	1
Y	1	2	1	0	-2	-5	-5	22	15

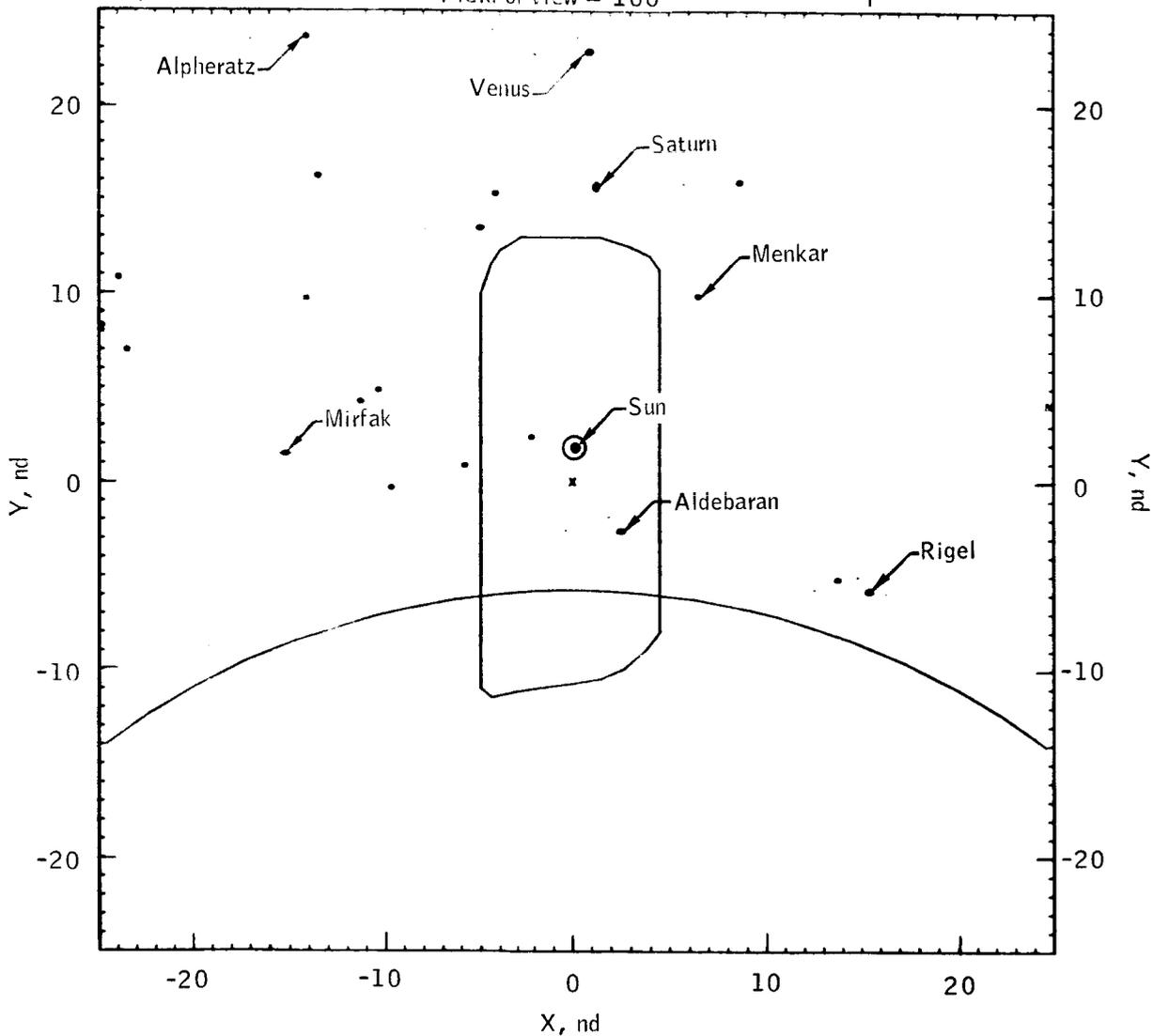
$R_M = 946$ n. mi.

$V_i = 5536$ fps

$h_M = 9$ stat. mi.

$V_i = 3775$ mph

Field of view = 100°

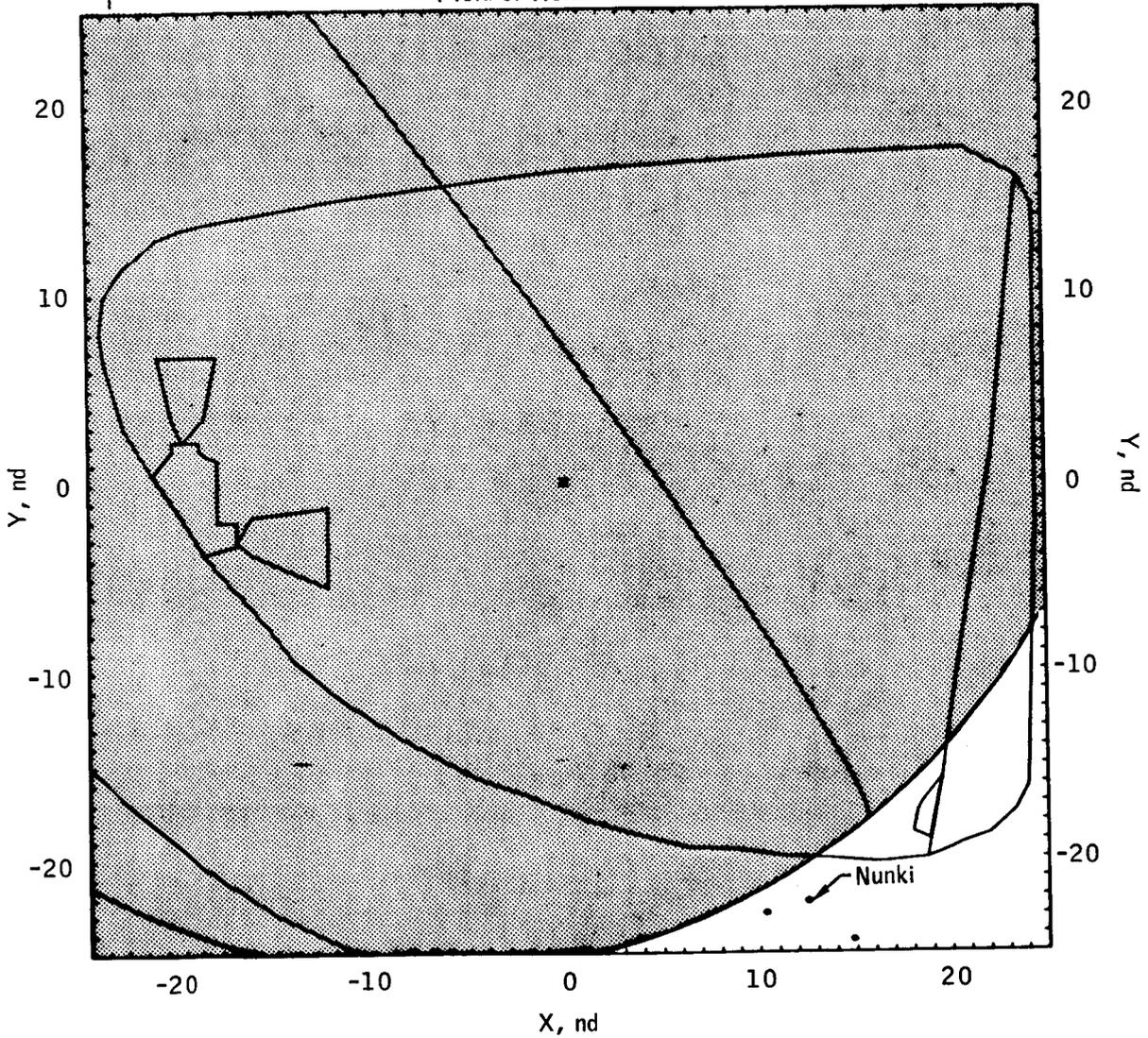


(n) End insertion burn - docking window (g.e.t. = 102:43:33).

Figure 12.- Continued.

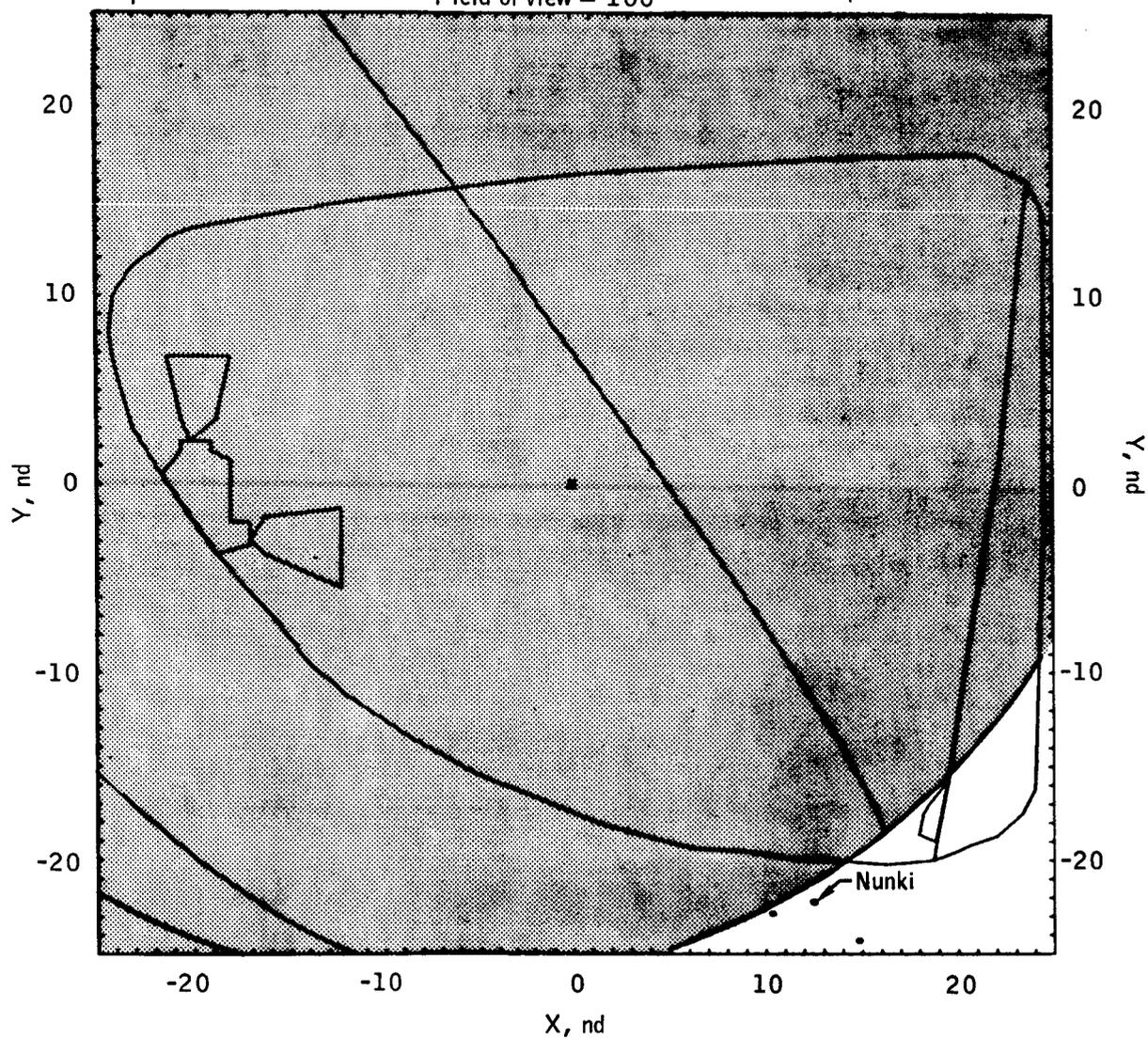
SEQ	844	861	871
X	14	12	10
Y	-24	-22	-22

 $R_M = 982 \text{ n. mi.}$
 $V_i = 5338 \text{ fps}$

 Field of view = 100°
 $h_M = 50 \text{ stat. mi.}$
 $V_i = 3640 \text{ mph}$


(o) Begin CSI burn - front window (g.e.t. = 103:33:46).

SEG	044	061	071
X	14	12	10
Y	-24	-22	-22

 $R_M = 982 \text{ n. mi.}$
 $V_i = 5388 \text{ fps}$
 $h_M = 50 \text{ stat. mi.}$
 $V_i = 3670 \text{ mph}$
Field of view = 100° 

(p) End CSI burn - front window (g.e.t. = 103:34:18).

Figure 12.- Continued.

SEQ	106	205	207	215	221	222	230	231	233	237	239	245	246
X	-2	5	10	-13	-15	11	-8	3	-21	-11	-20	-19	-12
Y	1	4	5	3	4	6	6	7	5	7	5	7	7

SEQ	248	252	256	265	270	271	281	290	301	308	349	356	362
X	0	-12	-16	-7	11	7	0	-20	3	-20	6	-8	4
Y	8	8	8	10	10	10	12	12	15	15	20	23	22

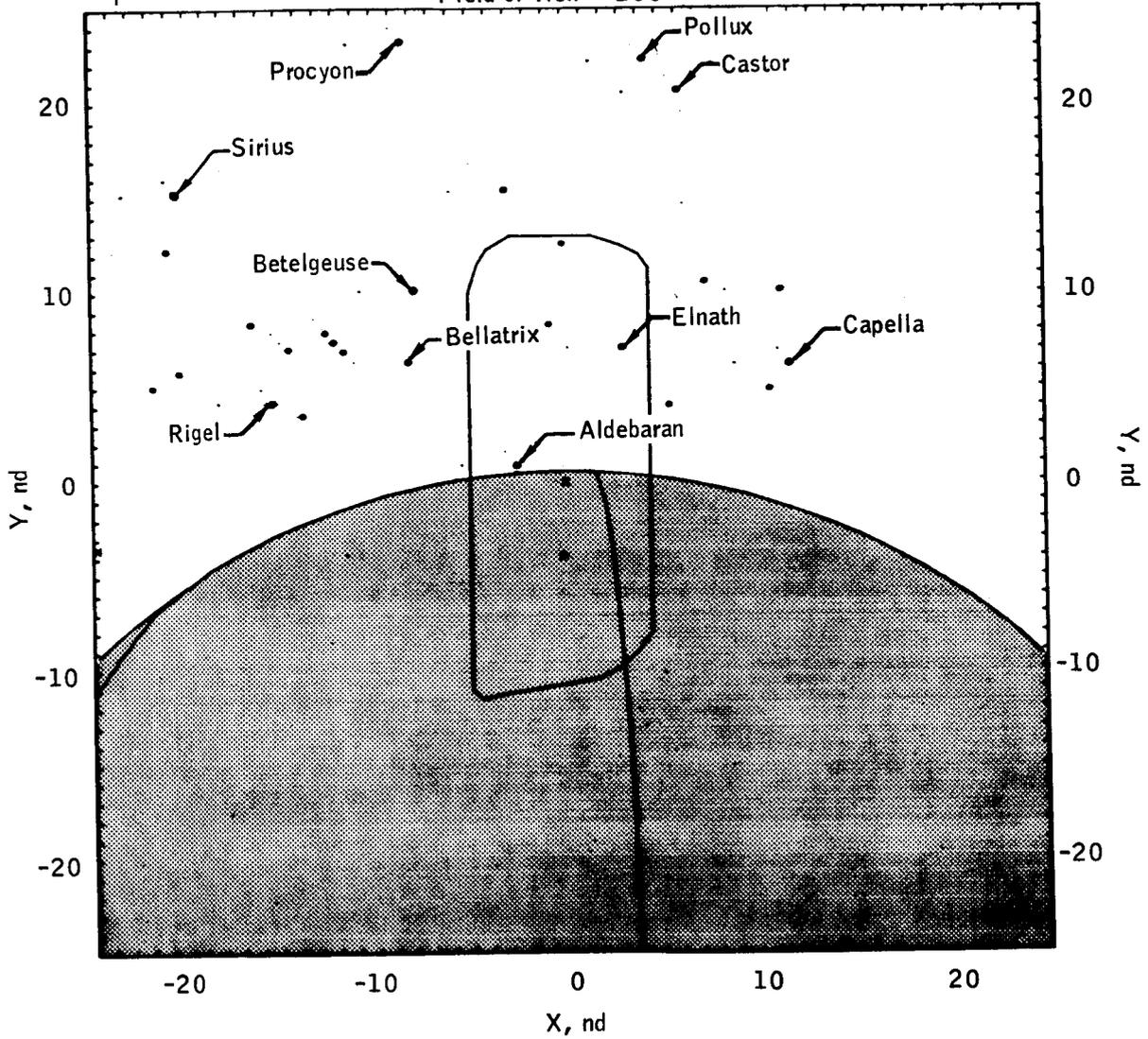
$R_M = 982$ n. mi.

$V_i = 5388$ fps

$h_M = 50$ stat. mi.

$V_i = 3670$ mph

Field of view = 100°



(q) End CSI burn - docking window (g.e.t. = 103:34:18).

SEQ	751	755	757	759	770	781	789	790	793	795
X	-4	21	-22	-8	-1	-18	-11	-16	-11	9
Y	1	15	-8	1	8	-2	4	0	4	17
SEQ	797	802	803	836	841	844	861	871	1080	
X	-14	-13	5	-12	-14	-10	-13	-15	-3	
Y	2	4	16	10	9	12	14	14	3	

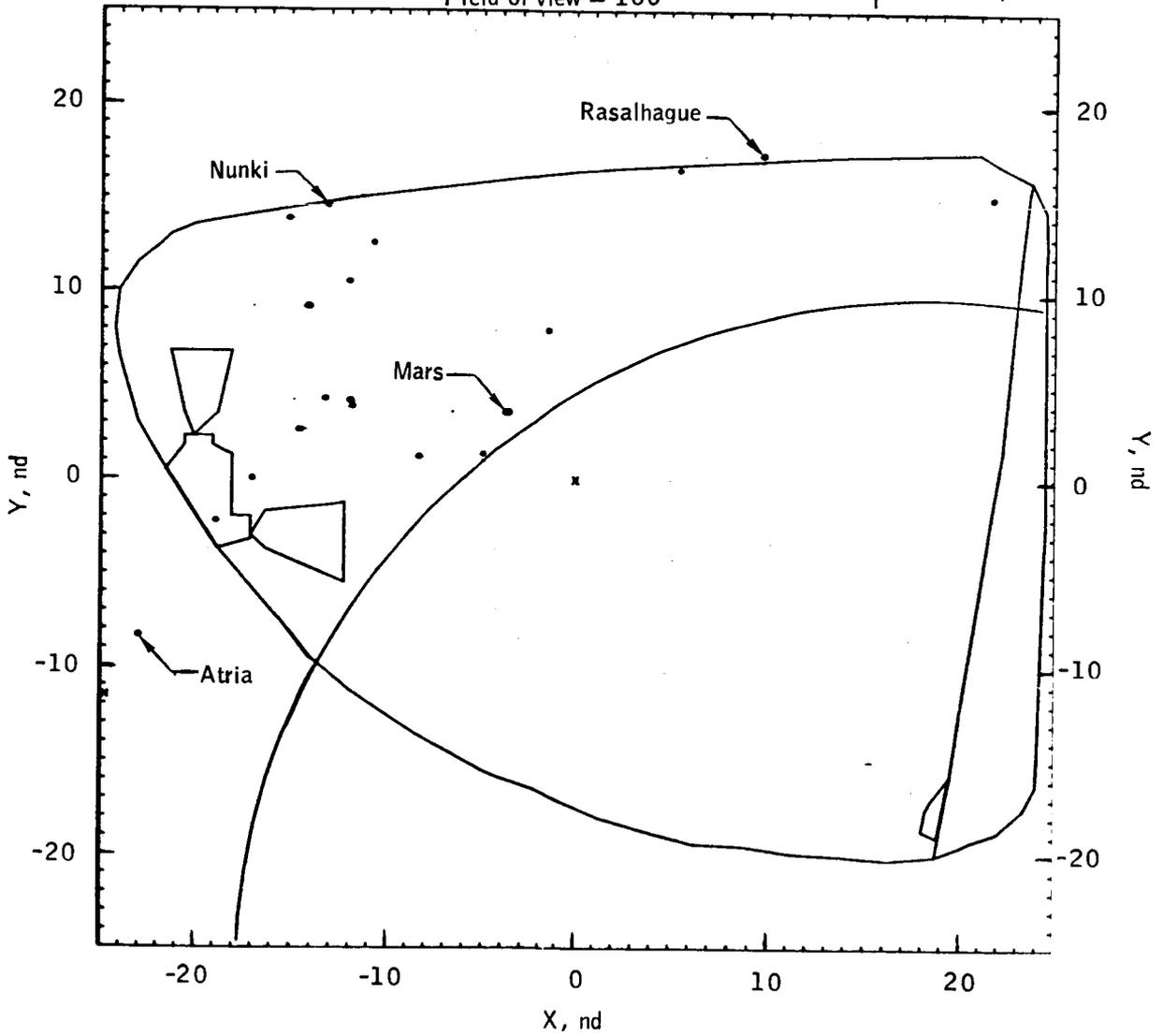
$R_M = 981$ n. mi.

$h_M = 49$ stat. mi.

$V_i = 5391$ fps

$V_i = 3676$ mph

Field of view = 100°



(r) Begin CDH burn - front window (g.e.t. = 104:31:42).

Figure 12.- Continued.

SEQ	4	7	15	25	41	904	907	909	933	950
X	13	6	-20	-11	14	16	14	10	-20	24
Y	16	15	3	11	24	-16	-16	-17	-18	-3
SEQ	984	990	1001	1010	1028	1041	1044	1046	1079	
X	10	-1	-17	-24	-18	-11	15	9	0	
Y	-2	-7	-9	-10	-6	-1	9	7	20	

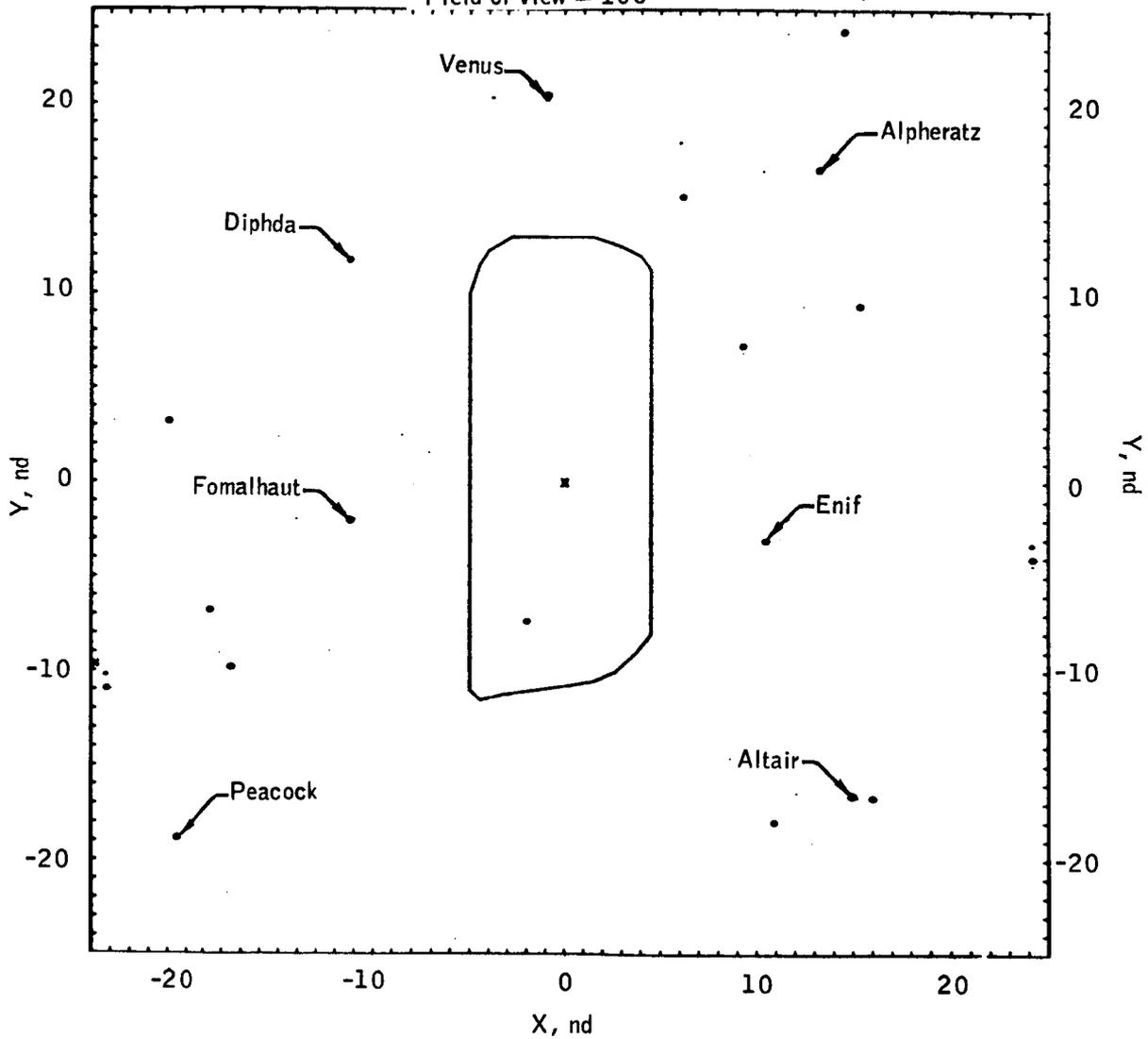
$R_M = 981$ n. mi.

$h_M = 49$ stat. mi.

$V_i = 3591$ fps

$V_i = 3676$ mph

Field of view = 100°



(s) Begin CDH burn - docking window (g.e.t. = 104:31:42).

Figure 12.- Continued.

SEQ	751	755	759	770	781	789	790	793	795
X	-10	18	-13	-6	-24	-17	-22	-17	5
Y	9	20	8	15	4	11	6	11	24
SEQ	797	802	803	836	841	844	861	871	1080
X	-20	-18	1	-17	-19	-16	-18	-20	-9
Y	9	11	24	18	16	20	22	21	11

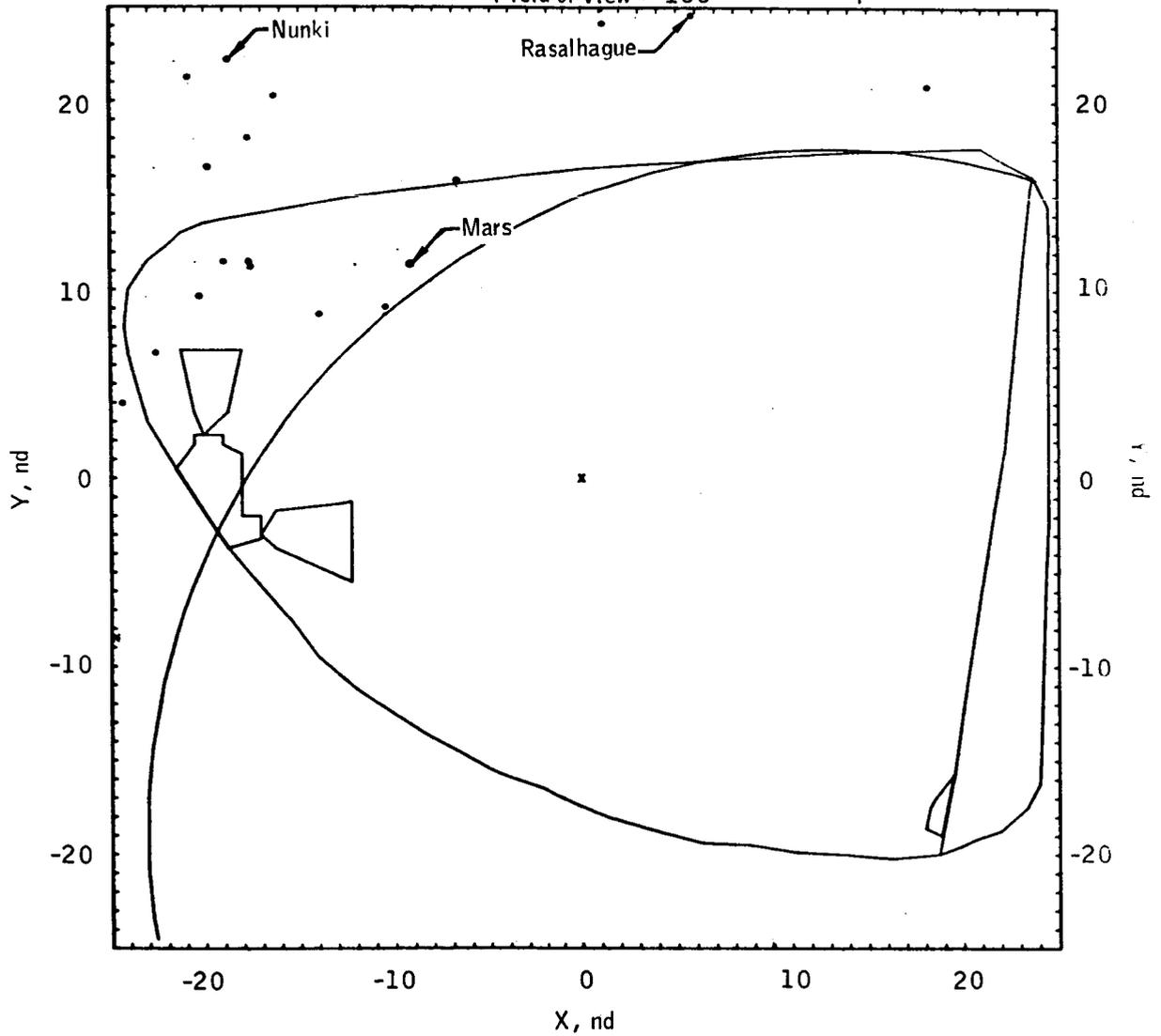
$R_M = 981$ n. mi.

$V_i = 5390$ fps

$h_M = 49$ stat. mi.

$V_i = 3675$ mph

Field of view = 100°



(t) End of CDH burn - front window (g.e.t. = 104:31:45).

Figure 12.- Continued.

SEQ	7	15	25	781	795	803	836	841	844	861	871	909
X	6	-21	-11	-19	20	15	-4	-6	-1	-2	-4	15
Y	24	10	20	-24	-23	-24	-22	-21	-21	-18	-17	-8
SEQ	907	909	933	950	984	990	1001	1010	1028	1041	1044	1048
X	14	10	-19	24	10	-1	-17	-23	-18	-11	16	9
Y	-7	-8	-10	3	6	2	-1	-3	1	7	17	16

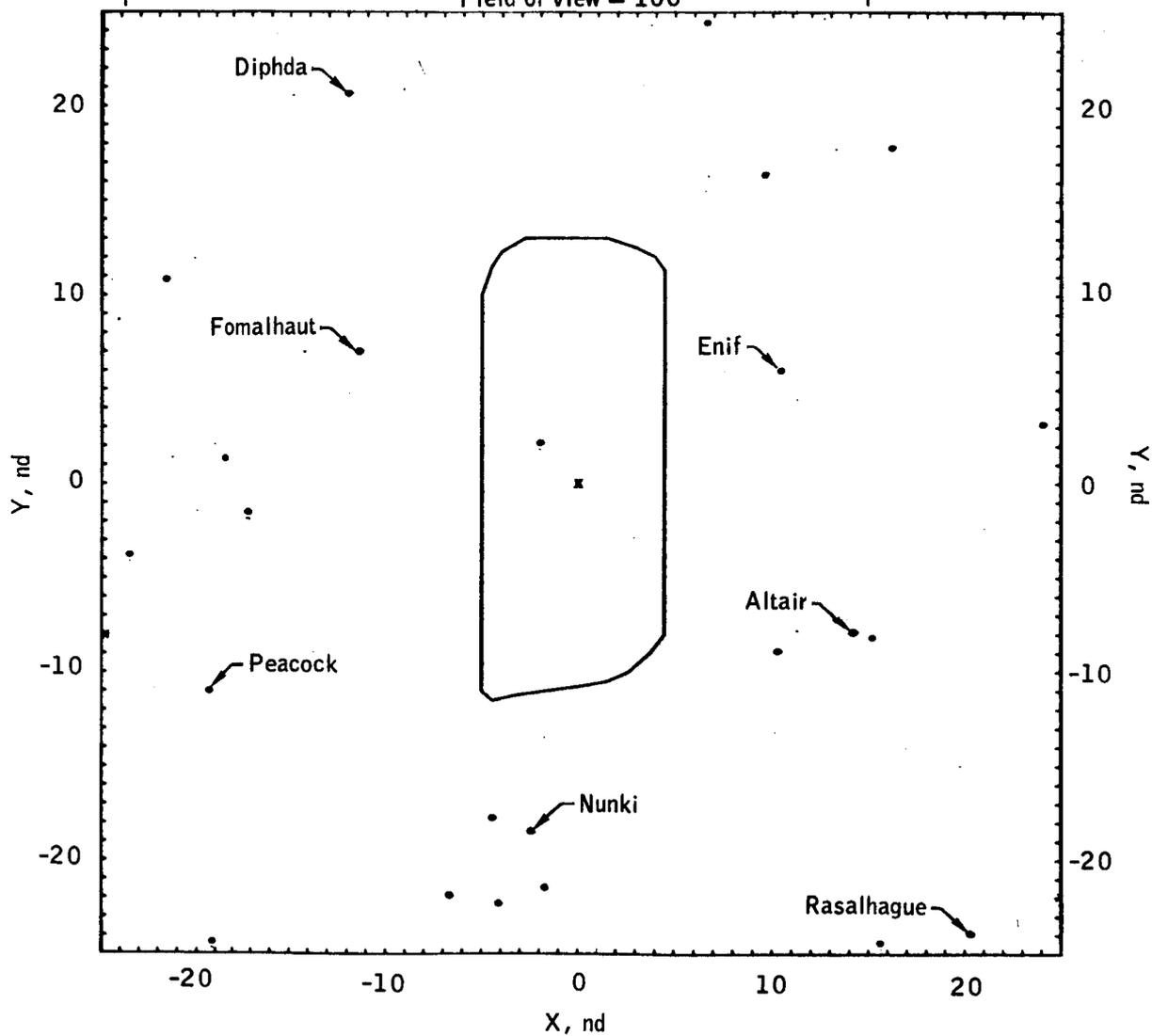
$R_M = 981$ n. mi.

$h_M = 49$ stat. mi.

$V_i = 5390$ fps

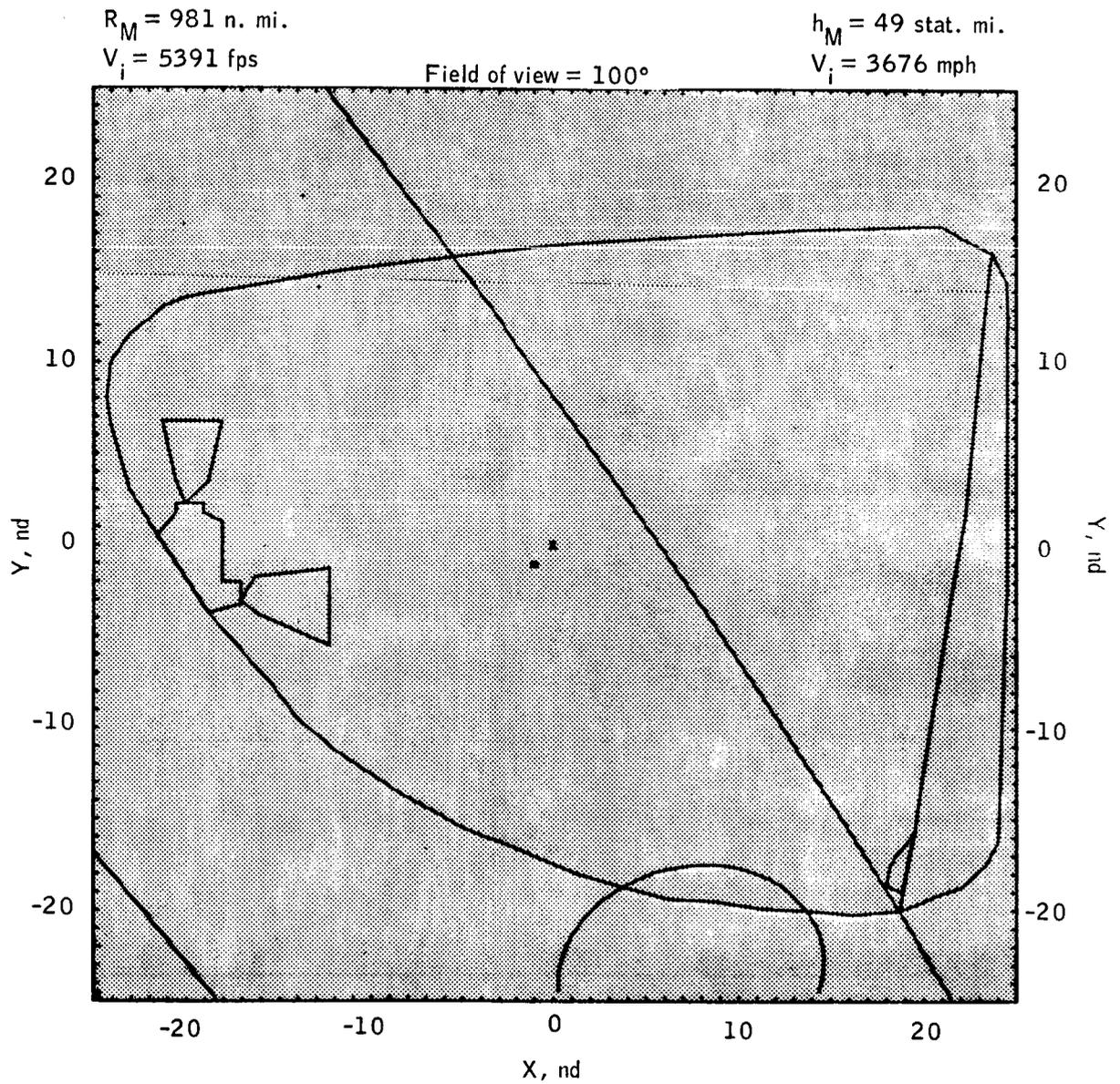
$V_i = 3675$ mph

Field of view = 100°



(u) End of CDH burn - docking window (g.e.t. = 104:31:45).

Figure 12.- Continued.



(v) Begin TPI burn - front window (g.e.t. = 105:08:57).

Figure 12.- Continued.

SEQ	377	440	473	480	507	515	535	540	545	551	566	569
X	-21	-10	0	4	23	7	6	24	-24	-7	-9	-22
Y	-11	-5	-4	-4	-7	1	6	-3	18	15	10	21
SEQ	570	580	582	589	593	595	610	624	651	1001		
X	1	20	8	-14	0	-7	15	17	22	1		
Y	15	6	15	24	22	24	18	20	20	0		

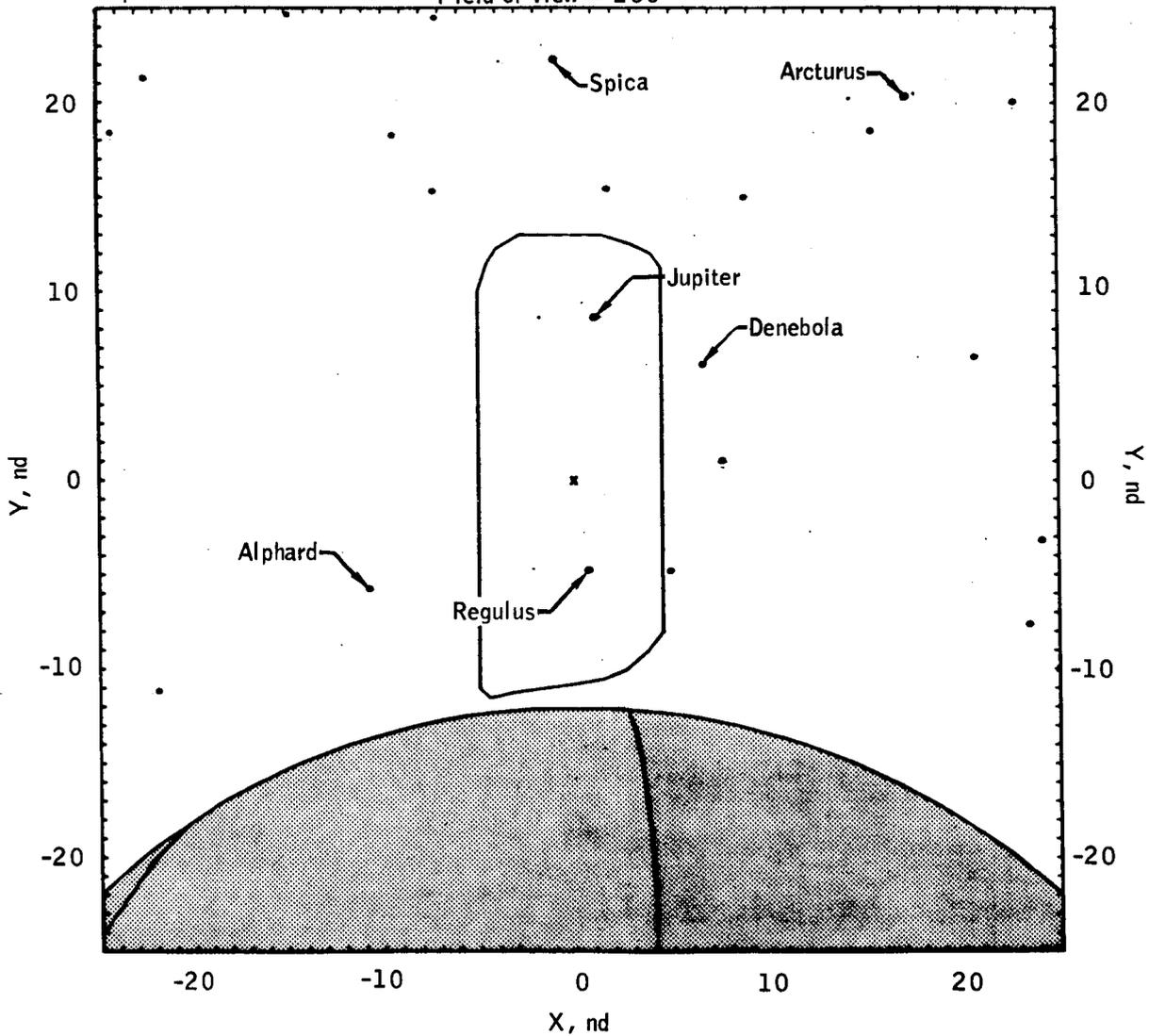
$R_M = 981$ n. mi.

$h_M = 49$ stat. mi.

$V_i = 5391$ fps

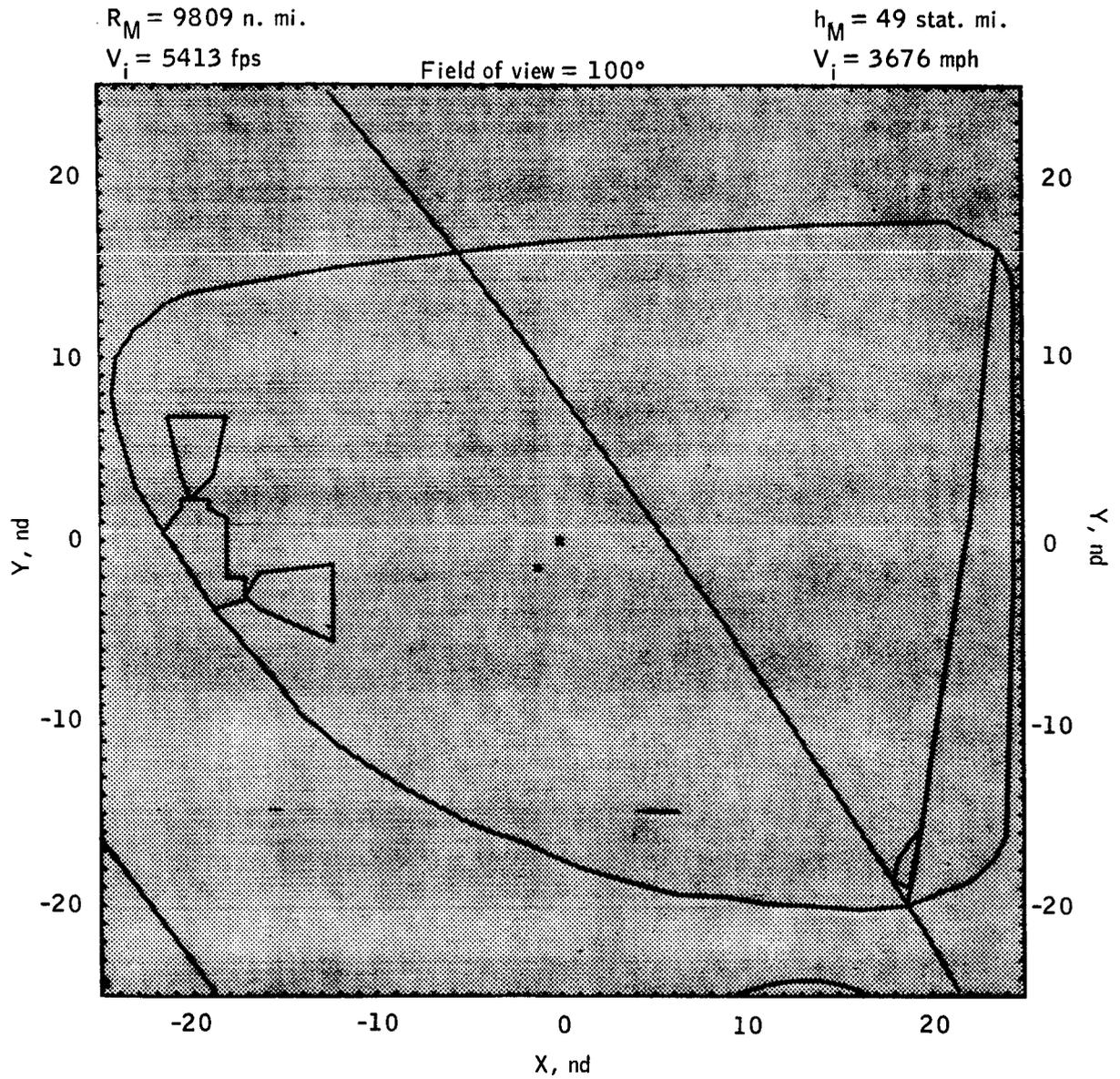
$V_i = 3676$ mph

Field of view = 100°



(w) Begin TPI burn - docking window (g.e.t. = 105:08:57).

Figure 12.- Continued.



(x) End TPI burn - front window (g.e.t. = 105:09:13).

Figure 12.- Continued.

SEQ	377	440	473	480	507	515	535	540	545	551	566	569
X	-21	-10	0	4	23	7	6	24	-24	-7	-9	-22
Y	-11	-5	-4	-4	-7	0	5	-3	18	15	18	21

SEQ	570	580	582	589	593	595	610	624	651	1001
X	1	20	8	-14	0	-7	15	17	22	1
Y	15	6	14	24	22	24	18	20	19	8

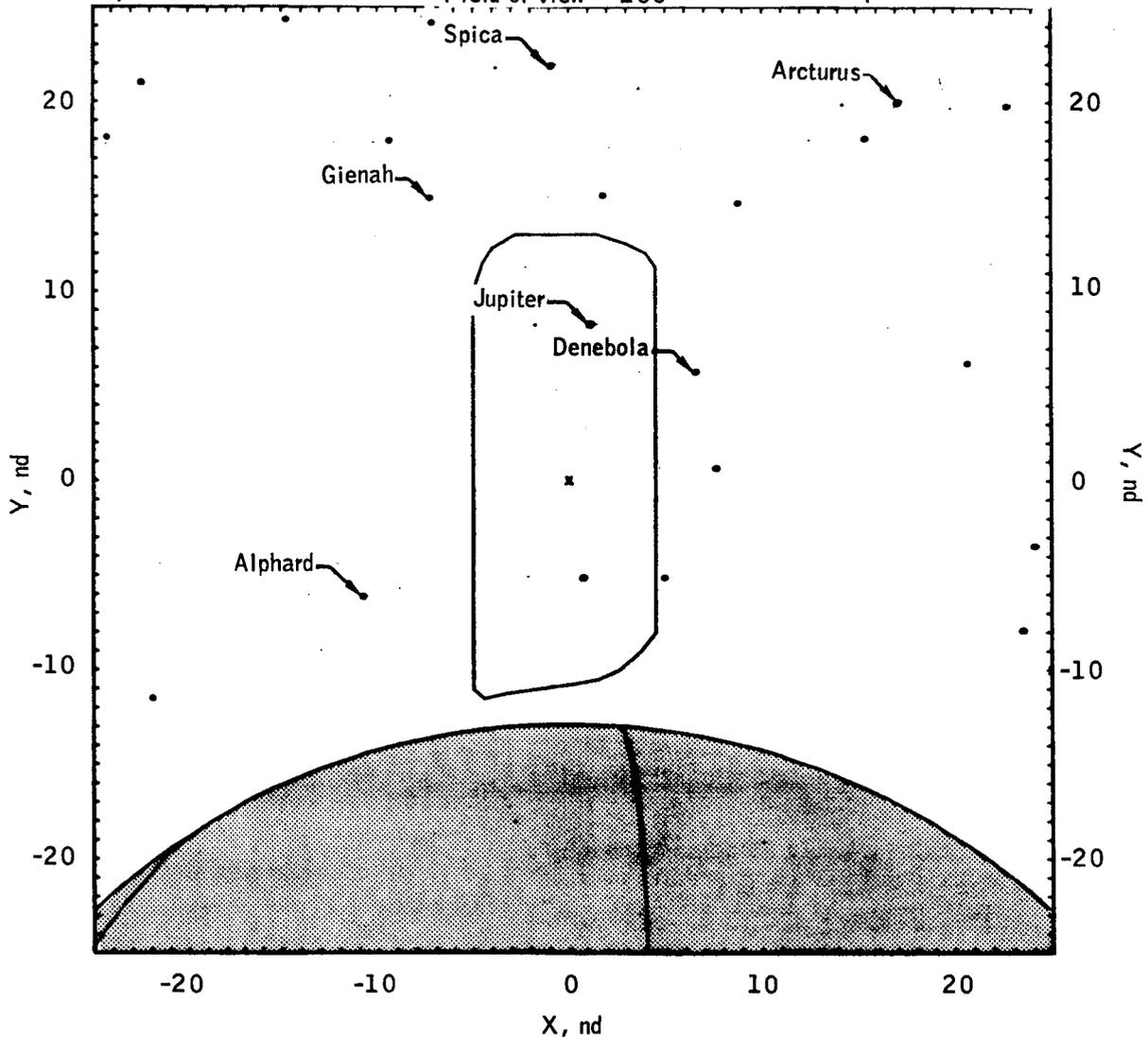
$R_M = 9809$ n. mi.

$h_M = 49$ stat. mi.

$V_i = 5431$ fps

$V_i = 3676$ mph

Field of view = 100°



(y) End of TPI burn - docking window (g.e.t. = 105:09:13).

Figure 12.- Concluded.

TRANSEARTH INJECTION
BURN

SEQ	22	31	41	47	63	73	75	80	108	111	112	120	144	150	151	186
X	-23	-24	-12	-23	-4	-13	-4	8	6	-10	-11	-15	-2	-6	-10	2
Y	1	-2	2	-4	0	-3	-1	1	-4	-9	-9	-11	-12	-13	-14	-17
SEQ	205	207	215	221	222	230	231	233	237	239	245	246	248	252	256	
X	-6	-11	14	16	-13	8	-3	23	12	22	15	13	0	13	18	
Y	-20	-20	-18	-18	-21	-22	-23	-17	-22	-19	-21	-22	-24	-23	-22	

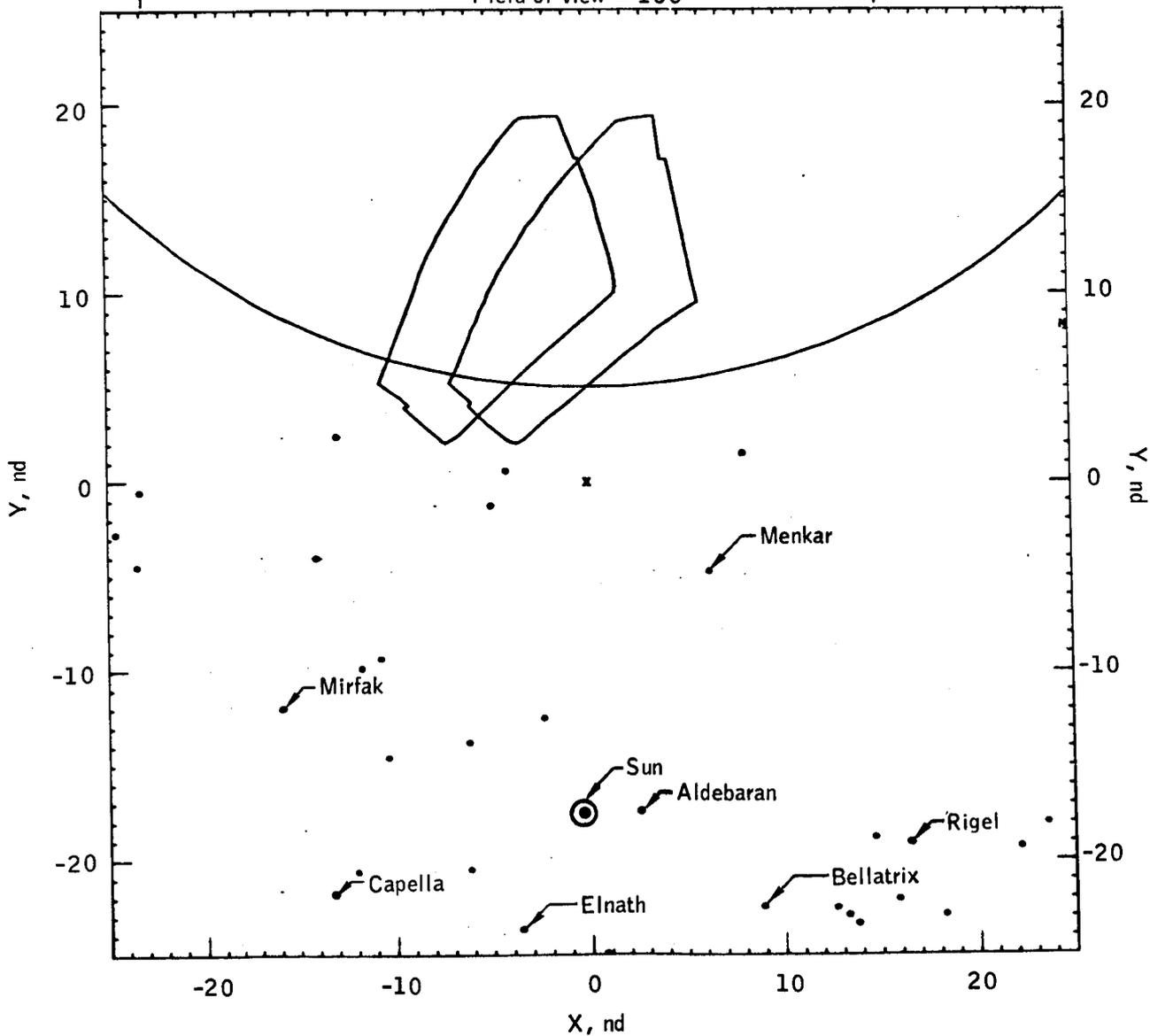
$R_M = 996$ n. mi.

$V_i = 5349$ fps

$h_M = 66$ stat. mi.

$V_i = 4758$ mph

Field of view = 100°



(a) Begin TEI burn (g. e. t. = 137:20:22.4).

Figure 13.- Transearth injection burn.

SEQ	41	63	73	75	80	108	111	112	120	144	150	151	186	205
X	-15	-8	-16	-7	5	10	13	14	18	-4	-8	-12	0	-8
Y	2	0	-4	-1	1	-4	-9	-10	-12	-12	-14	-14	-17	-20
SEQ	207	215	221	222	230	231	233	237	239	245	246	252	256	
X	-14	12	14	-15	6	-5	21	10	19	13	11	11	16	
Y	-20	-18	-19	-22	-22	-23	-17	-22	-19	-21	-22	-23	-22	

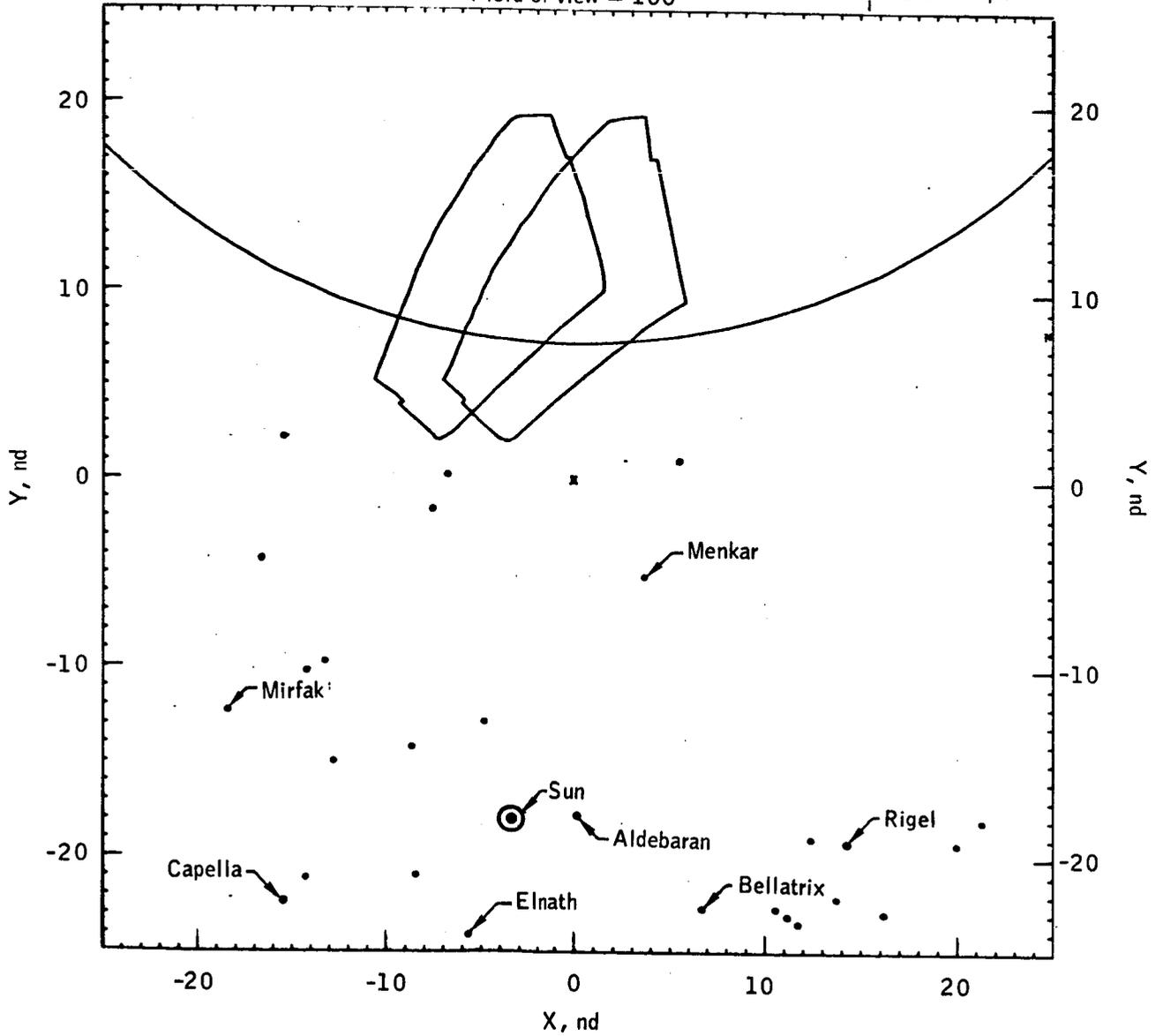
$R_M = 995$ n. mi.

$V_i = 6978$ fps

$h_M = 67$ stat. mi.

$V_i = 3647$ mph

Field of view = 100°



(b) Middle of TEI burn (g.e.t. = 137:21:52.4).

SEQ	4	22	31	41	47	63	73	75	80	108	111	112	120	144	150	151
X	-12	-23	-24	-12	-23	-4	-14	-5	7	6	-10	-11	-15	-2	-6	-10
Y	9	0	-3	1	-4	0	-4	-1	0	-5	-9	-10	-12	-13	-14	-15

SEQ	186	205	207	215	221	222	230	231	233	237	239	245	246	252	256
X	2	-6	-12	14	16	-13	5	-3	23	12	22	15	13	13	10
Y	-18	-21	-21	-19	-19	-22	-23	-24	-18	-23	-19	-22	-23	-23	-23

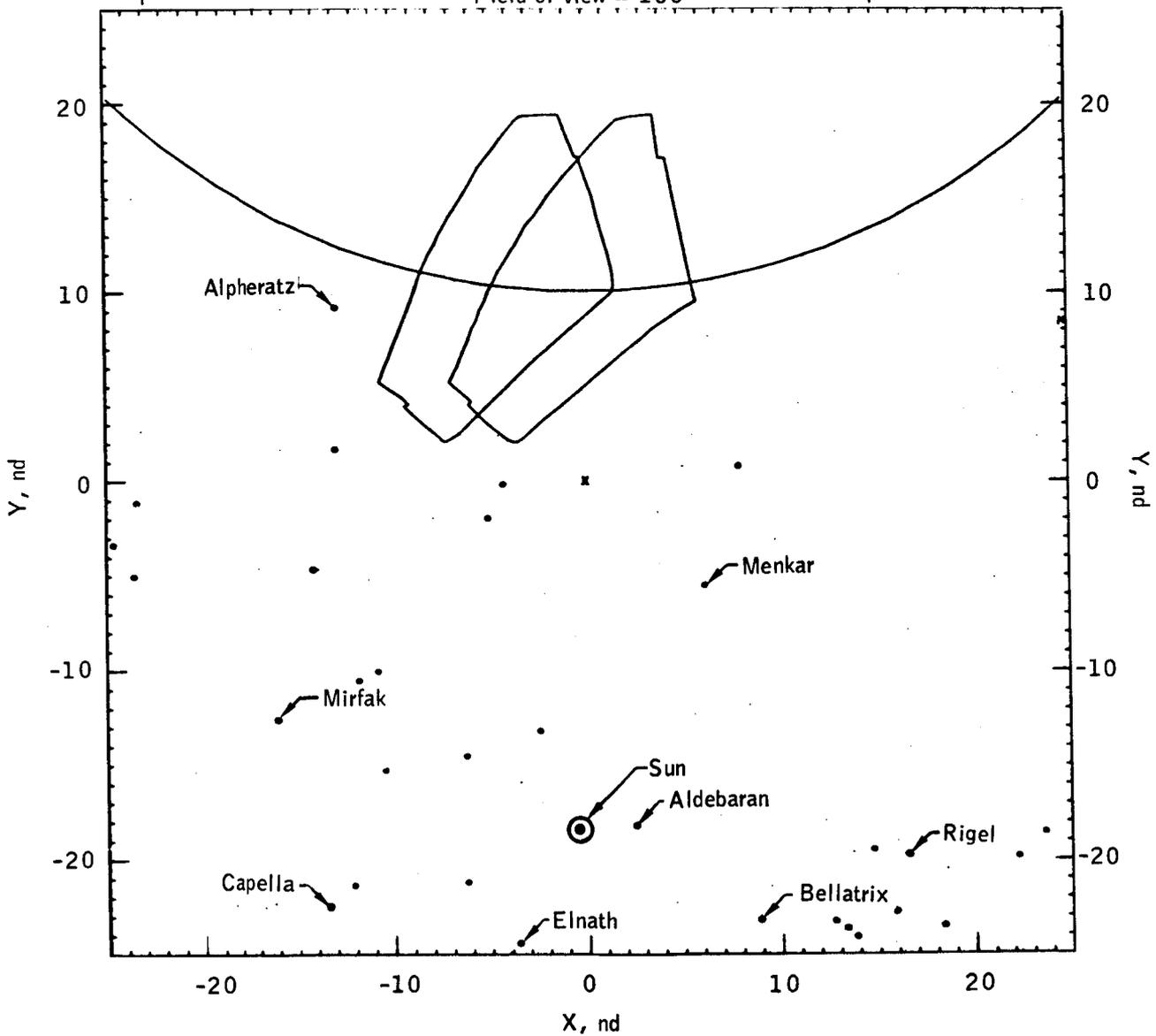
$R_M = 998$ n. mi.

$V_i = 8958$ fps

$h_M = 68$ stat. mi.

$V_i = 6108$ mph

Field of view $\approx 100^\circ$



(c) End of TEI burn (g.e.t. = 137:23:11.3).

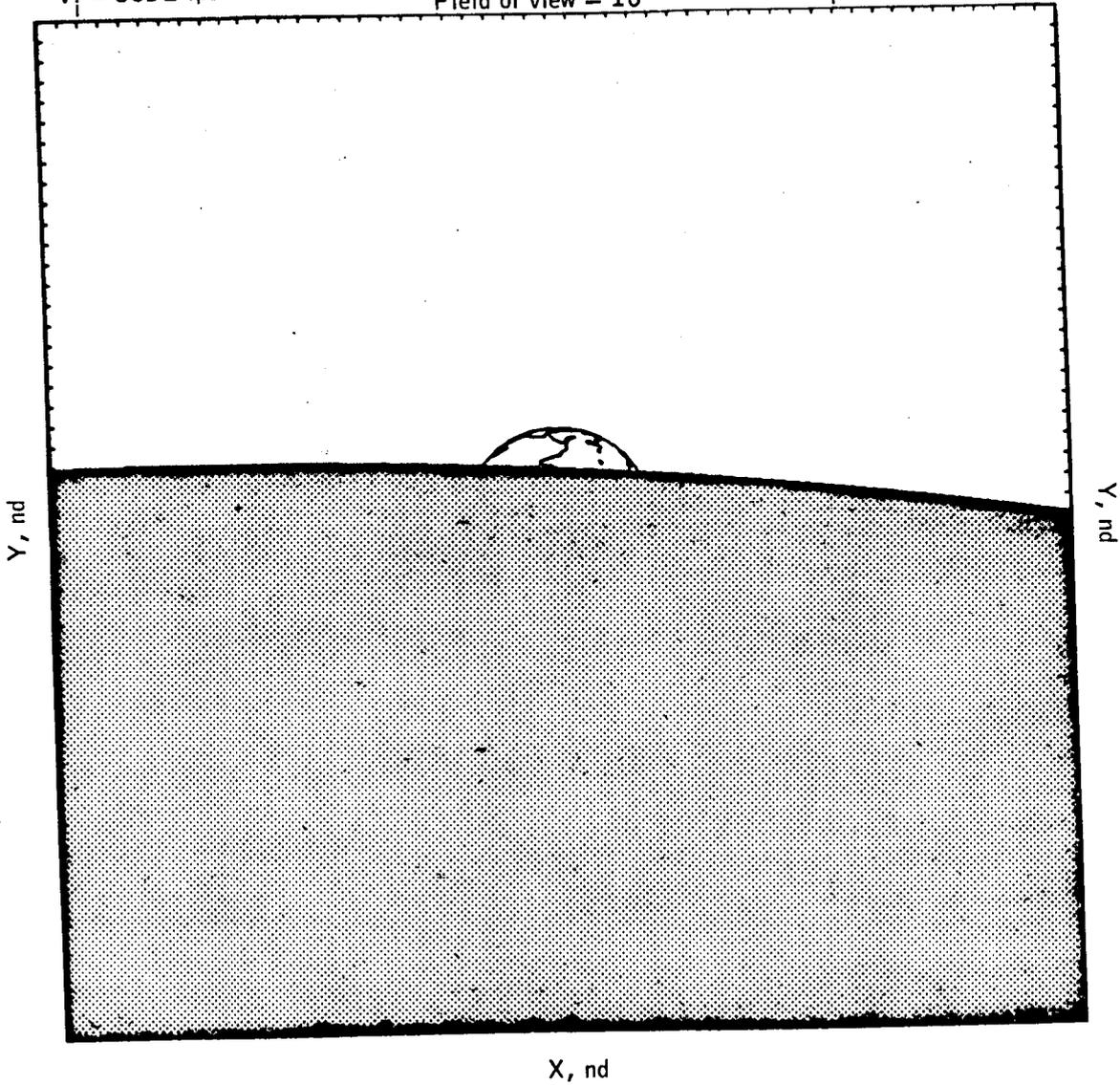
TRANSEARTH COAST

POST TEI

$R_M = 1109 \text{ n. mi.}$
 $V_i = 8632 \text{ fps}$

$h_M = 198 \text{ stat. mi.}$
 $V_i = 5885 \text{ mph}$

Field of view = 10°



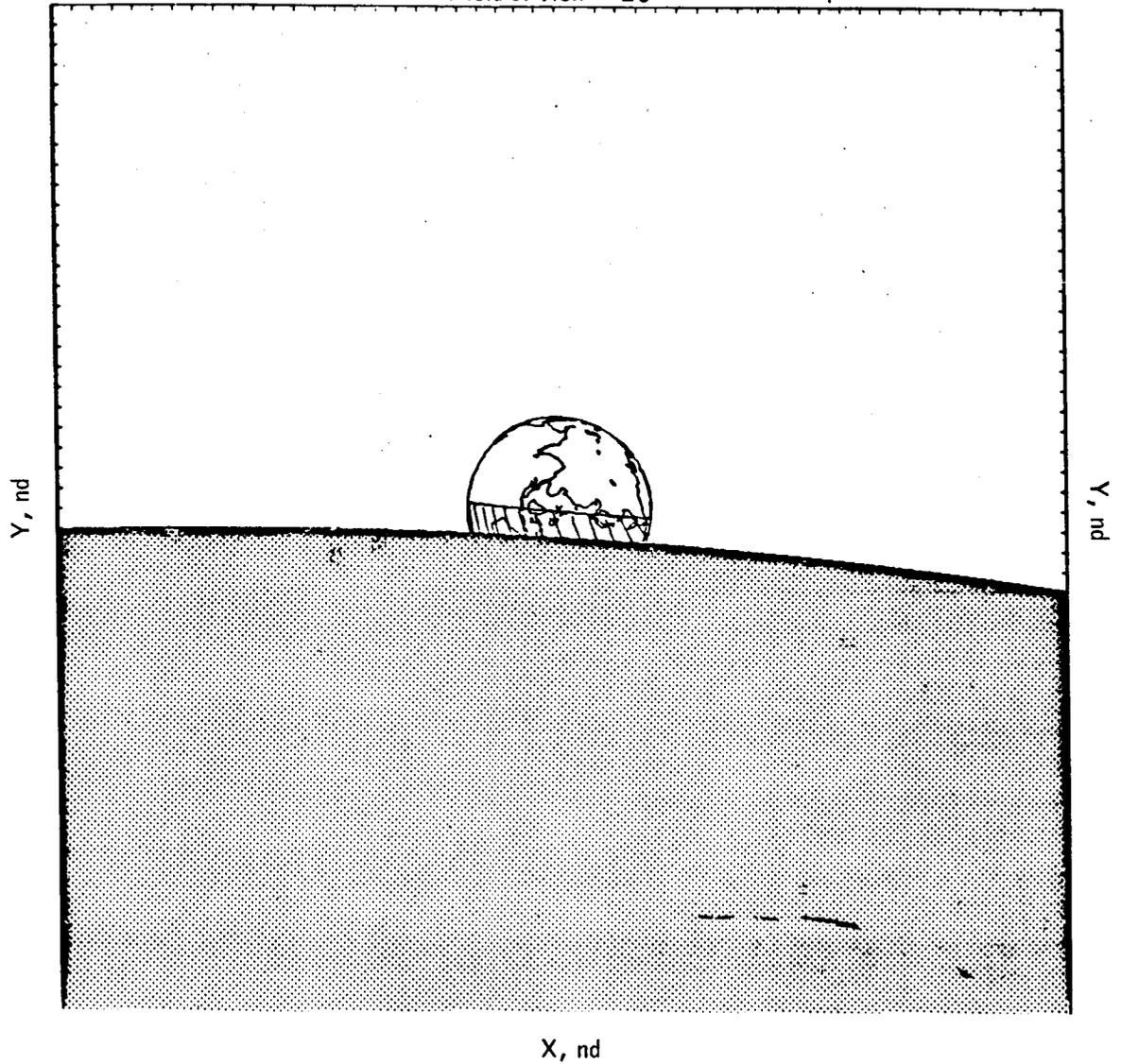
(a) G.e.t. = 137:29:11.3.

Figure 14. - Post TEI.

$R_M = 1113$ n. mi.
 $V_i = 8622$ fps

$h_M = 200$ stat. mi.
 $V_i = 5879$ mph

Field of view = 10°



(b) G.e.t. = 137:29:18.5.

Figure 14.- Continued.

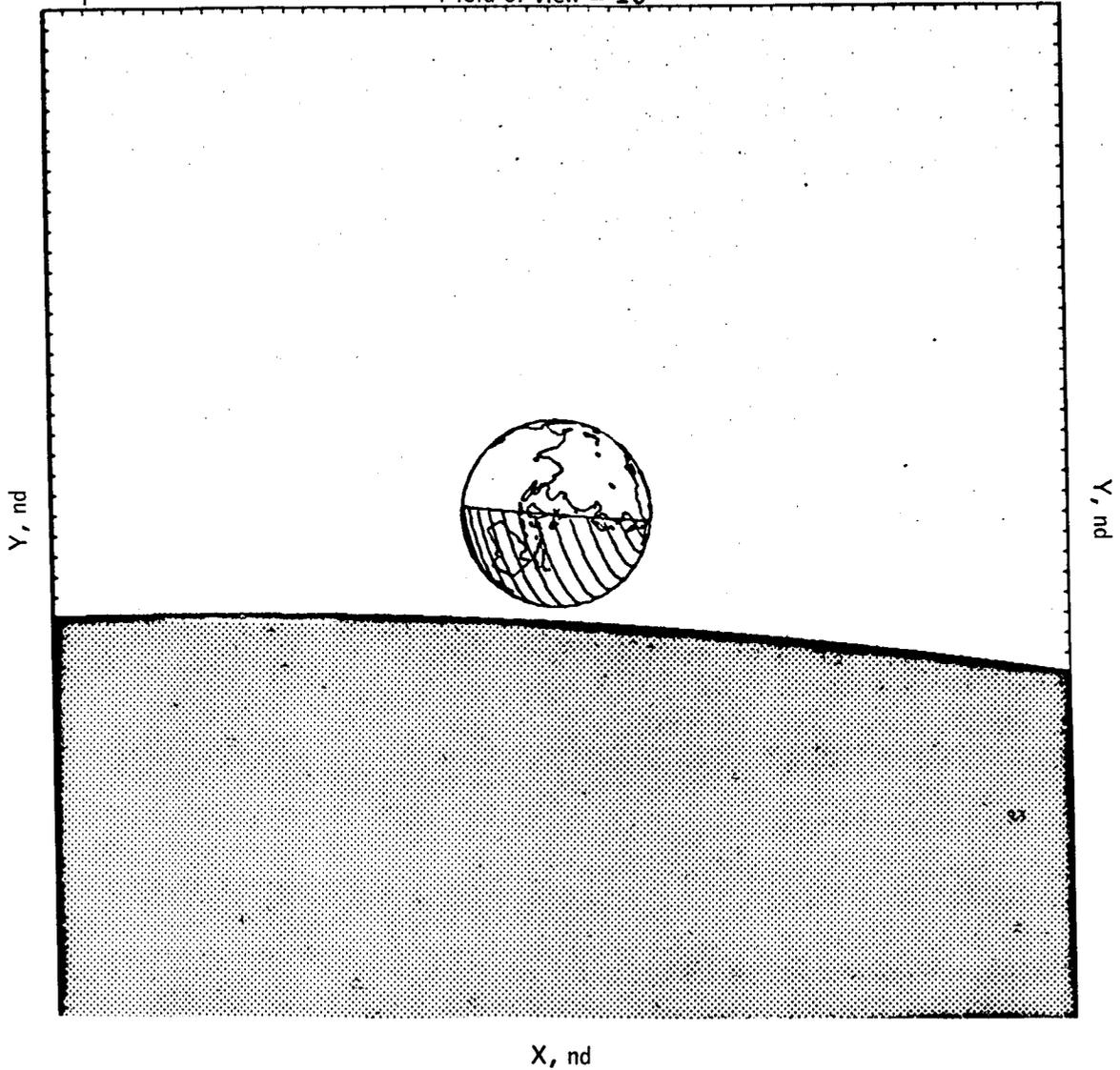
$R_M = 1117 \text{ n. mi.}$

$V_i = 8612 \text{ fps}$

$h_M = 205 \text{ stat. mi.}$

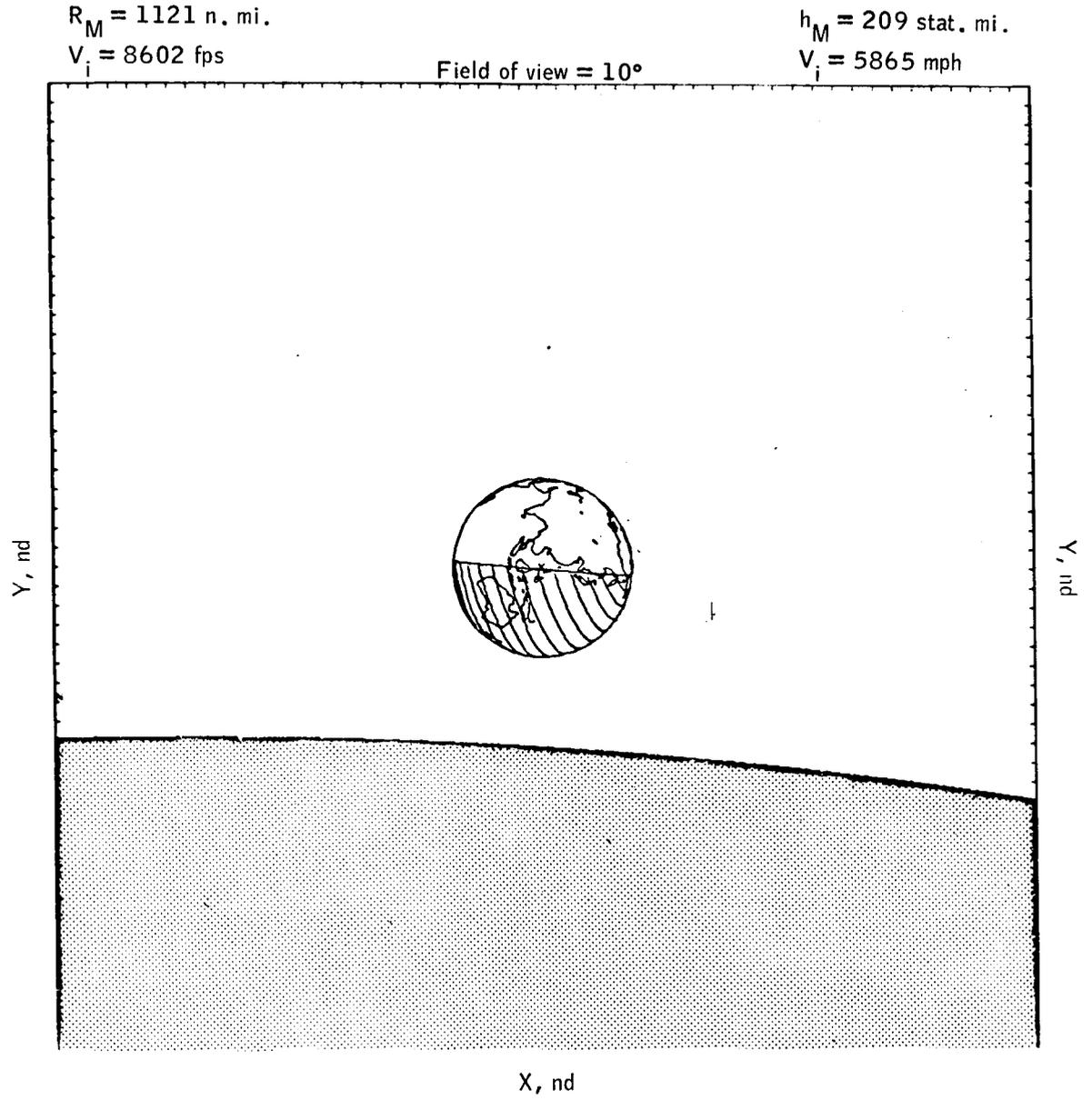
$V_i = 5872 \text{ mph}$

Field of view = 10°



(c) G.e.t. = 137:29:25.7.

Figure 14.- Continued.



(d) G.e.t. = 137:29:32.9.

Figure 14.- Concluded.

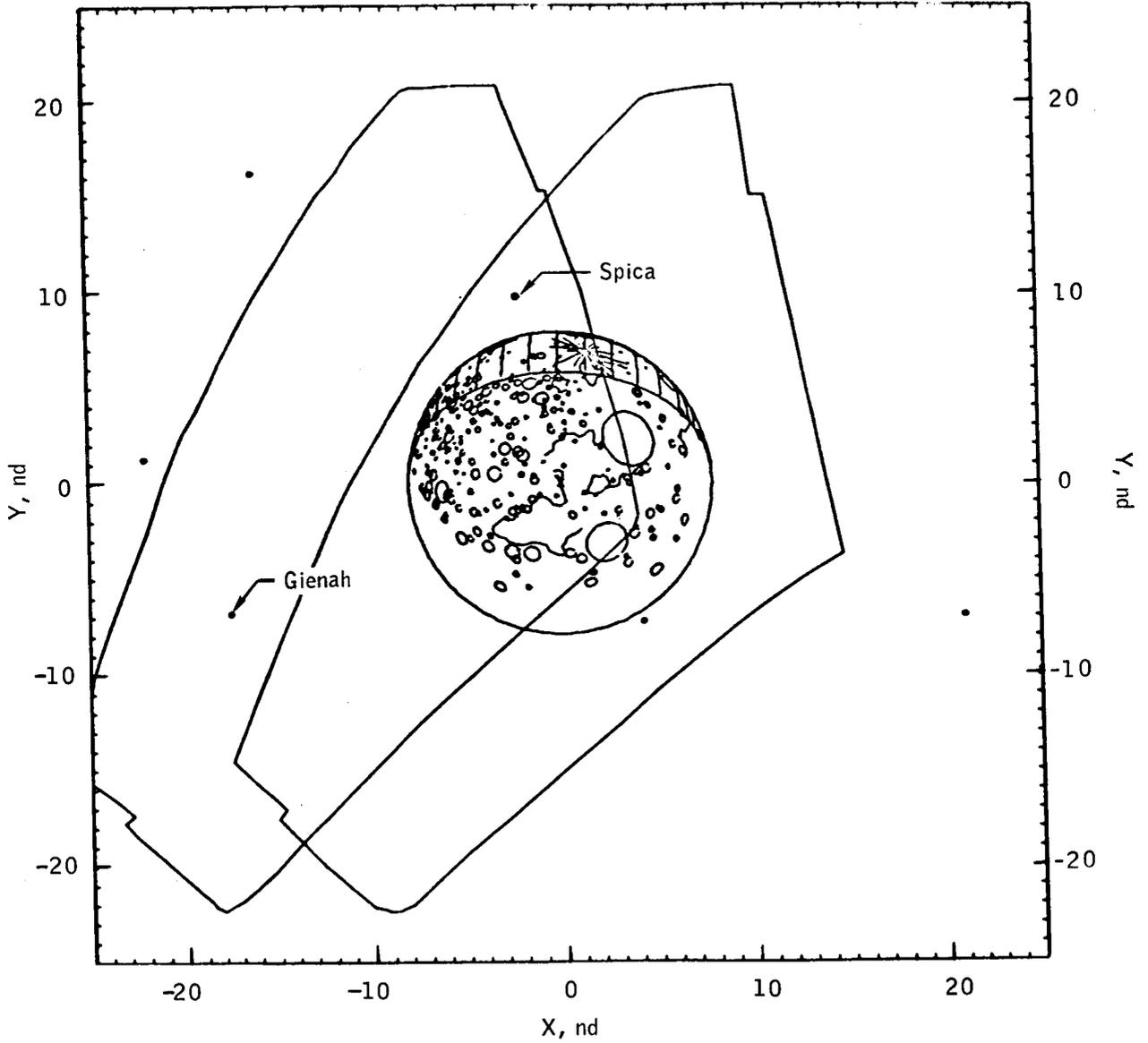
MOON VIEWS

SEQ	551	566	570	582	593	595
X	-17	-21	4	21	-2	-15
Y	-6	1	-7	-6	9	16

$R_M = 8528$ n. mi.
 $V_i = 5462$ fps

$h_M = 8724$ stat. mi.
 $V_i = 3724$ mph

Field of view = 40°



(a) G.e.t. = 140 hours.

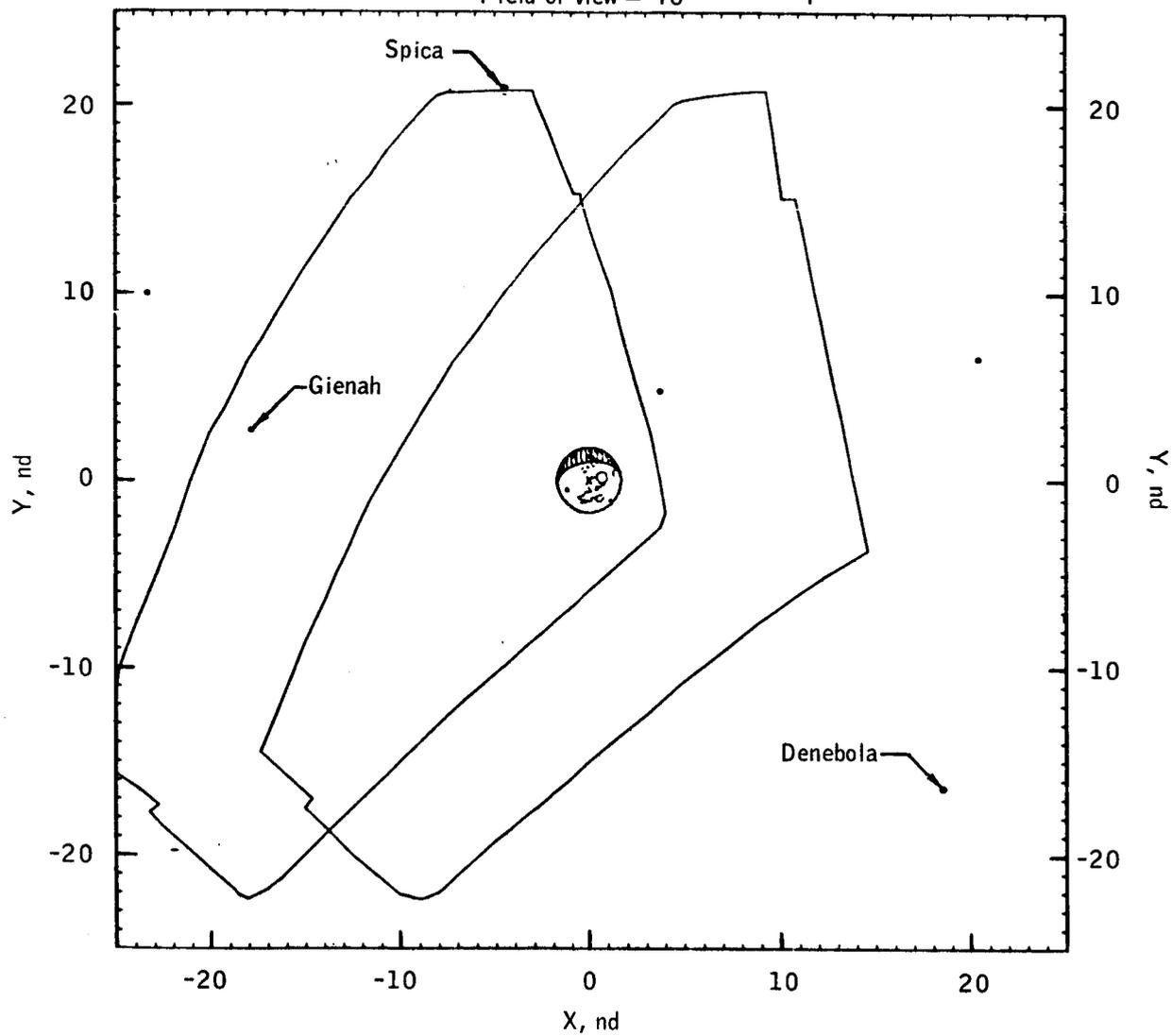
Figure 15.- Transearth coast-constant field of view (moon).

SEG	535	551	566	570	582	593
X	18	-17	-23	3	20	4
Y	-16	2	10	4	6	21

 $R_E = 179\,288$ n. mi.

 $V_i = 4876$ fps

 $h_E = 202\,358$ stat. mi.

 $V_i = 3324$ mph
Field of view = 40° 

(b) G.e.t. = 150 hours.

Figure 15.- Continued.

SEG	535	551	566	570	582	593
X	16	-17	-22	4	20	-2
Y	-15	6	14	6	6	23

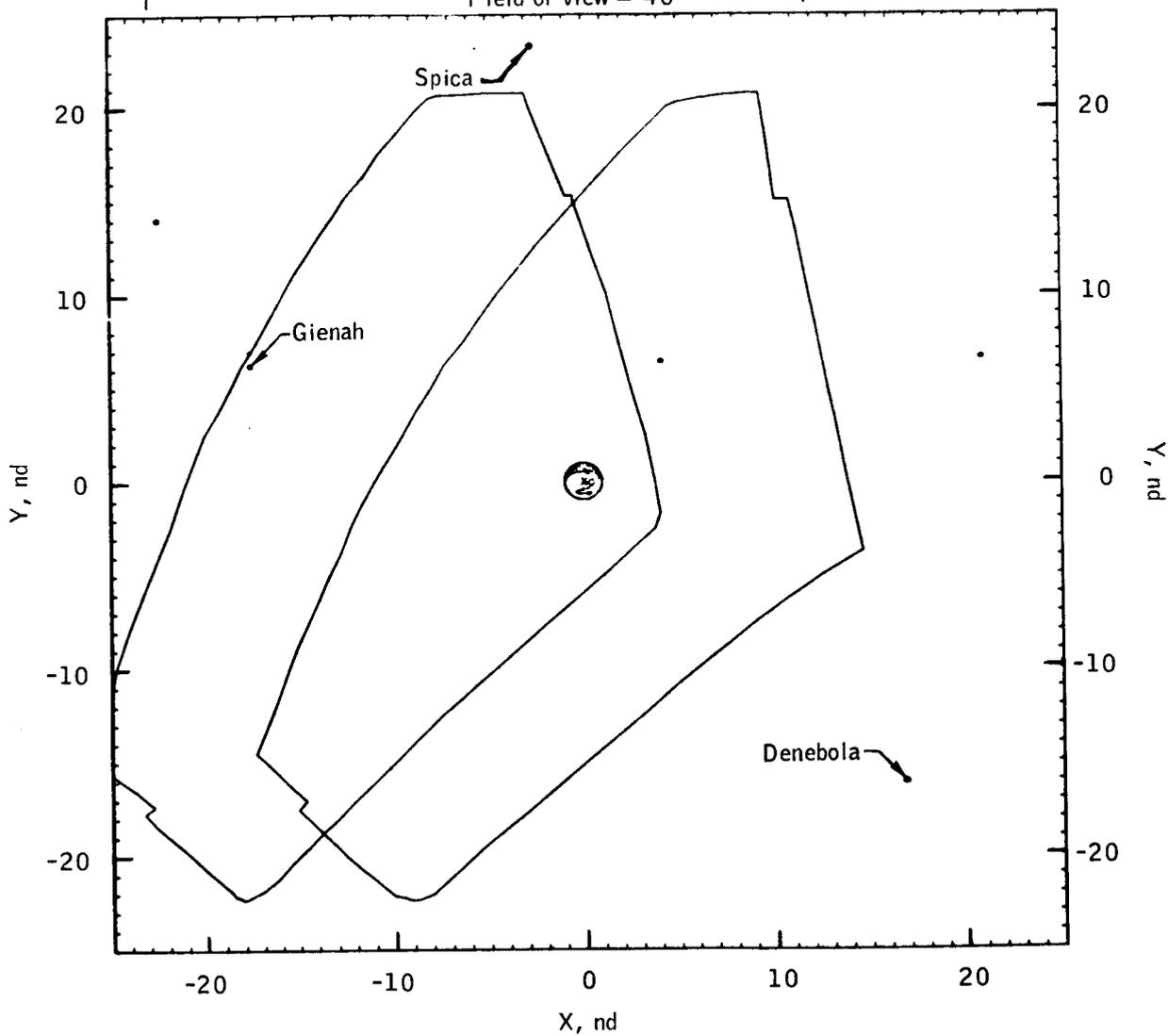
$R_E = 149\,473$ n. mi.

$h_E = 168\,046$ stat. mi.

$V_i = 5338$ fps

Field of view = 40°

$V_i = 3640$ mph



(c) G.e.t. = 160 hours.

Figure 15.- Continued.

SEQ	535	551	566	570	582
X	15	-17	-21	4	21
Y	-15	9	17	7	7

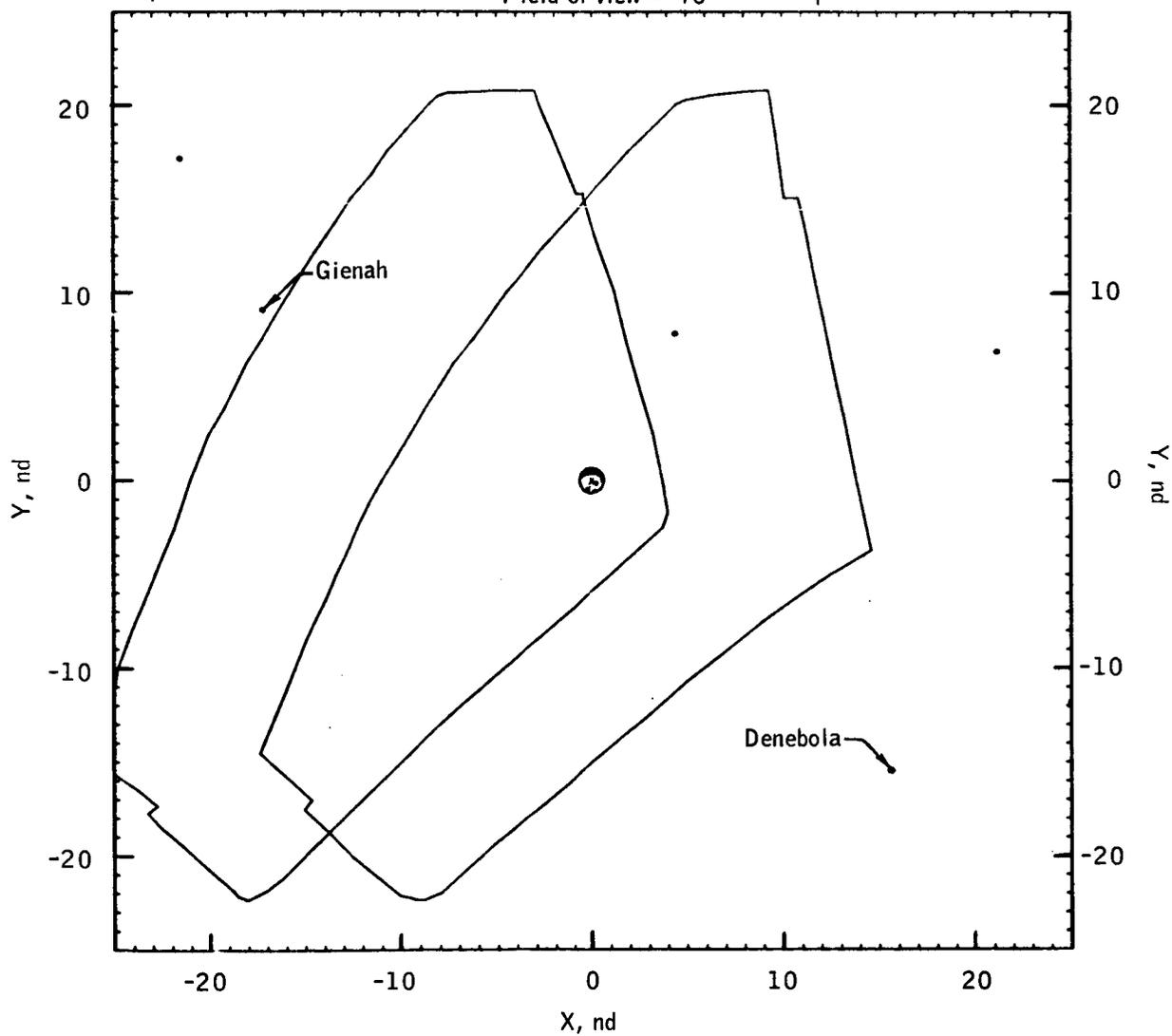
$R_E = 116\,265$ n. mi.

$h_E = 129\,832$ stat. mi.

$V_i = 6097$ fps

$V_i = 4157$ mph

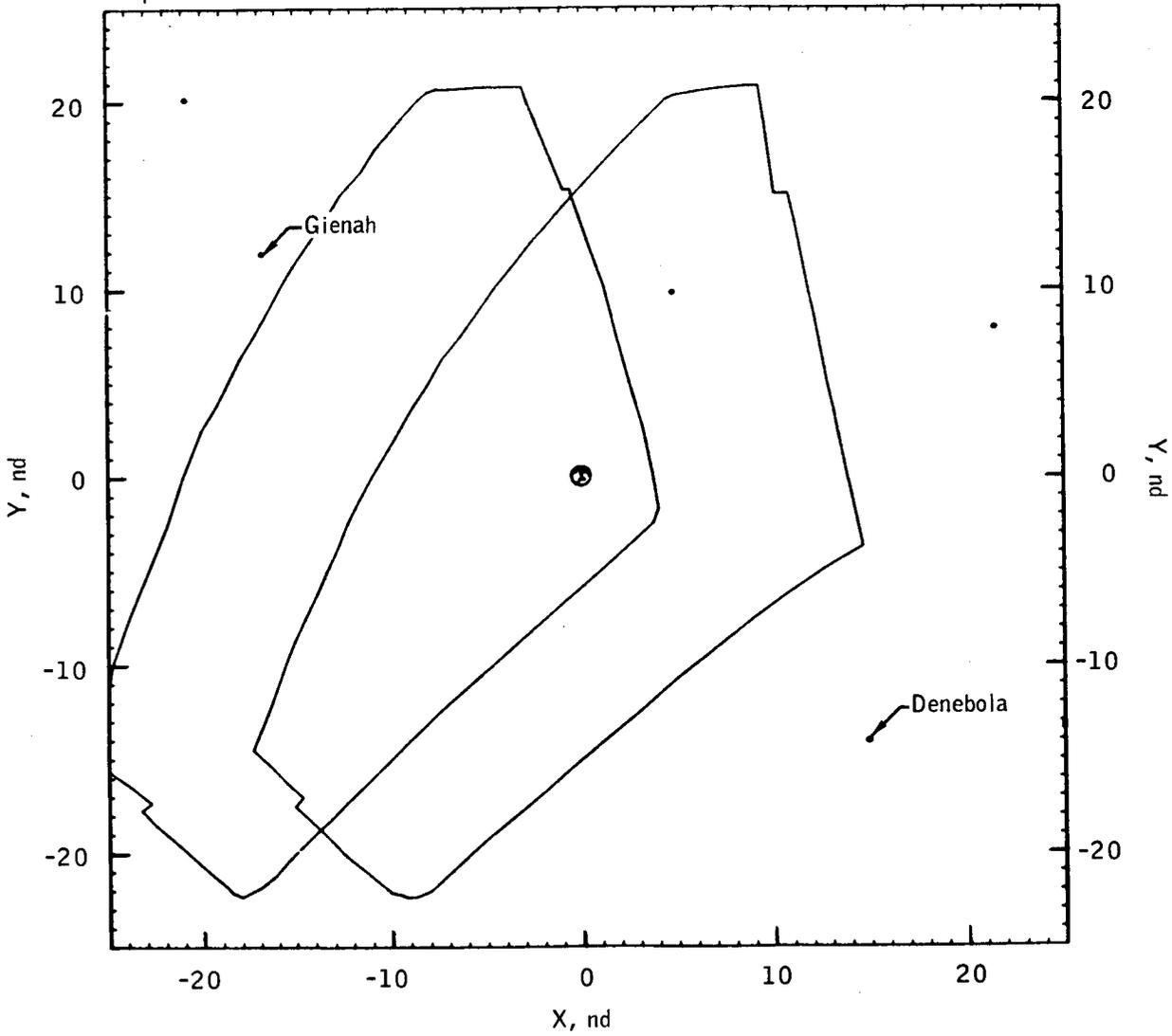
Field of view = 40°



(d) G.e.t. = 170 hours.

Figure 15.- Continued.

SEC	535	551	566	570	582
X	14	-16	-20	4	21
Y	-13	12	20	9	8

 $R_E = 77\,138 \text{ n. mi.}$
 $V_i = 7571 \text{ fps}$
 $h_E = 84\,807 \text{ stat. mi.}$
 $V_i = 5162 \text{ mph}$
Field of view = 40° 

(e) G.e.t. = 180 hours.

Figure 15.- Continued.

SEG	515	535	551	566	570	5A2
X	15	14	-16	-20	5	21
Y	-24	-11	15	23	12	10

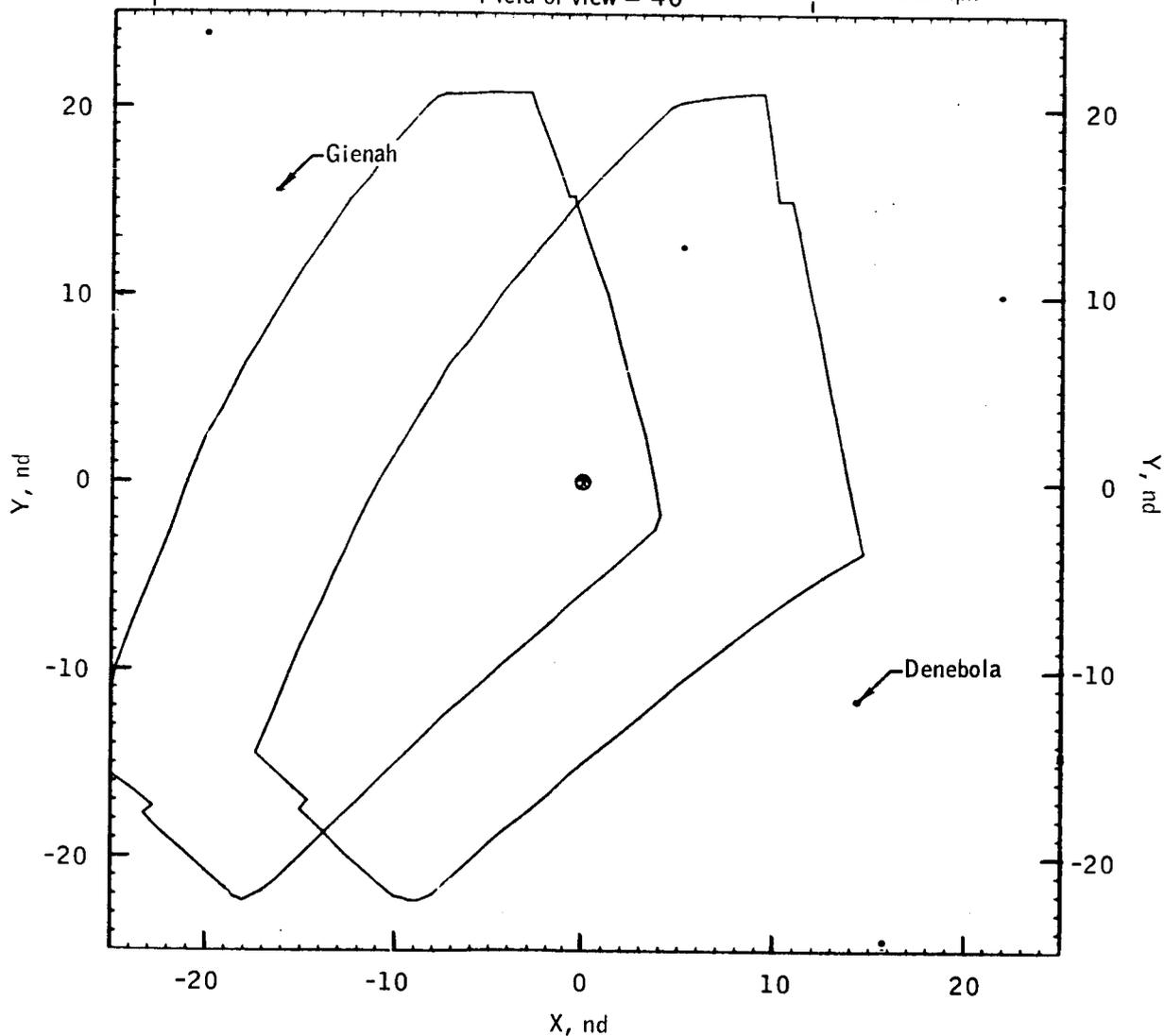
$R_E = 22\,296$ n. mi.

$V_i = 14\,318$ fps

$h_M = 25\,658$ stat. mi.

$V_i = 9762$ mph

Field of view = 40°



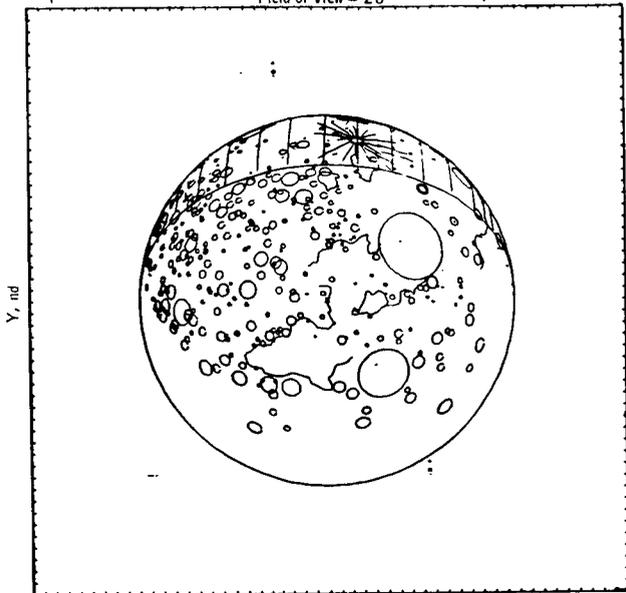
(f) G.e.t. = 190 hours.

Figure 15.- Concluded.

$R_M = 8528$ n. mi.
 $V_i = 5462$ fps

$h_M = 8734$ stat. mi.
 $V_i = 3724$ mph

Field of view = 20°



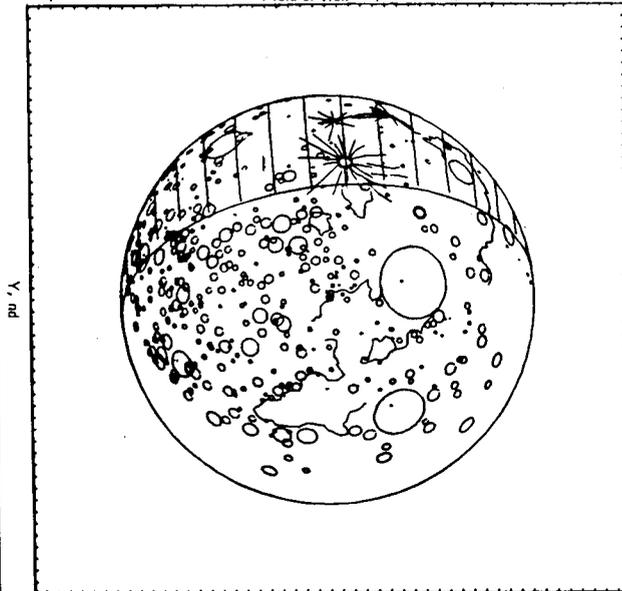
X, nd

(a) G.e.t. = 140 hours..

$R_E = 179288$ n. mi.
 $V_i = 4876$ fps

$h_E = 202358$ stat. mi.
 $V_i = 3324$ mph

Field of view = 4°



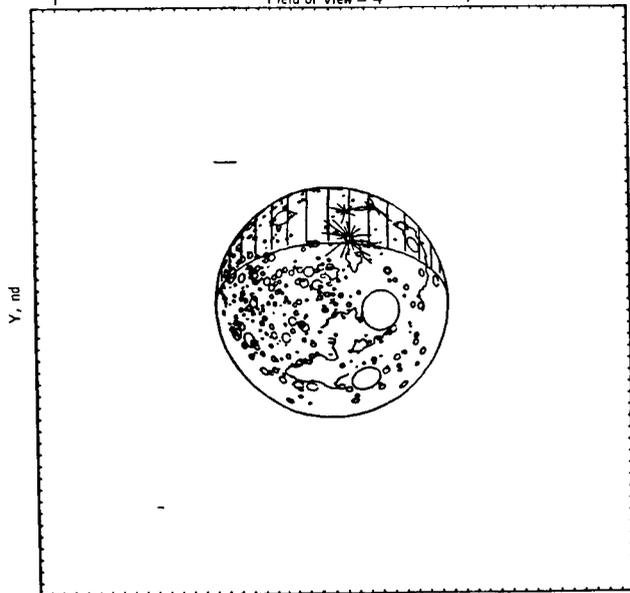
X, nd

(b) G.e.t. = 150 hours.

$R_E = 149473$ n. mi.
 $V_i = 5338$ fps

$h_E = 168046$ stat. mi.
 $V_i = 3640$ mph

Field of view = 4°



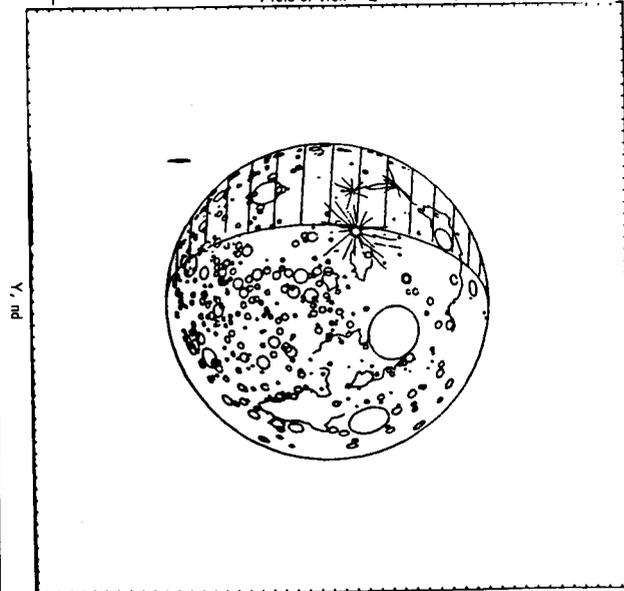
X, nd

(c) G.e.t. = 160 hours.

$R_E = 116265$ n. mi.
 $V_i = 6097$ fps

$h_E = 129832$ stat. mi.
 $V_i = 4157$ mph

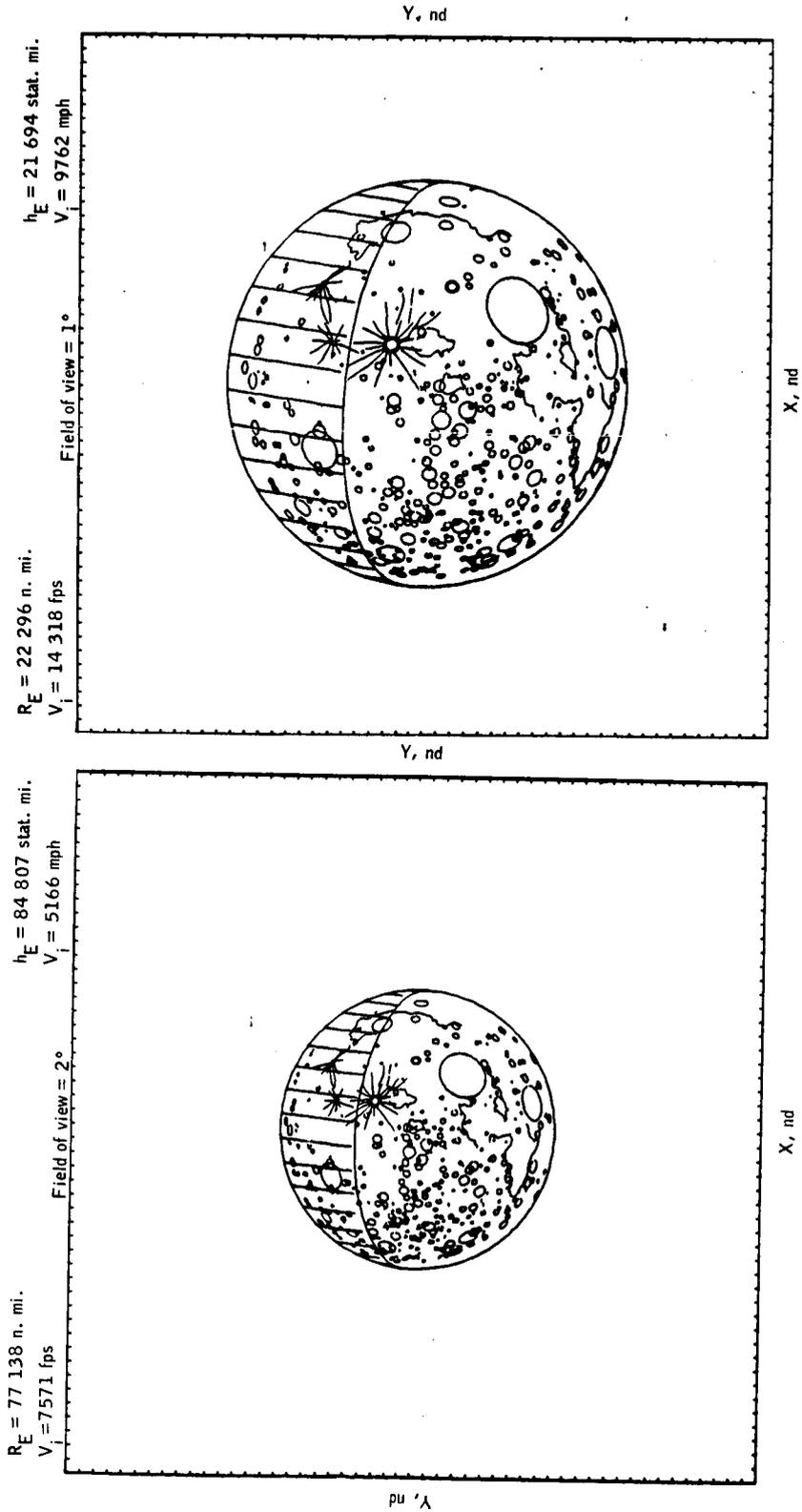
Field of view = 2°



X, nd

(d) G.e.t. = 170 hours.

Figure 16. - Transearth coast variable field of view (moon).



(e) G.e.t. = 180 hours.

(f) G.e.t. = 190 hours.

Figure 16. - Concluded.

SEC 990 1041
 X 0 23
 Y 12 0

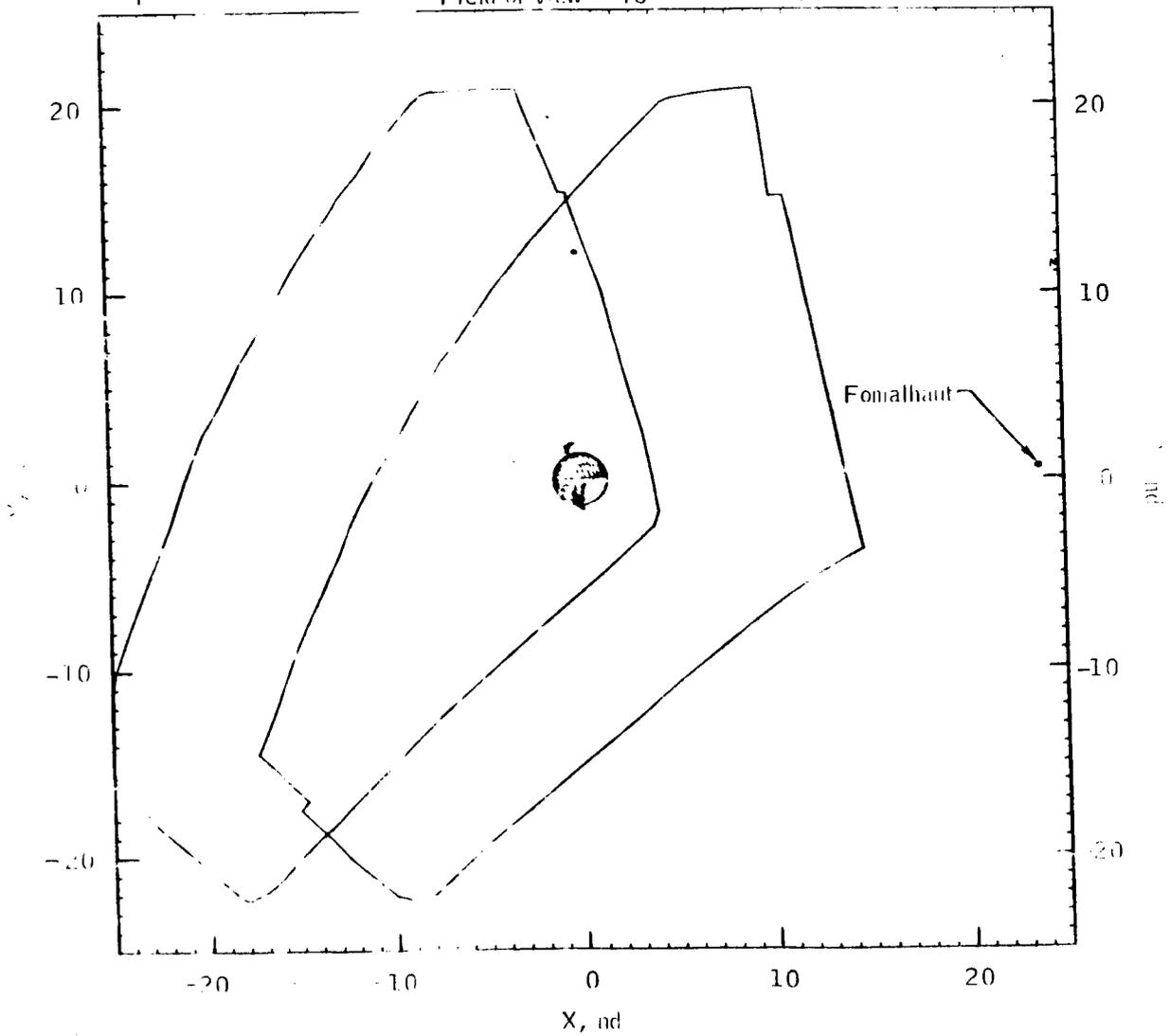
$R_E = 179\,288$ n. mi.

$V_i = 4876$ fps

$h_E = 202\,358$ stat. mi.

$V_i = 3324$ mph

Field of view = 40°



) G.e.t. = 150 hours.

Figure 17. Trans-earth coast-constant field of view (earth).

SEQ 990 1091
X 0 23
Y 14 2

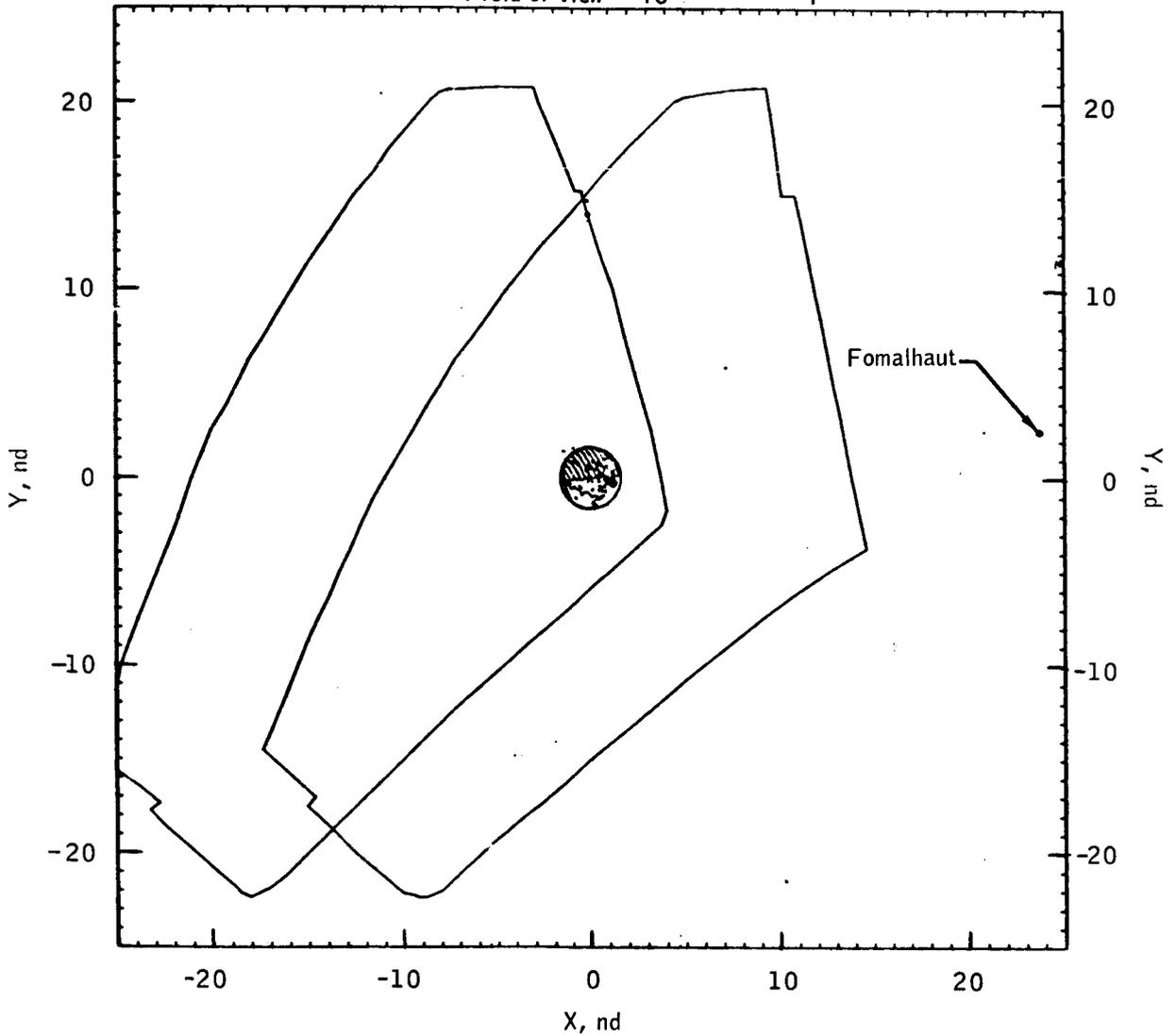
$R_E = 149\,473$ n. mi.

$V_i = 5338$ fps

$h_E = 168\,046$ stat. mi.

$V_i = 3640$ mph

Field of view = 40°



(b) G.e.t. = 160 hours.

Figure 17.- Continued.

SEQ 990 1041
 X 0 23
 Y 17 5

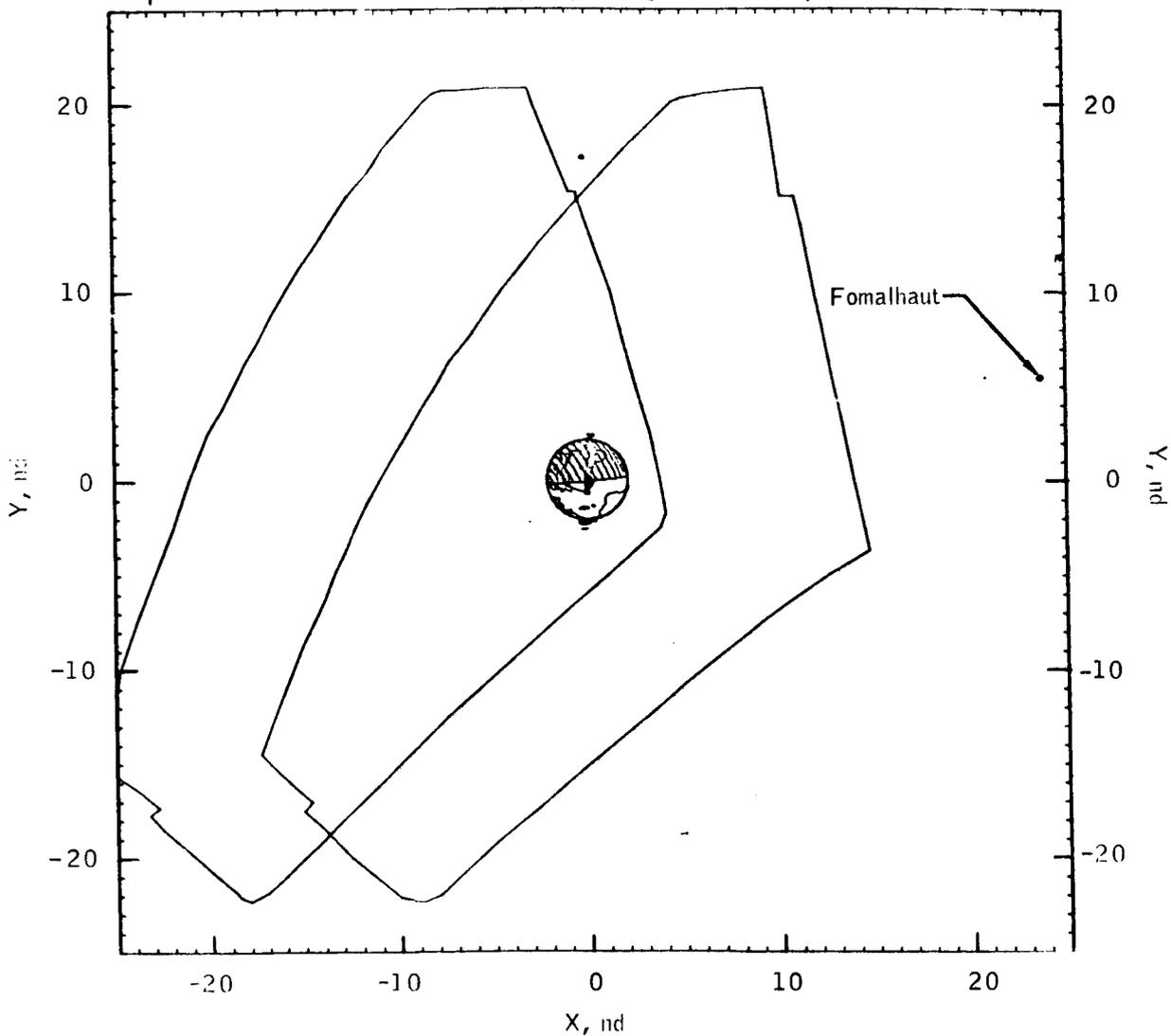
$R_E = 116\,265$ n. mi.

$V_i = 6097$ fps

$h_E = 129\,832$ stat. mi.

$V_i = 4157$ mph

Field of view = 40°



(c) G.c.t. = 170 hours.

Figure 17.- Continued.

SEQ 990 1041
 X 0 23
 Y 23 11

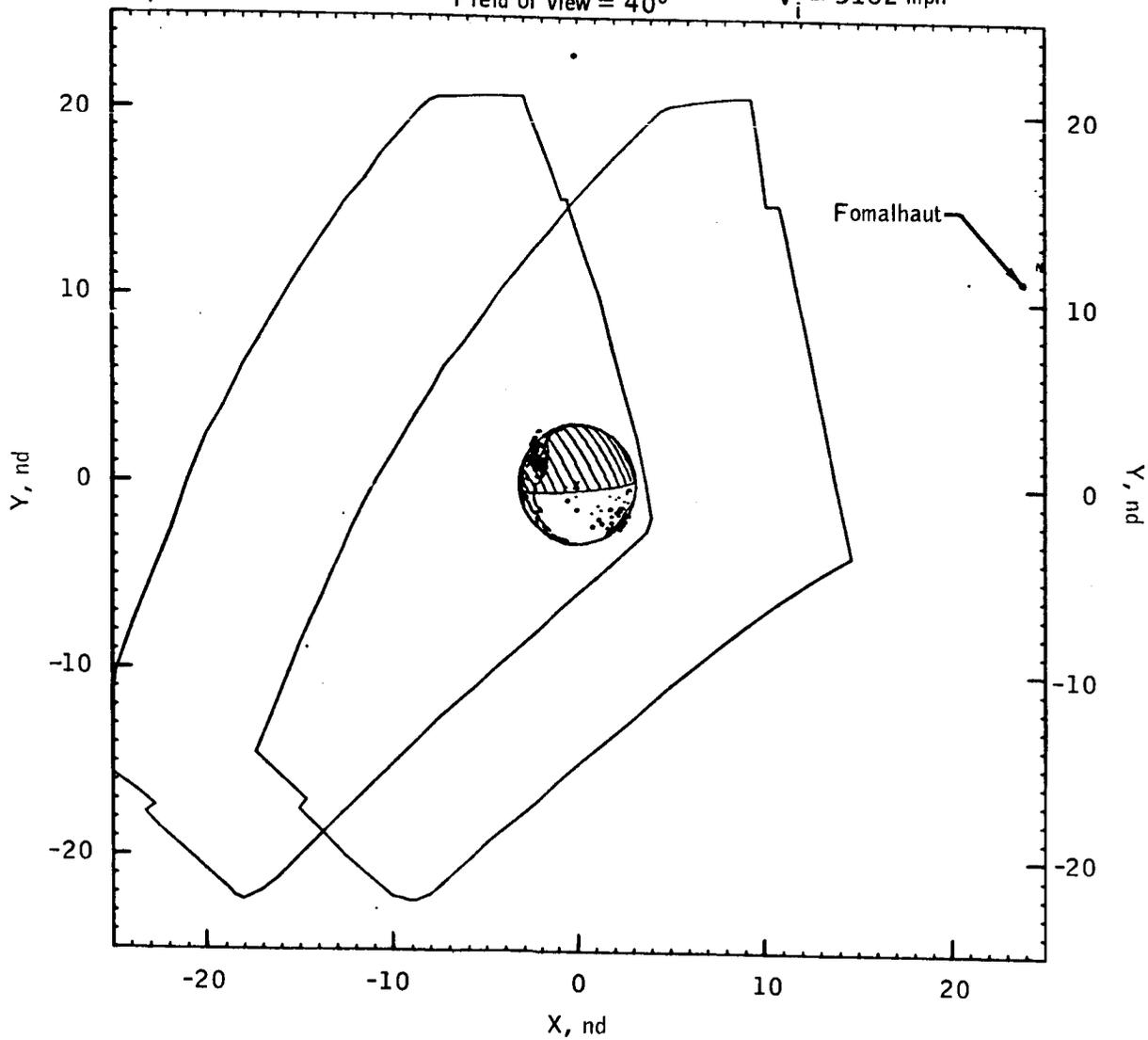
$R_E = 77\,138$ n. mi.

$V_i = 7571$ fps

$h_E = 84\,807$ stat. mi.

$V_i = 5162$ mph

Field of view = 40°



(d) G.e.t. = 180 hours.

Figure 17.- Continued.

SEQ 7 117
 X -15 2
 Y -7 -18

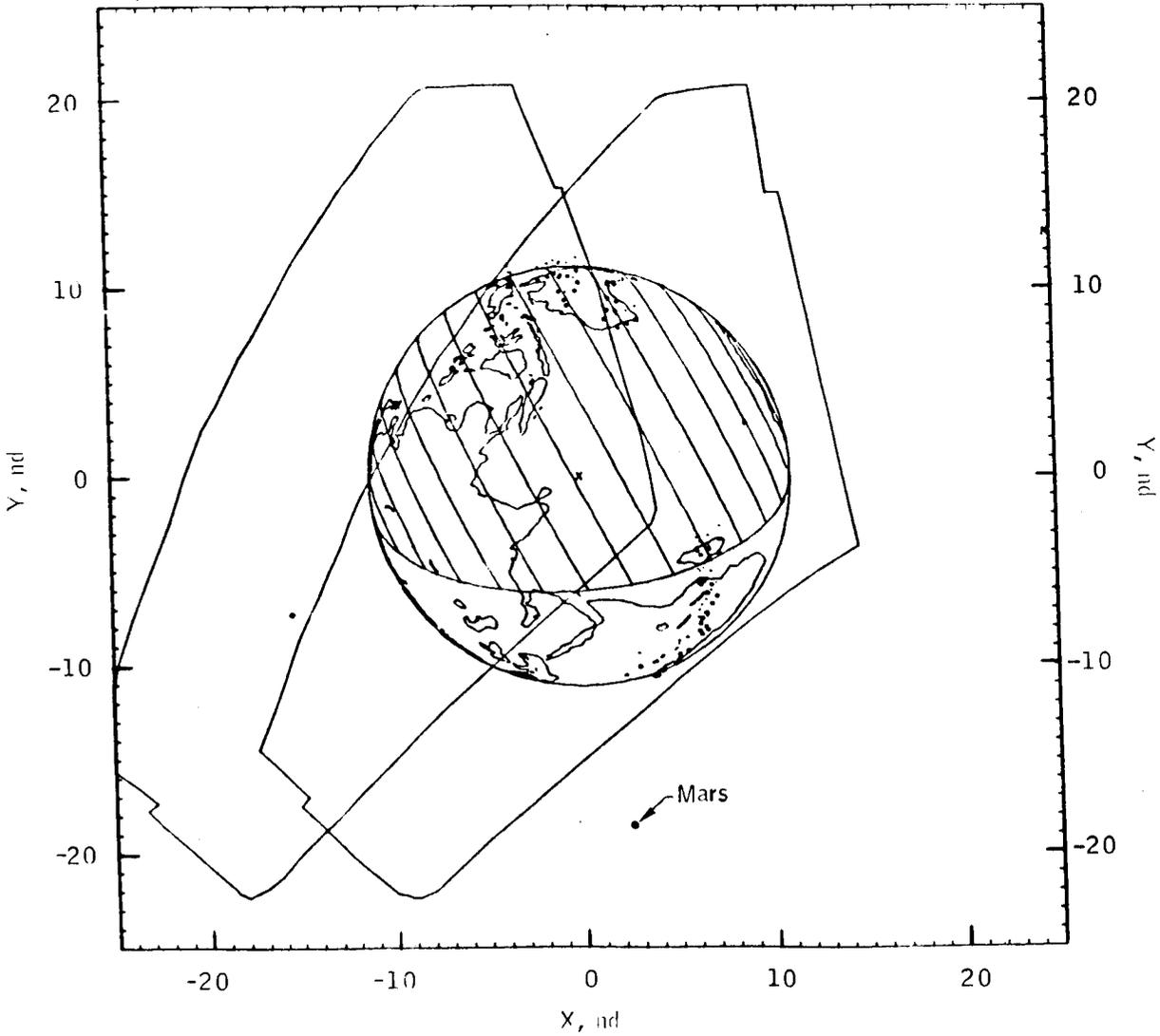
$R_E = 22\,296$ n. mi.

$h_E = 25\,658$ stat. mi.

$V_i = 14\,318$ fps

$V_i = 9762$ mph

Field of view = 40°



(e) G.c.t. = 190 hours.

Figure 17.- Concluded.

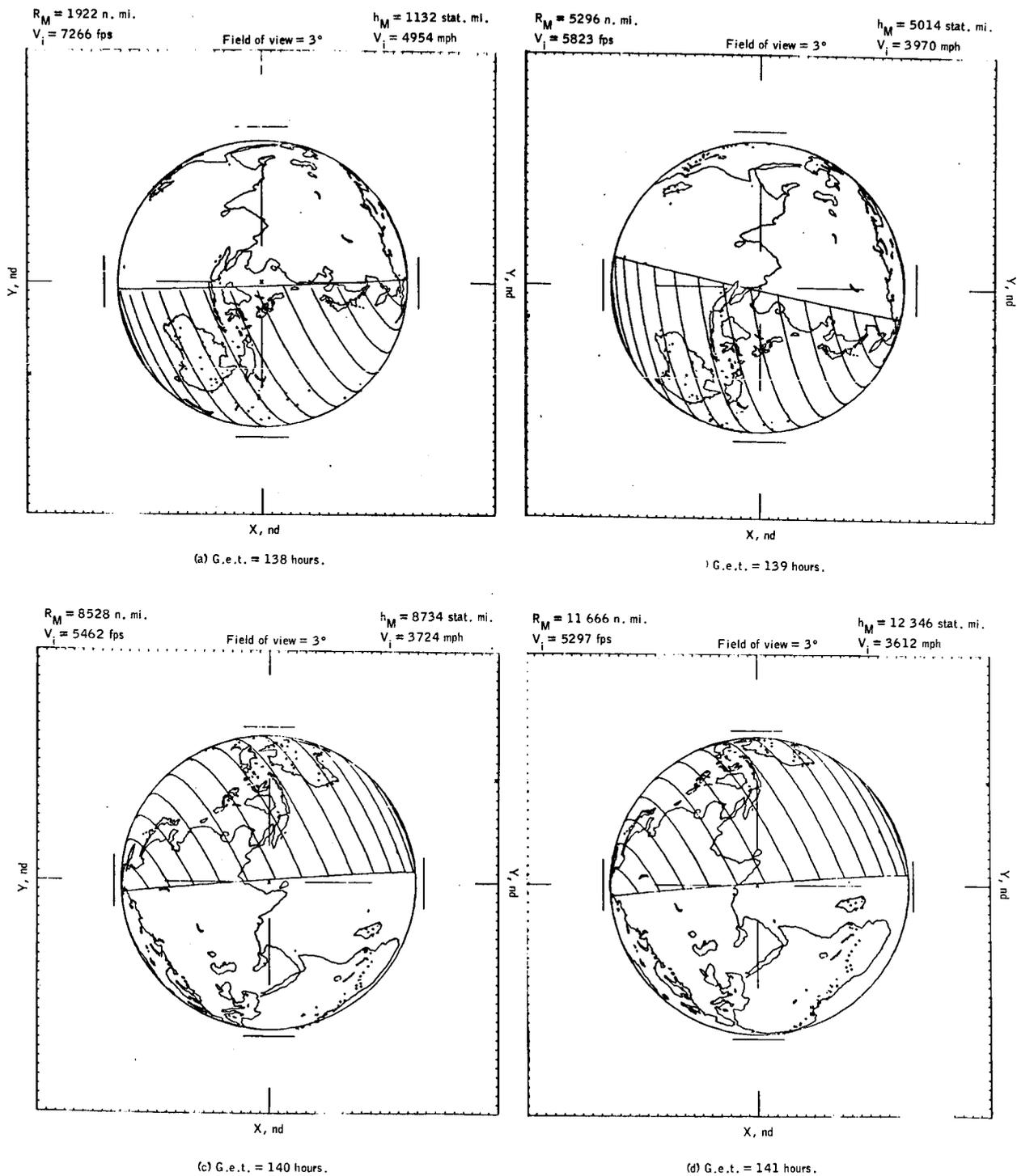
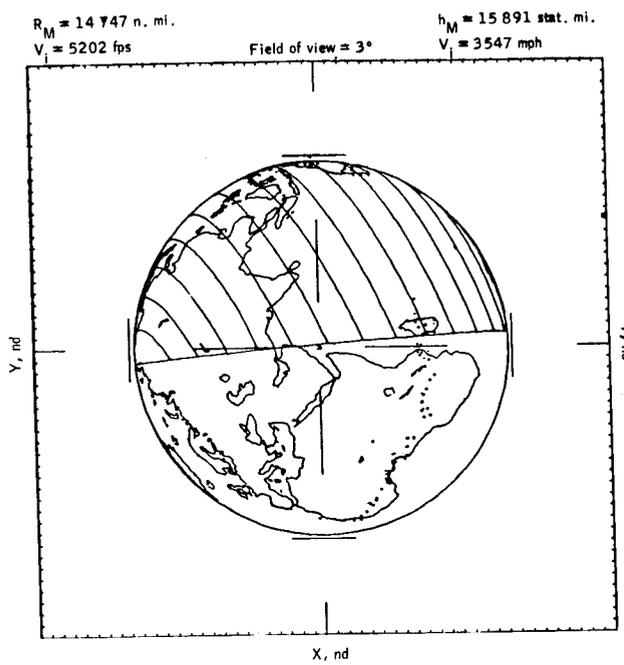
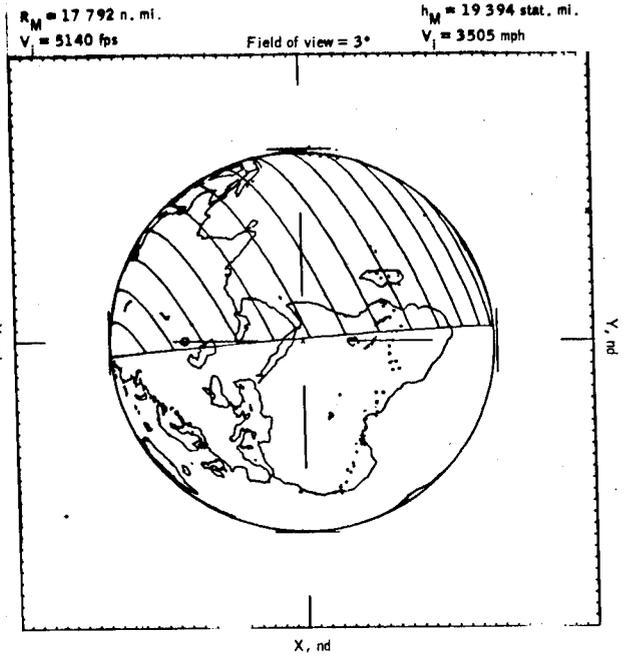


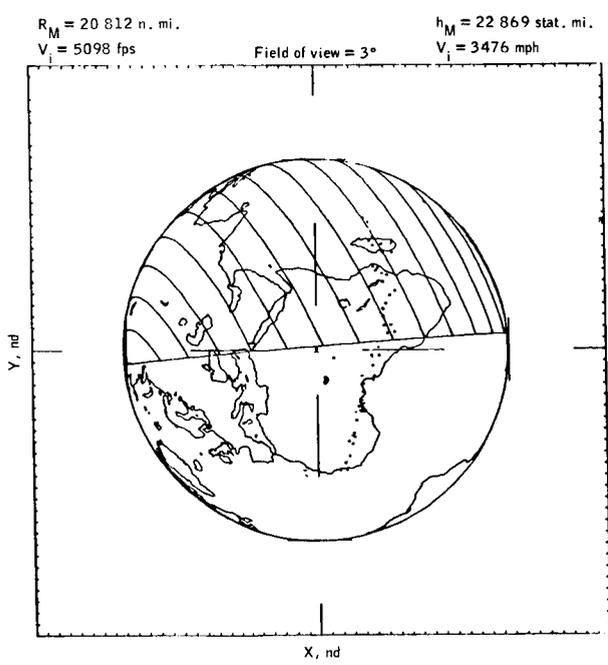
Figure 18. - Transearth coast - variable field of view (earth).



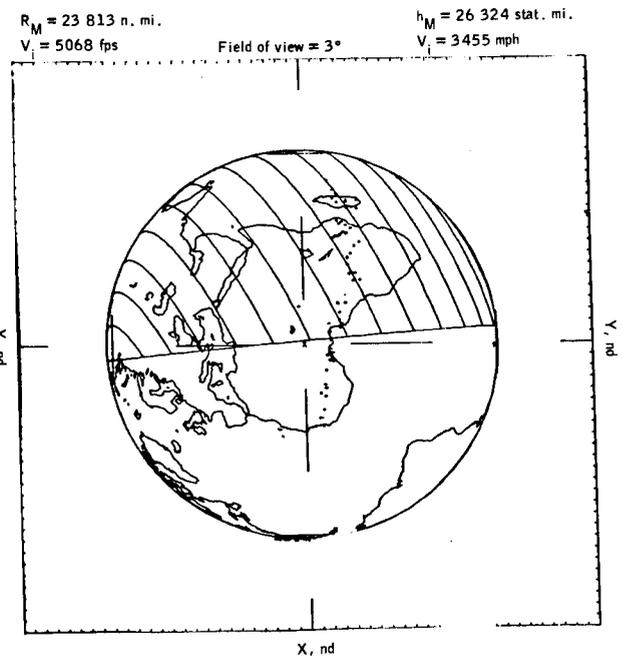
(e) G.e.t. = 142 hours.



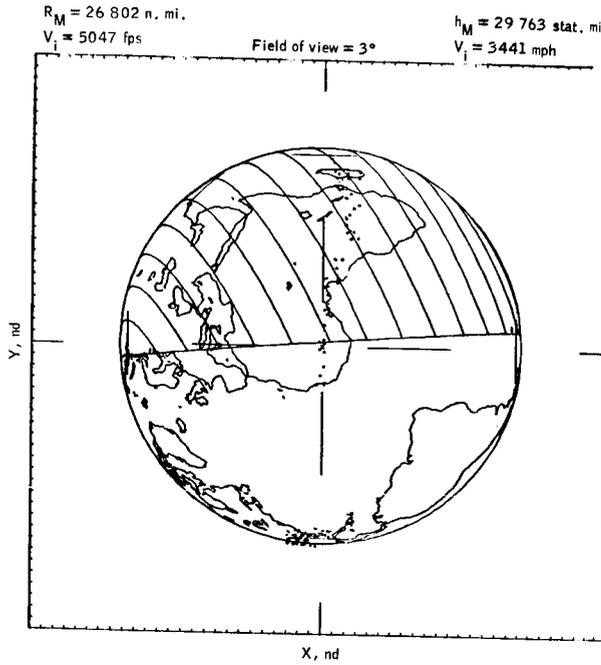
(f) G.e.t. = 143 hours.



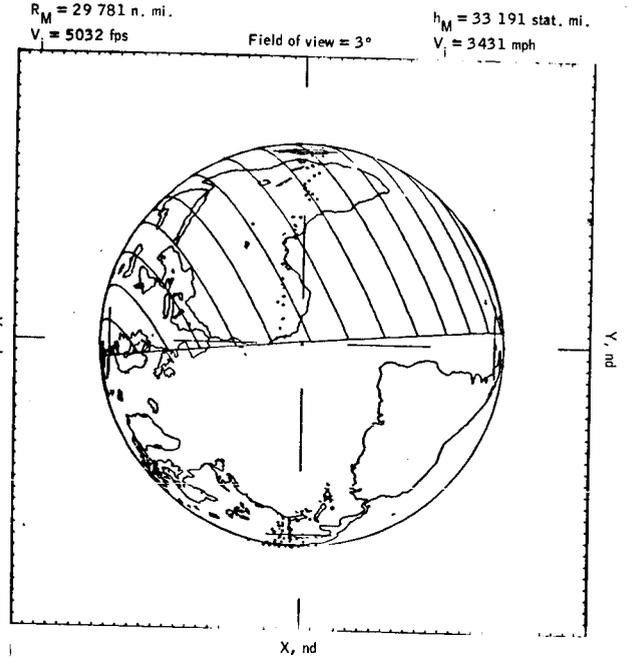
(g) G.e.t. = 144 hours.



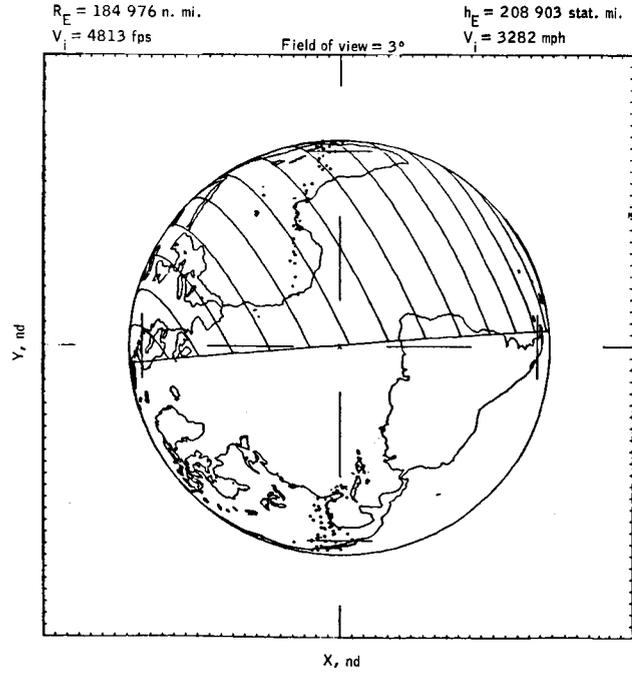
(h) G.e.t. = 145 hours.



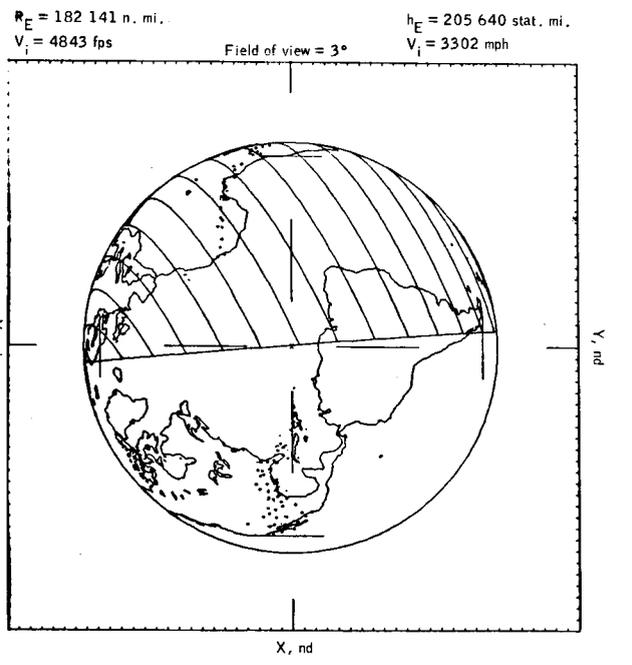
(i) G.e.t. = 146 hours.



(j) G.e.t. = 147 hours.



(k) G.e.t. = 148 hours.

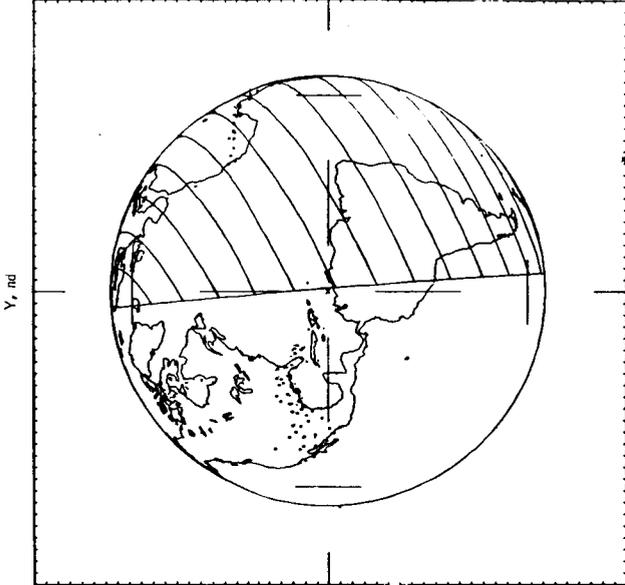


(l) G.e.t. = 149 hours.

Figure 18.- Continued.

$R_E = 179\ 288$ n. mi. $h_E = 202\ 358$ stat. mi.
 $V_i = 4876$ fps $V_i = 3\ 224$ mph

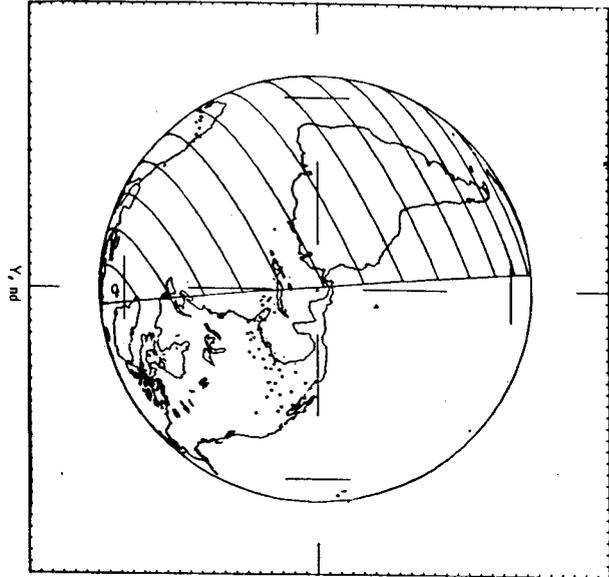
Field of view = 3°



(m) G.e.t. = 150 hours.

$R_E = 176\ 416$ n. mi. $h_E = 199\ 053$ stat. mi.
 $V_i = 4911$ fps $V_i = 3\ 348$ mph

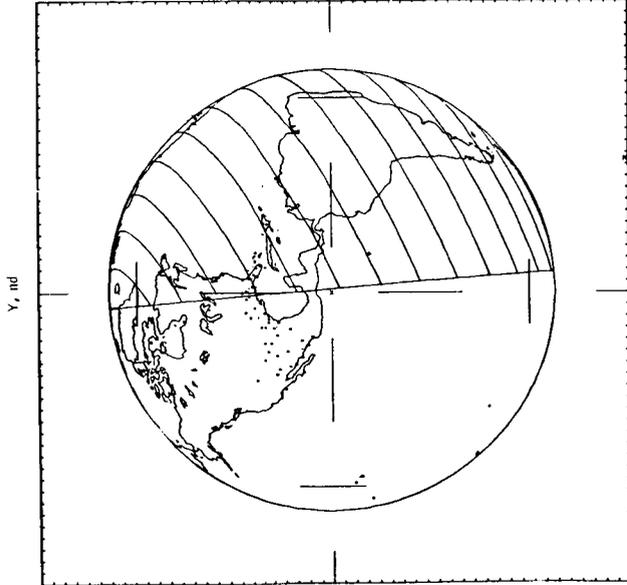
Field of view = 3°



(n) G.e.t. = 151 hours.

$R_E = 173\ 523$ n. mi. $h_E = 195\ 724$ stat. mi.
 $V_i = 4949$ fps $V_i = 3\ 374$ mph

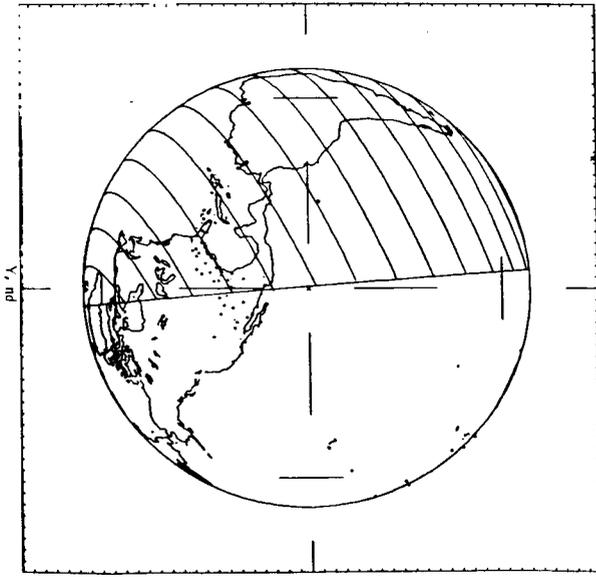
Field of view = 3°



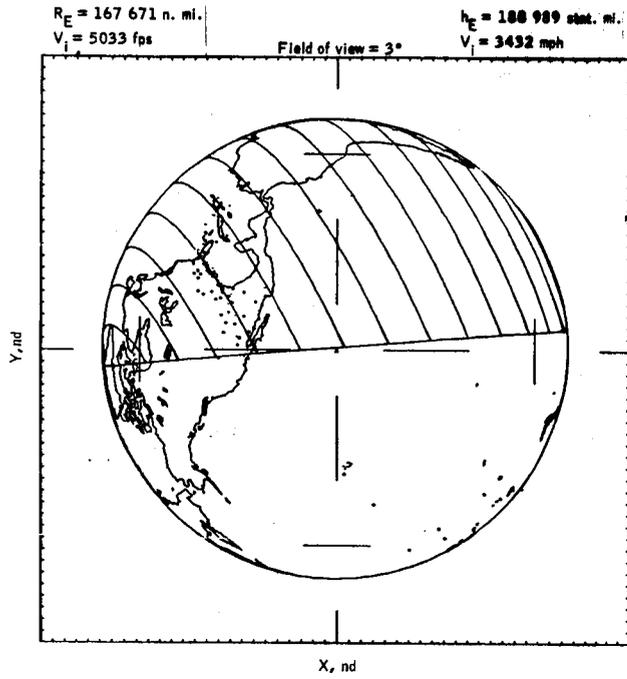
(o) G.e.t. = 152 hours.

$R_E = 170\ 609$ n. mi. $h_E = 192\ 370$ stat. mi.
 $V_i = 4990$ fps $V_i = 3\ 402$ mph

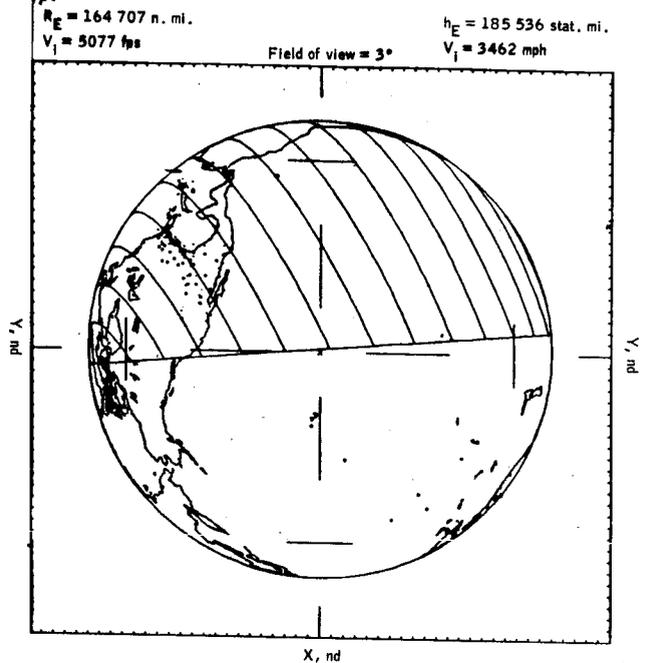
Field of view = 3°



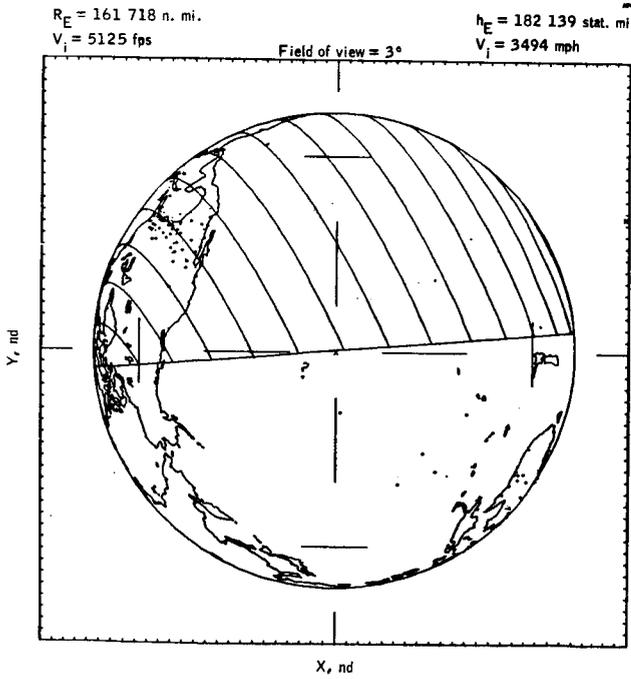
(p) G.e.t. = 153 hours.



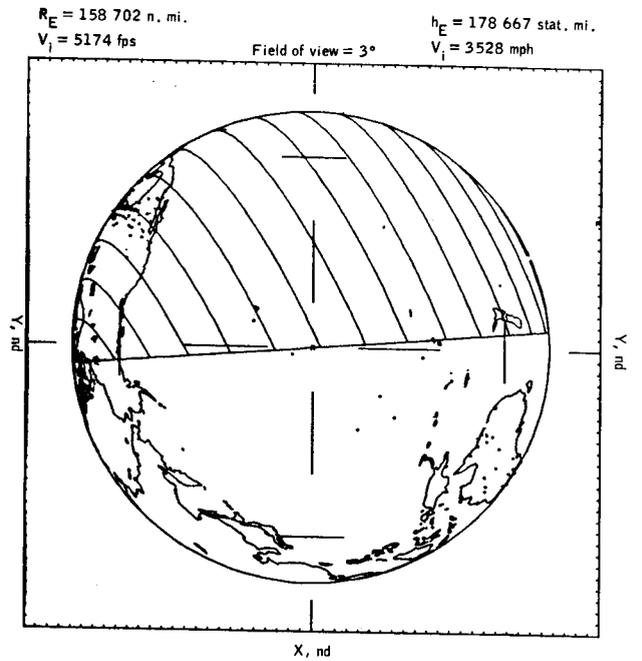
(q) G.e.t. = 154 hours.



(r) G.e.t. = 155 hours.



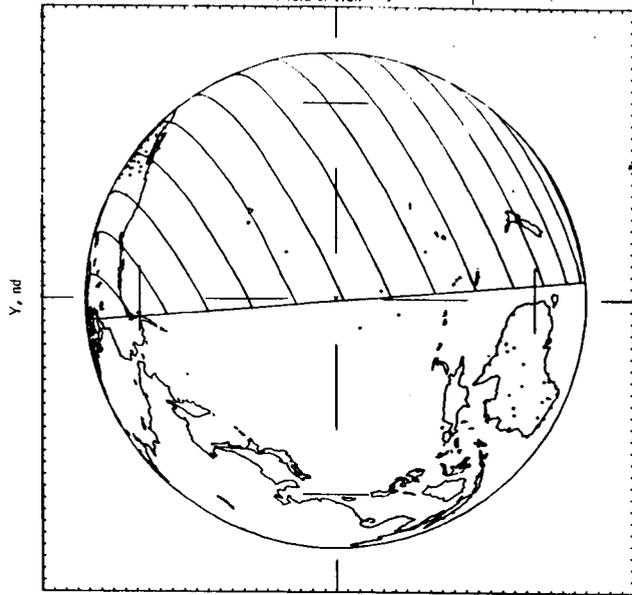
(s) G.e.t. = 156 hours.



(t) G.e.t. = 157 hours.

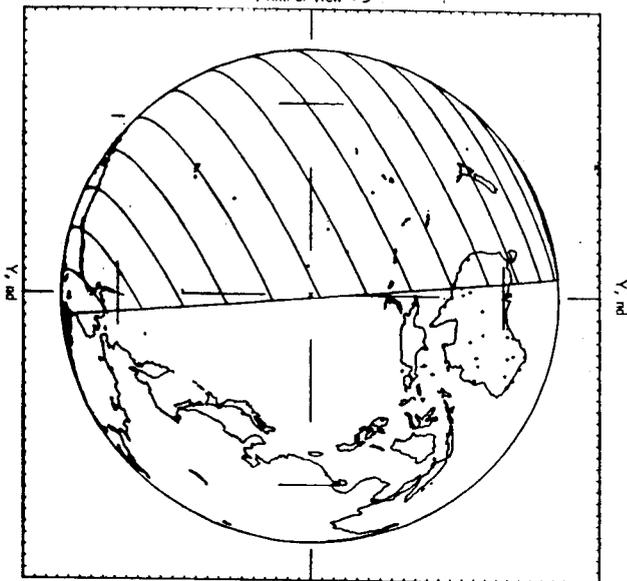
Figure 18.- Continued.

$R_E = 155\ 656$ n. mi. $h_E = 175\ 163$ stat. mi.,
 $V_i = 5226$ fps $V_i = 3563$ mph



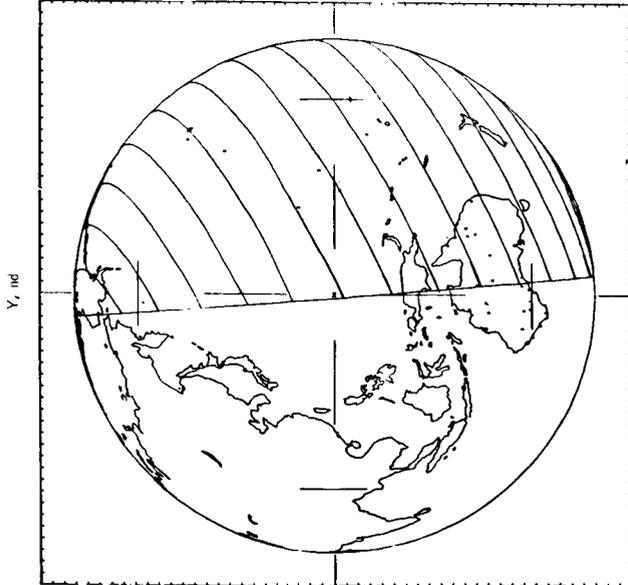
(u) G.e.t. = 158 hours.

$R_E = 152\ 580$ n. mi. $h_E = 175\ 163$ stat. mi.,
 $V_i = 5280$ fps $V_i = 3600$ mph



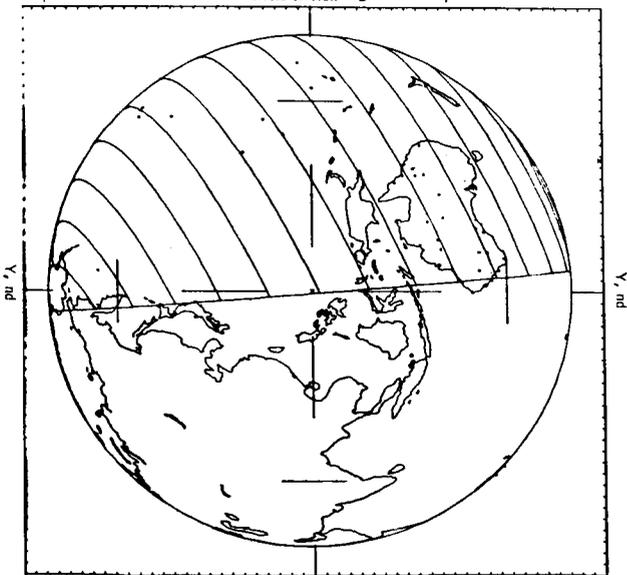
(v) G.e.t. = 159 hours.

$R_E = 149\ 473$ n. mi. $h_E = 168\ 046$ stat. mi.,
 $V_i = 5338$ fps $V_i = 3640$ mph

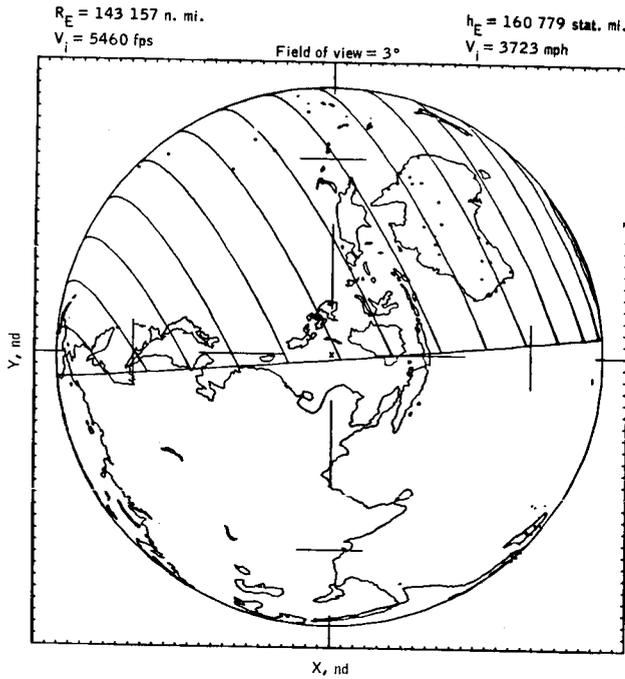


(w) G.e.t. = 160 hours.

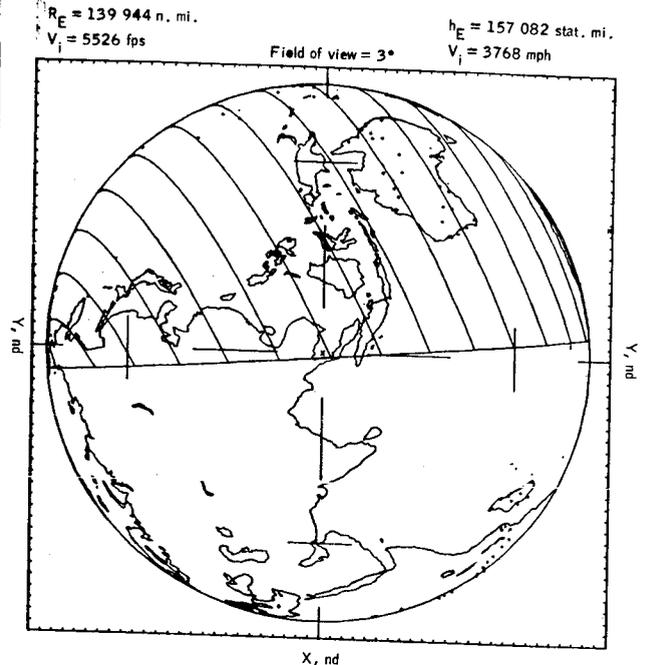
$R_E = 146\ 332$ n. mi. $h_E = 164\ 433$ stat. mi.,
 $V_i = 5398$ fps $V_i = 3680$ mph



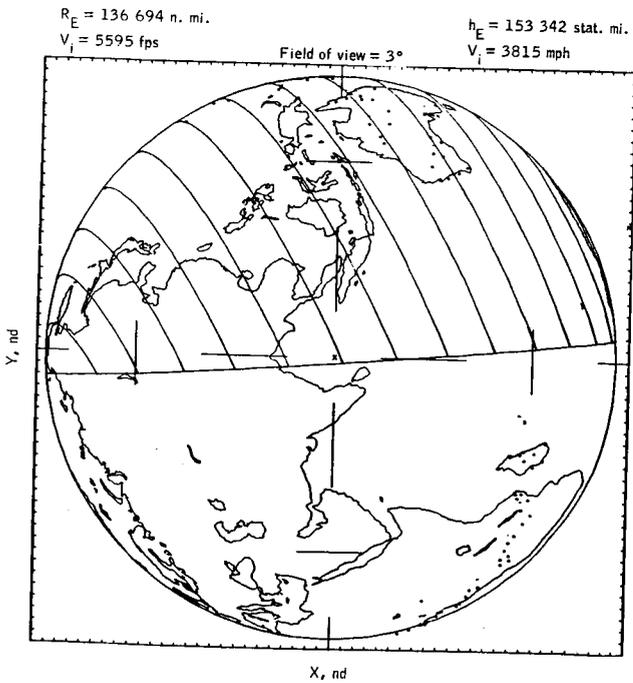
(x) G.e.t. = 161 hours.



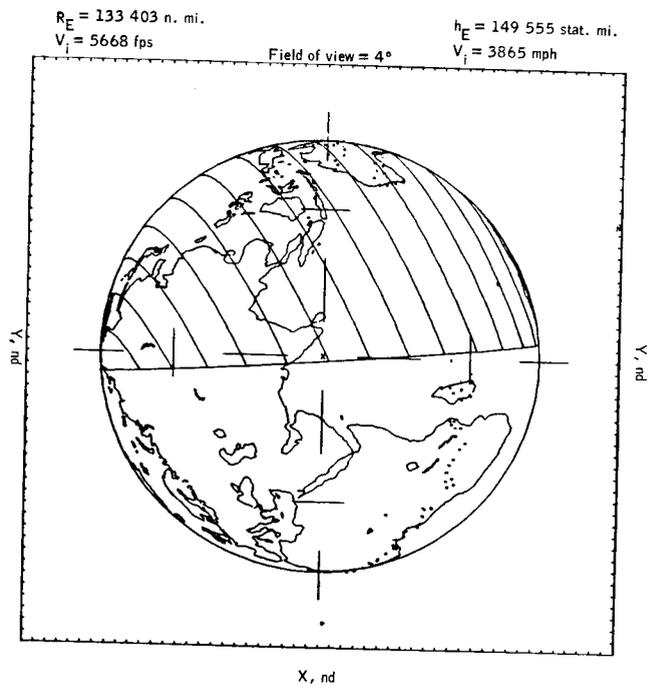
(y) G. e. t. = 162 hours.



(z) G. e. t. = 163 hours.



(aa) G. e. t. = 164 hours.

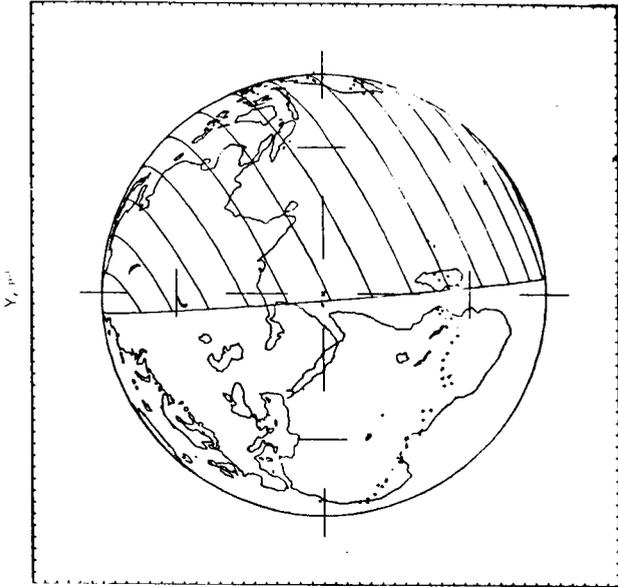


(bb) G. e. t. = 165 hours.

$R_E = 130\ 070$ n. mi.
 $V_i = 5744$ fps

$h_E = 145\ 719$ stat. mi.
 $V_i = 3916$ mph

Field of view = 4°

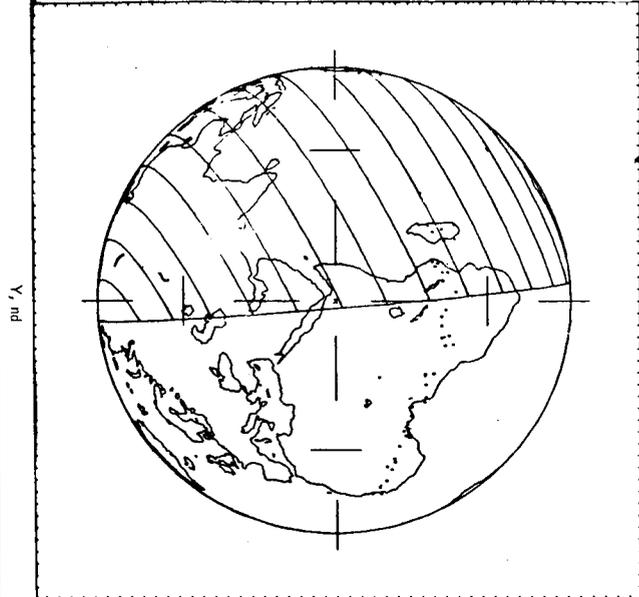


(cc) G.e.t. = 166 hours.

$R_E = 126\ 692$ n. mi.
 $V_i = 5825$ fps

$h_E = 141\ 832$ stat. mi.
 $V_i = 3972$ mph

Field of view = 4°

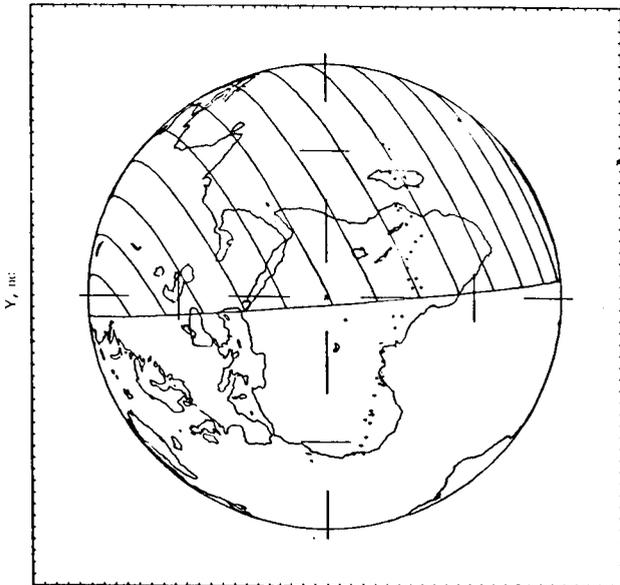


(dd) G.e.t. = 167 hours.

$R_E = 123\ 267$ n. mi.
 $V_i = 5911$ fps

$h_E = 137\ 891$ stat. mi.
 $V_i = 4030$ mph

Field of view = 4°

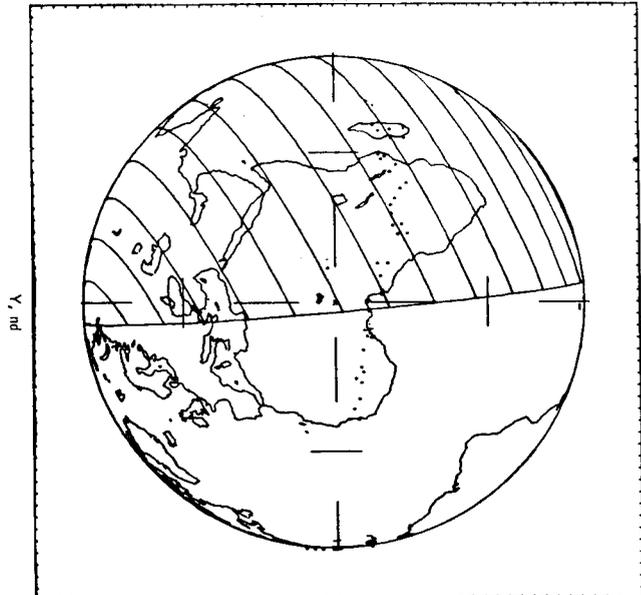


(ee) G.e.t. = 168 hours.

$R_E = 119\ 793$ n. mi.
 $V_i = 6001$ fps

$h_E = 133\ 892$ stat. mi.
 $V_i = 4092$ mph

Field of view = 4°

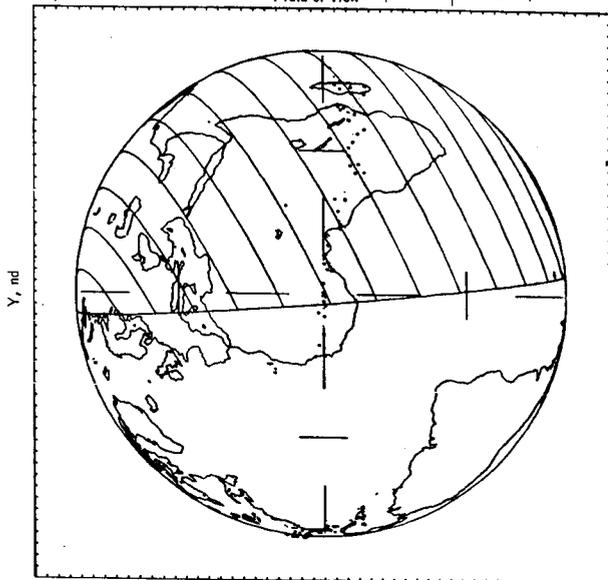


(ff) G.e.t. = 169 hours.

Figure 18.- Continued.

$R_E = 116\ 265$ n. mi. $h_E = 129\ 832$ stat. mi.
 $V_i = 6097$ fps $V_i = 4157$ mph

Field of view = 4°

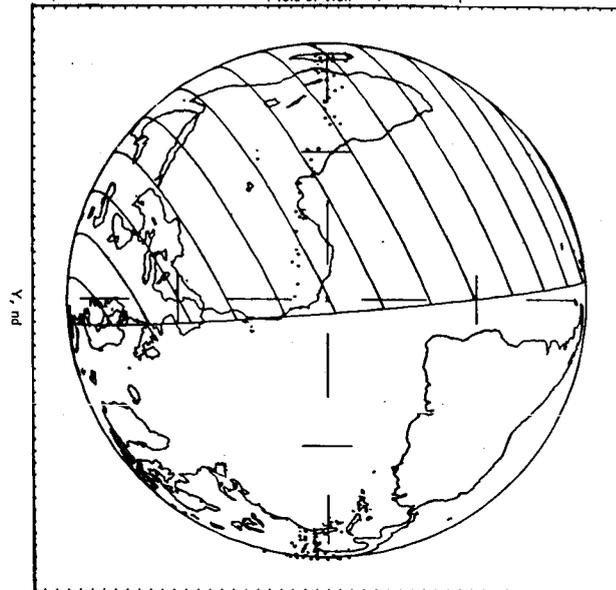


X, nd

(gg) G.e.t. = 170 hours.

$R_E = 112\ 681$ n. mi. $h_E = 125\ 709$ stat. mi.
 $V_i = 6199$ fps $V_i = 4227$ mph

Field of view = 4°

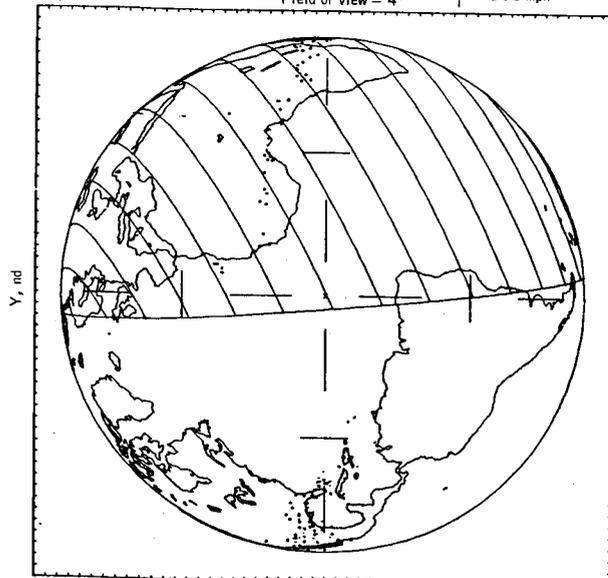


X, nd

(hh) G.e.t. = 171 hours.

$R_E = 109\ 038$ n. mi. $h_E = 121\ 515$ stat. mi.
 $V_i = 6308$ fps $V_i = 4301$ mph

Field of view = 4°

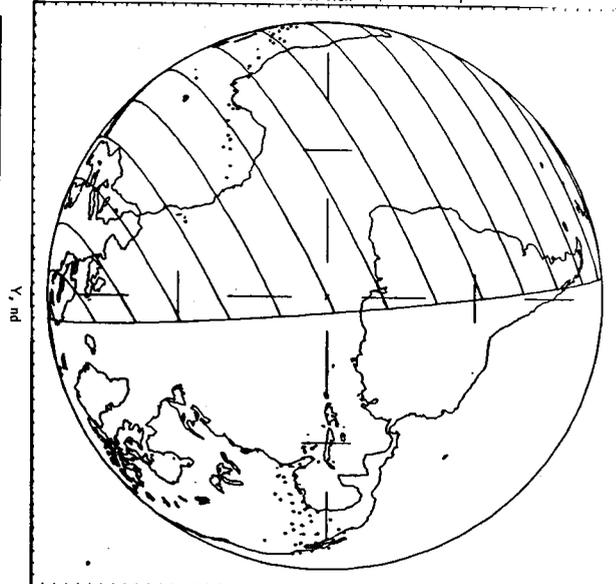


X, nd

(ii) G.e.t. = 172 hours.

$R_E = 105\ 331$ n. mi. $h_E = 117\ 250$ stat. mi.
 $V_i = 6425$ fps $V_i = 4381$ mph

Field of view = 4°



X, nd

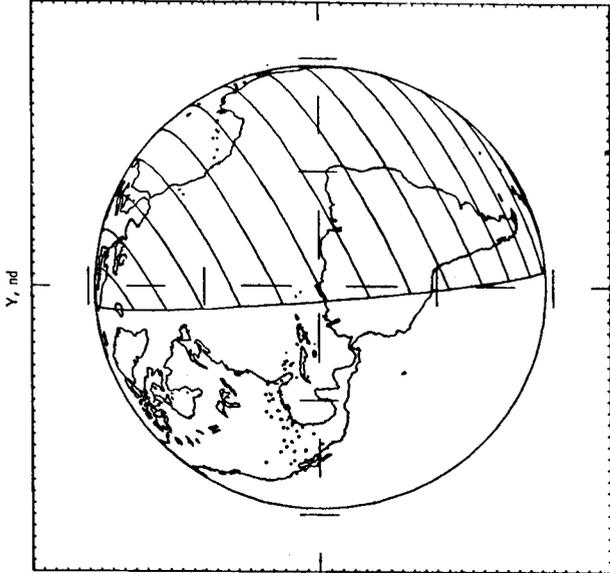
(jj) G.e.t. = 173 hours.

Figure 18. - Continued.

$R_E = 101\,556$ n. mi.
 $V_i = 6551$ fps

$h_E = 112\,906$ stat. mi.
 $V_i = 4467$ mph

Field of view = 5°



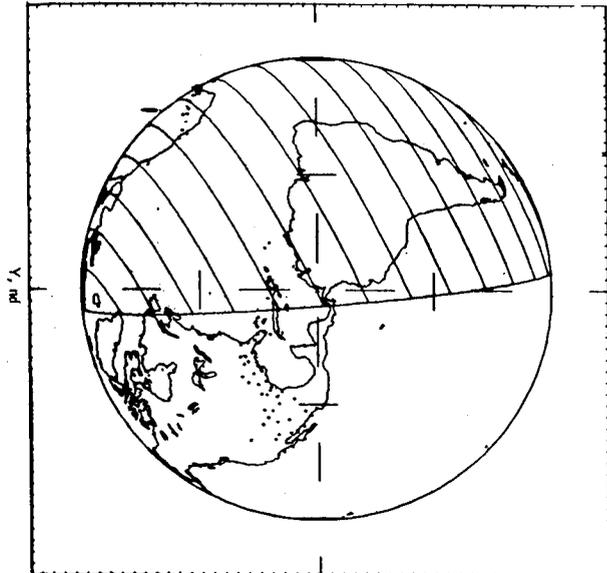
X, nd

(kk) G.e.t. = 174 hours.

$R_E = 97\,708$ n. mi.
 $V_i = 6686$ fps

$h_E = 108\,478$ stat. mi.
 $V_i = 4559$ mph

Field of view = 5°



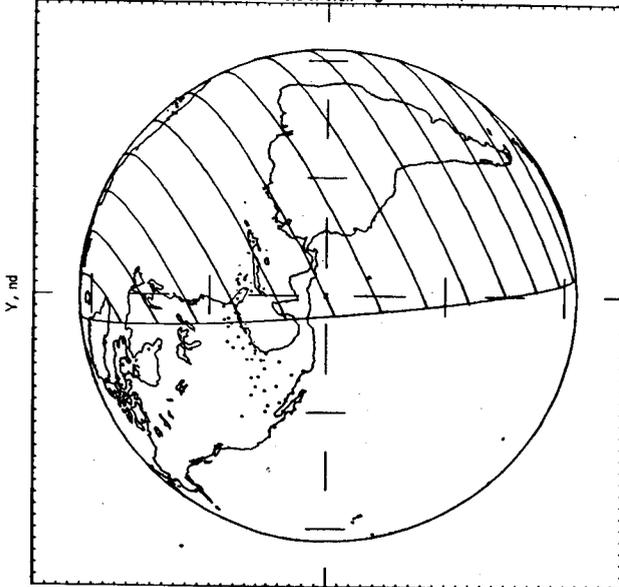
X, nd

(ll) G.e.t. = 175 hours.

$R_E = 93\,781$ n. mi.
 $V_i = 6832$ fps

$h_E = 103\,959$ stat. mi.
 $V_i = 4658$ mph

Field of view = 5°



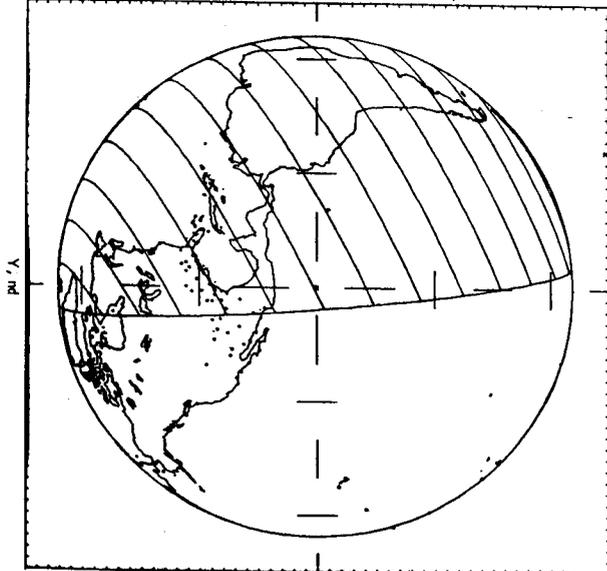
X, nd

(mm) G.e.t. = 176 hours.

$R_E = 89\,769$ n. mi.
 $V_i = 6991$ fps

$h_E = 99\,342$ stat. mi.
 $V_i = 4658$ mph

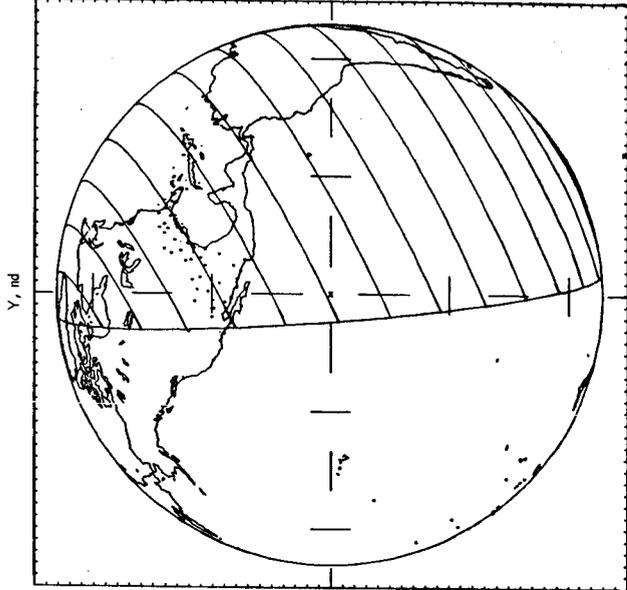
Field of view = 5°



X, nd

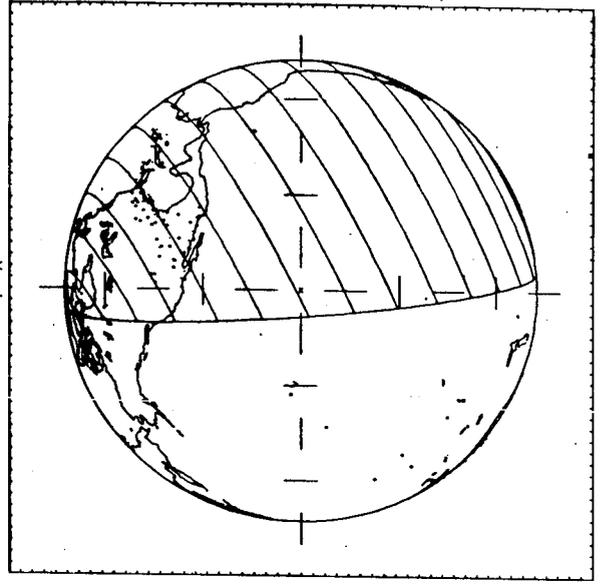
(nn) G.e.t. = 177 hours.

$R_E = 85\ 664$ n. mi.
 $V_i = 7166$ fps
Field of view = 5°
 $h_E = 94\ 618$ stat. mi.
 $V_i = 4886$ mph



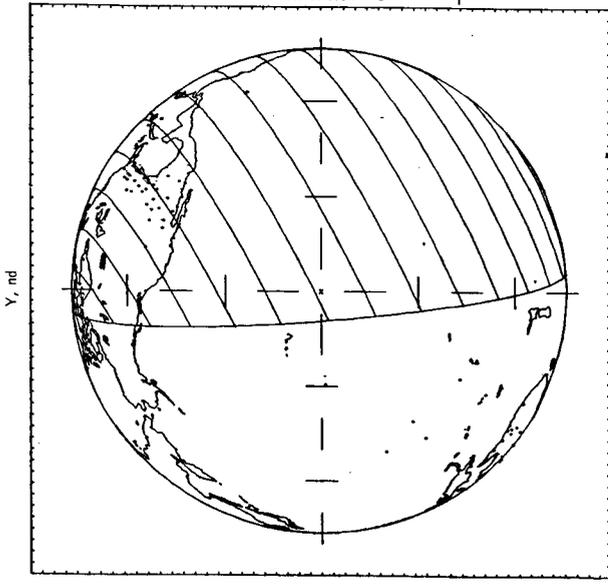
(oo) G.e.t. = 178 hours.

$R_E = 81\ 457$ n. mi.
 $V_i = 7357$ fps
Field of view = 6°
 $h_E = 89\ 776$ stat. mi.
 $V_i = 5016$ mph



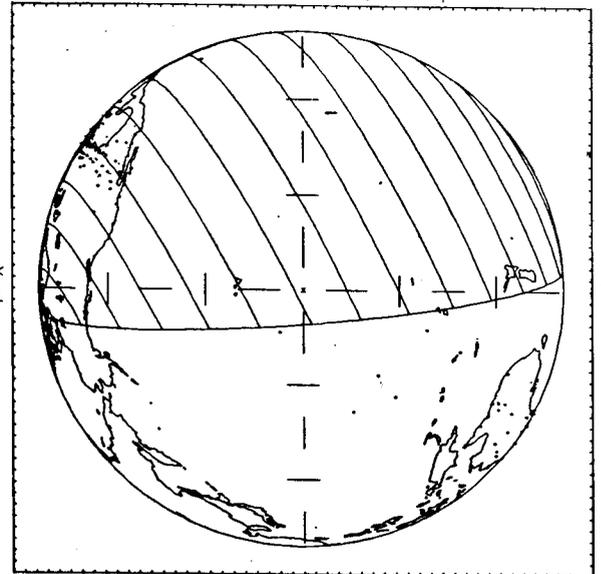
(pp) G.e.t. = 179 hours.

$R_E = 77\ 138$ n. mi.
 $V_i = 7571$ fps
Field of view = 6°
 $h_E = 84\ 807$ stat. mi.
 $V_i = 5162$ mph



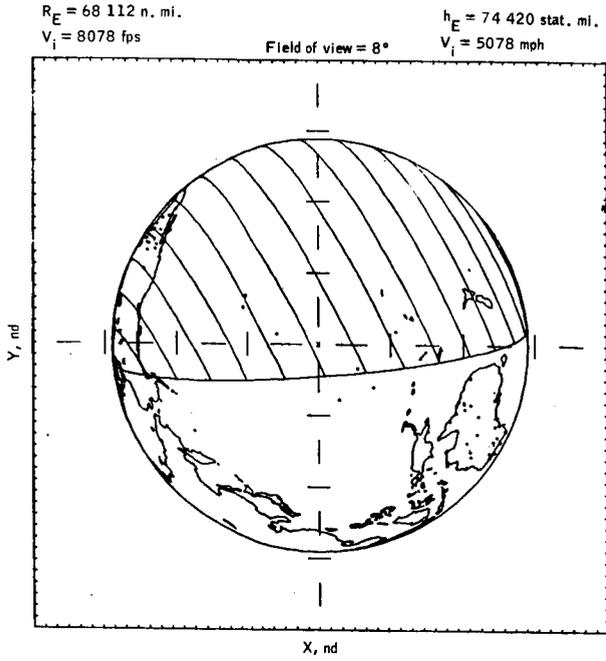
(qq) G.e.t. = 180 hours.

$R_E = 72\ 695$ n. mi.
 $V_i = 7809$ fps
Field of view = 6°
 $h_E = 79\ 692$ stat. mi.
 $V_i = 5324$ mph

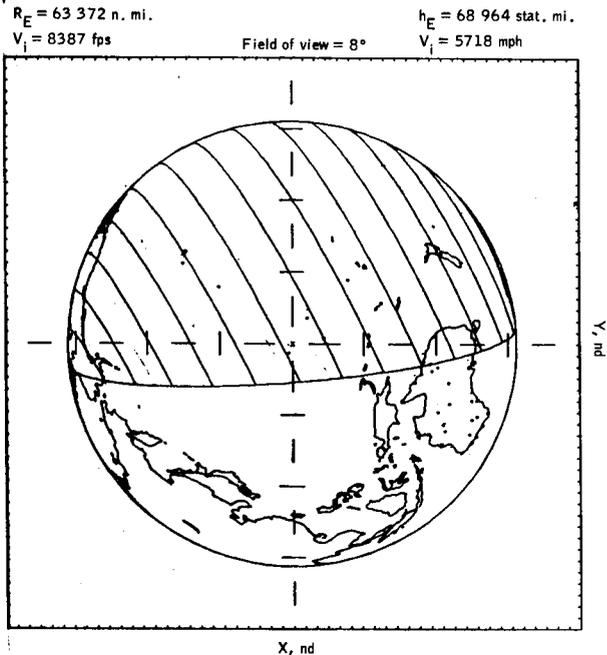


(rr) G.e.t. = 181 hours.

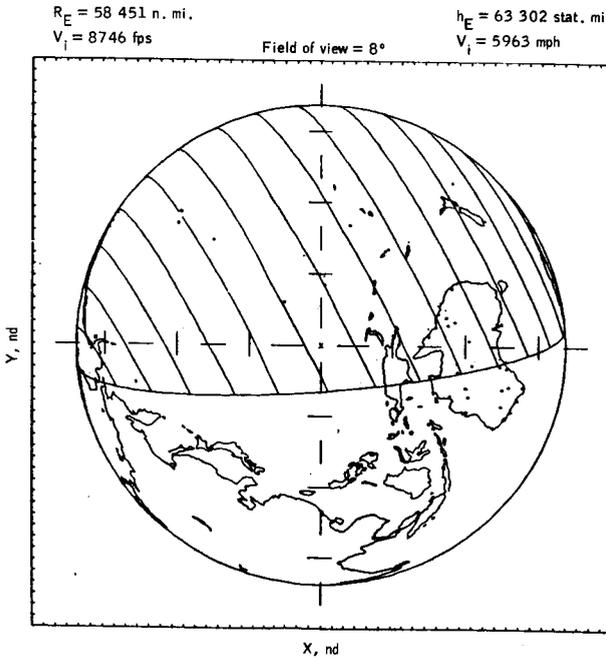
Figure 18.- Continued.



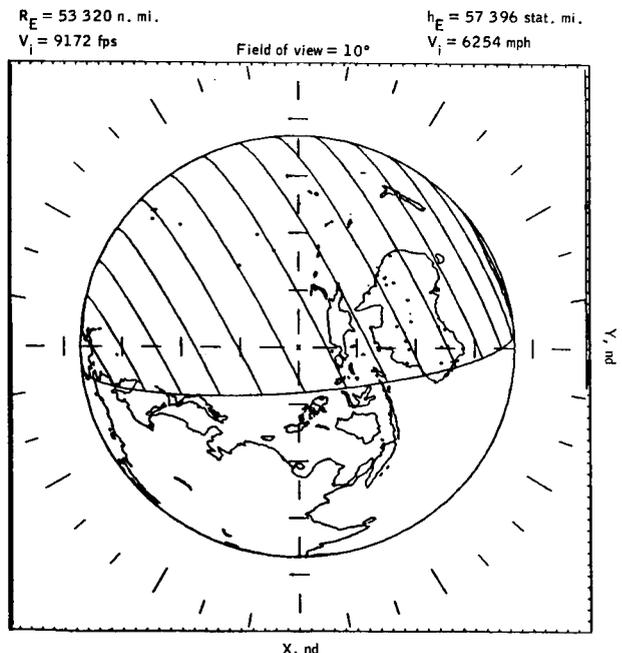
(ss) G.e.t. = 182 hours.



(tt) G.e.t. = 183 hours.



(uu) G.e.t. = 184 hours.

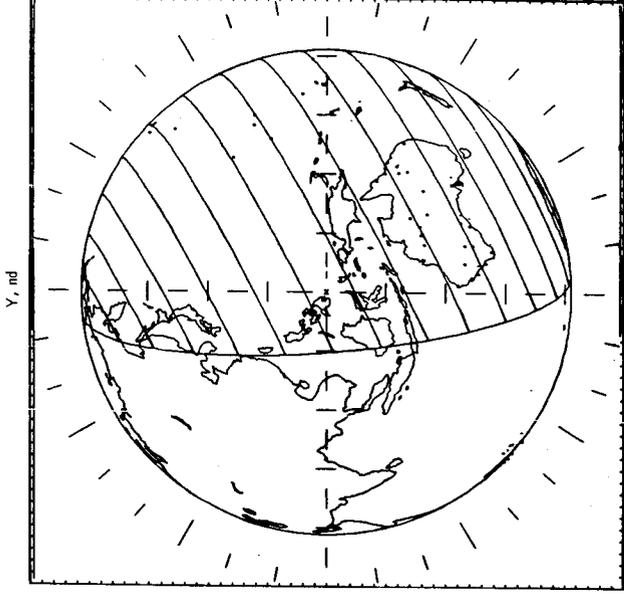


(vv) G.e.t. = 185 hours.

Figure 18.- Continued.

$R_E = 47\,938$ n. mi. $h_E = 51\,204$ stat. mi.
 $V_i = 9689$ fps $V_i = 6606$ mph

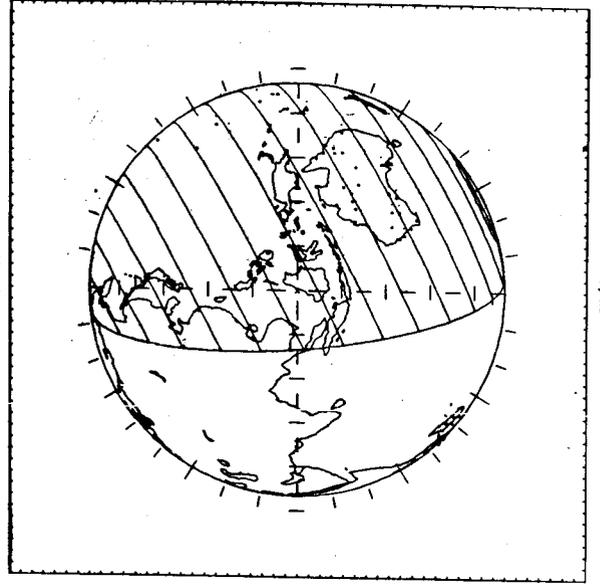
Field of view = 10°



(ww) G.e.t. = 186 hours.

$R_E = 42\,252$ n. mi. $h_E = 44\,661$ stat. mi.
 $V_i = 10\,338$ fps $V_i = 7049$ mph

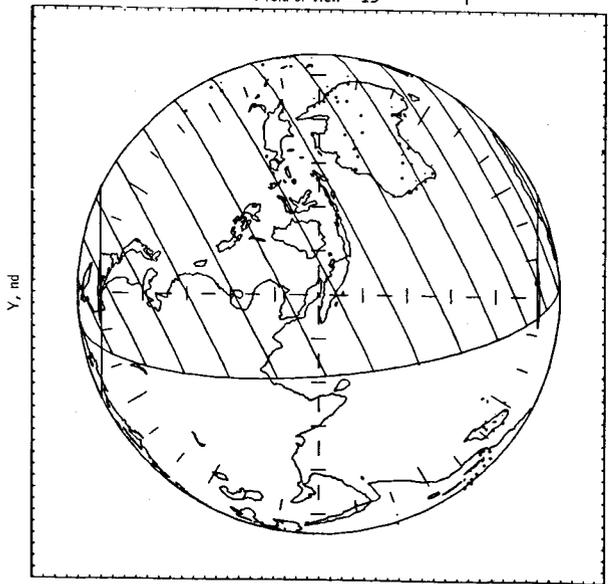
Field of view = 13°



(xx) G.e.t. = 187 hours.

$R_E = 36\,182$ n. mi. $h_E = 37\,674$ stat. mi.
 $V_i = 11\,192$ fps $V_i = 7631$ mph

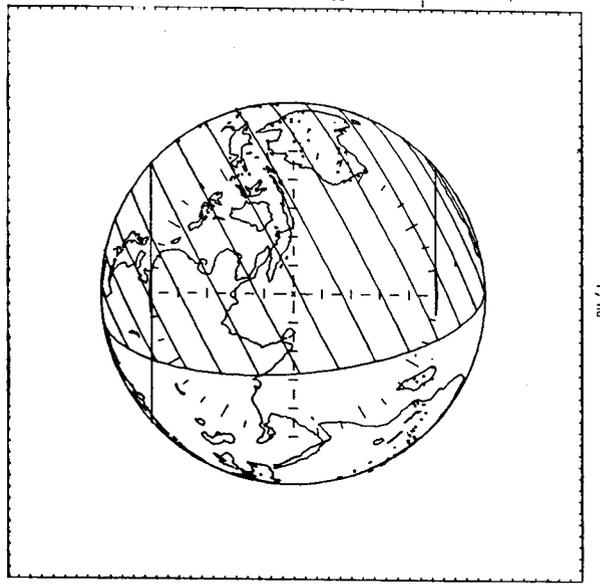
Field of view = 13°



(yy) G.e.t. = 188 hours.

$R_E = 29\,603$ n. mi. $h_E = 30\,103$ stat. mi.
 $V_i = 12\,399$ fps $V_i = 9762$ mph

Field of view = 20°



(zz) G.e.t. = 189 hours.

Figure 18.- Continued.

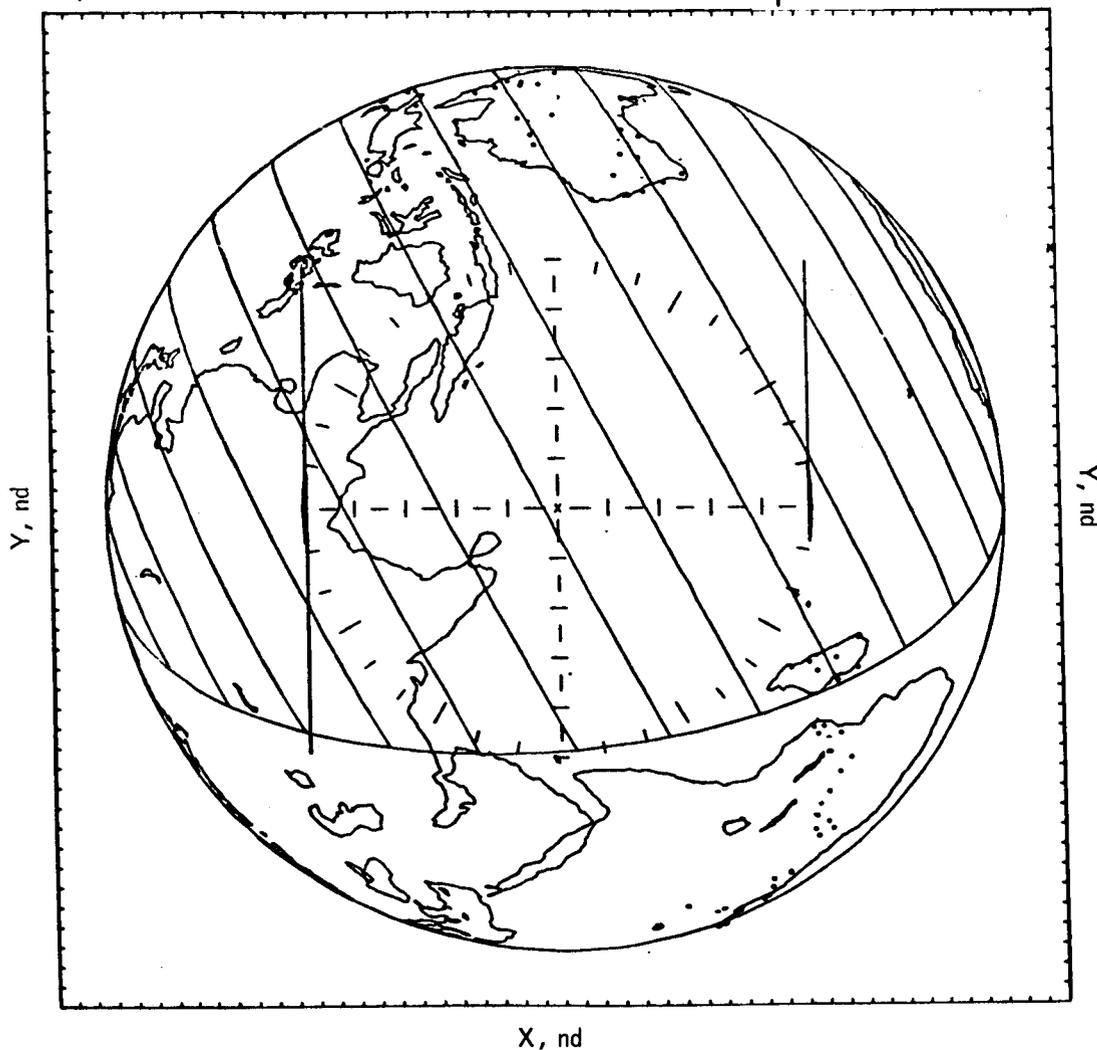
$R_E = 22\,296$ n. mi.

$V_i = 14\,318$ fps

$h_E = 21\,694$ stat. mi.

$V_i = 9762$ mph

Field of view = 20°



(aaa) G.e.t. = 190 hours.

Figure 18.- Concluded.

SEQ	286	290	308	349	356	362	377	440	473	480	507	509
X	70	24	22	-3	10	-1	23	12	0	-3	-21	-23
Y	21	15	12	13	9	11	1	-5	-6	-6	0	1

SEQ	515	535	540	580
X	-6	-6	-22	-20
Y	-11	-16	-4	-14

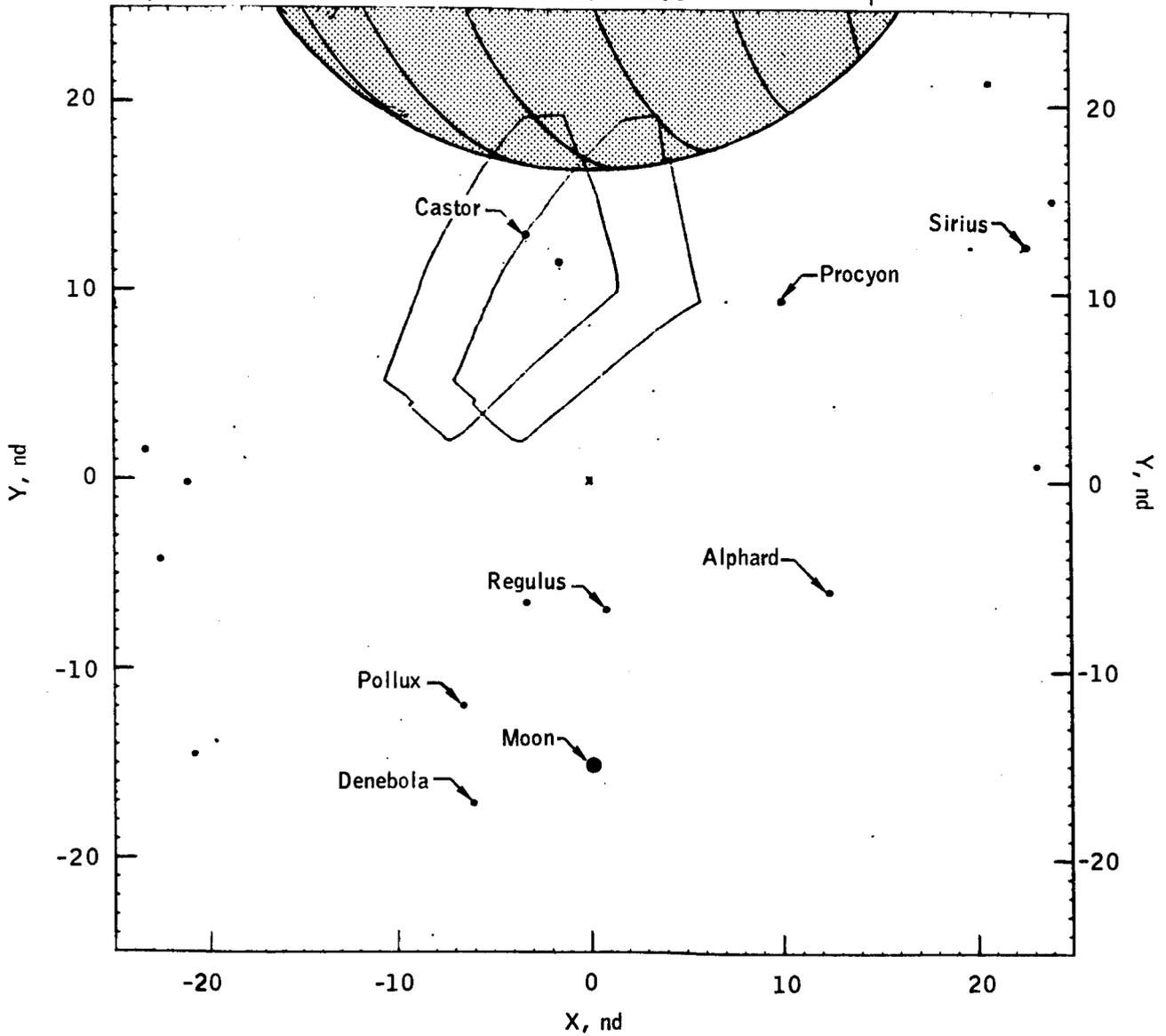
$R_E = 5426$ n. mi.

$V_i = 29\,175$ fps

$h_E = 2283$ stat. mi.

$V_i = 19\,892$ mph

Field of view = 100°



(a) 15 min prior to entry (g.e.t. = 191:35:32.2).

Figure 19.- Entry phase.

SEQ	290	308	356	362	377	440	473	480	507	509	515	535	540
X	24	23	10	-1	23	12	0	-3	-21	-23	-6	-5	-22
Y	18	15	13	15	4	-1	-2	-2	3	4	-7	-12	0

SEQ	551	570	580	582	610	651
X	7	-1	-20	-9	-16	-24
Y	-22	-22	-10	-21	-23	-23

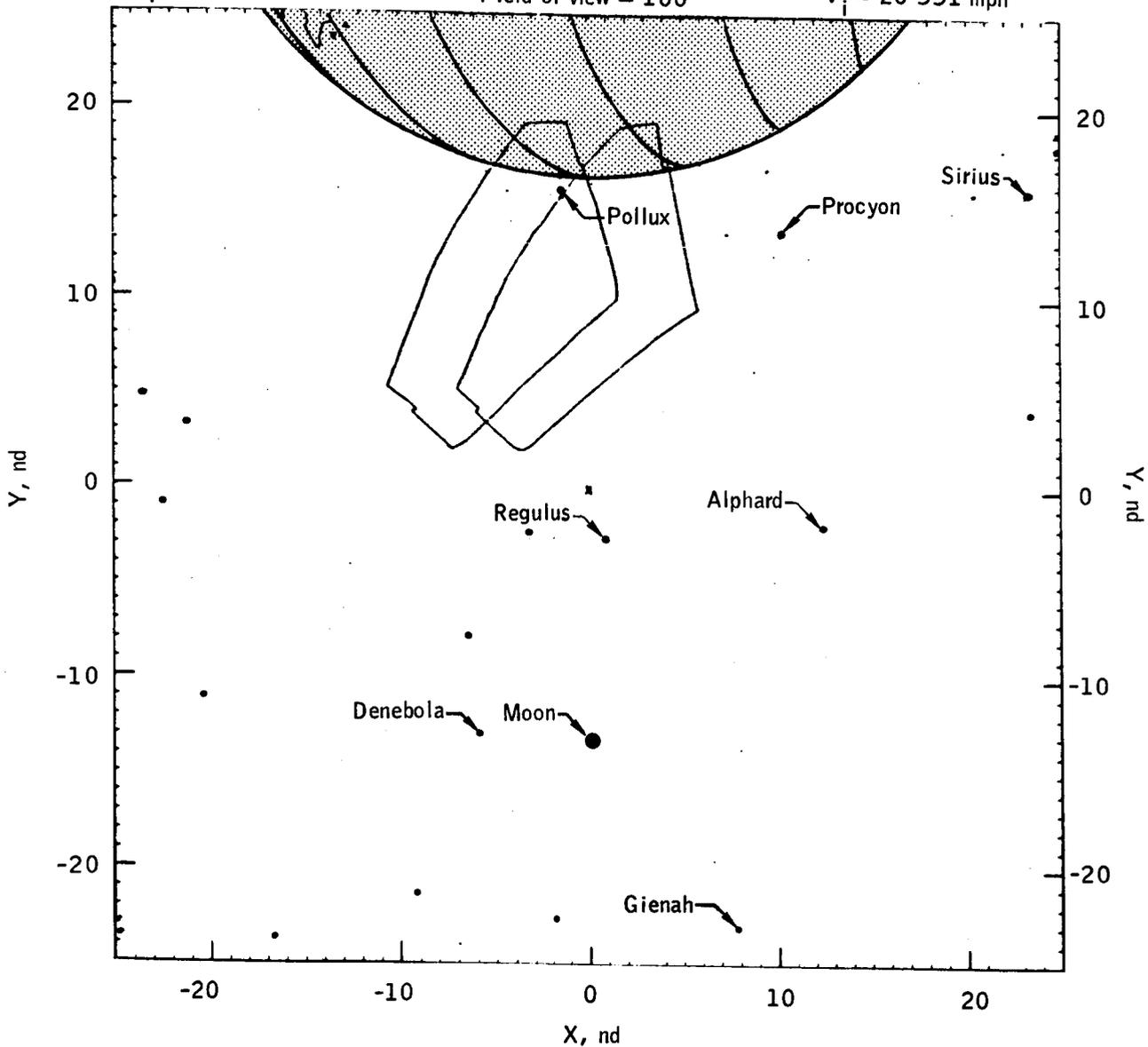
$R_E = 5085$ n. mi.

$V_i = 30\ 141$ fps

$h_E = 1891$ stat. mi.

$V_i = 20\ 551$ mph

Field of view = 100°



(b) 13 min prior to entry (g.e.t. = 191:39:32.2).

Figure 19. - Continued.

SEQ	378	377	440	473	480	507	509	515	535	540	545	551	566
X	24	23	12	0	-3	-21	-23	-6	-5	-22	24	7	9
Y	19	8	2	2	2	7	-8	-2	-7	3	-21	-18	-21

SEQ	570	580	582	583	610	624	651
X	-1	-19	-8	0	-15	-17	-23
Y	-17	-6	-16	-24	-19	-20	-19

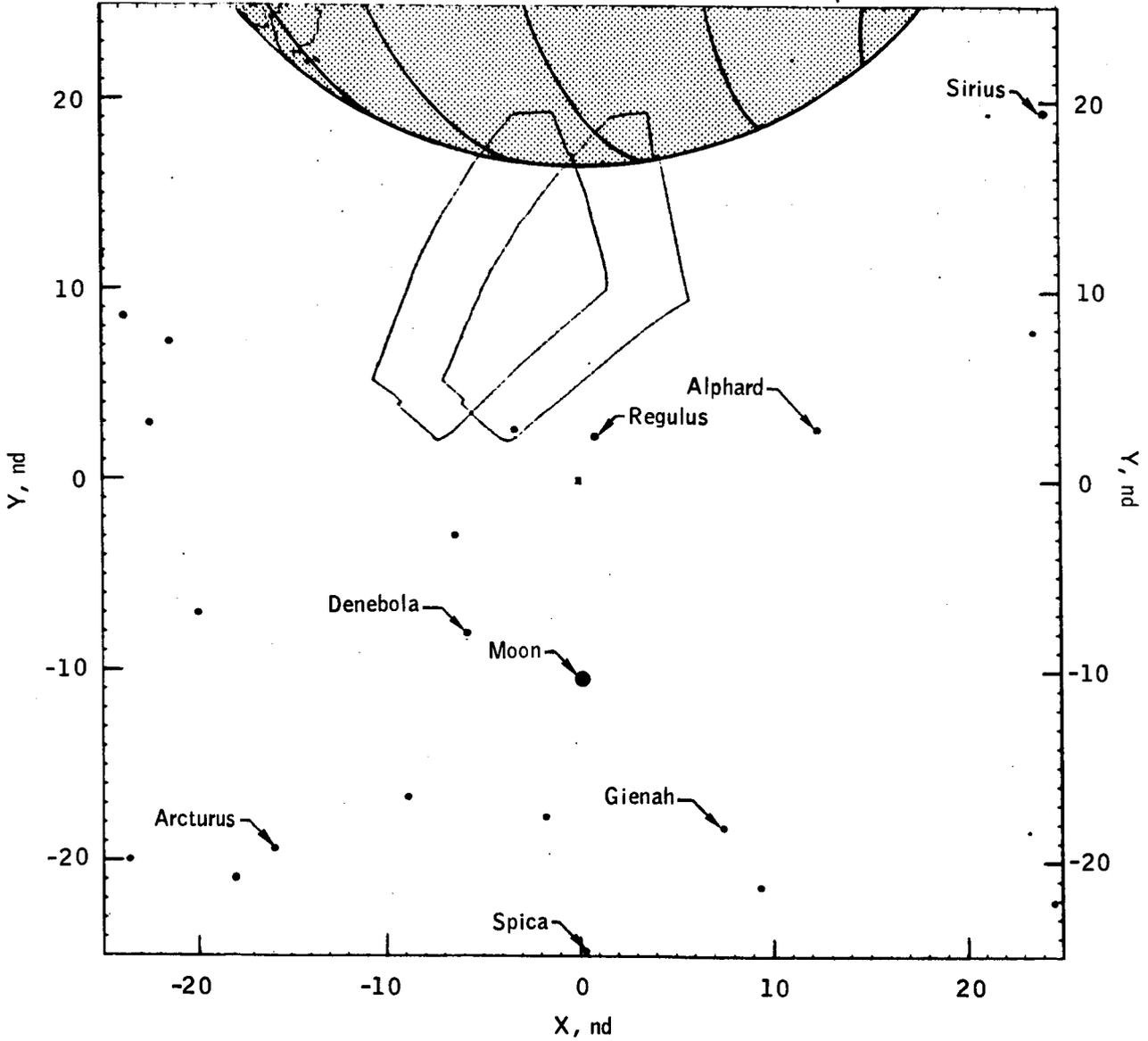
$R_E = 4756$ n. mi.

$h_E = 1512$ stat. mi.

$V_i = 31\,168$ fps

$V_i = 21\,251$ mph

Field of view = 100°



(c) 11 min prior to entry (g.e.t. = 191:39:32.2).

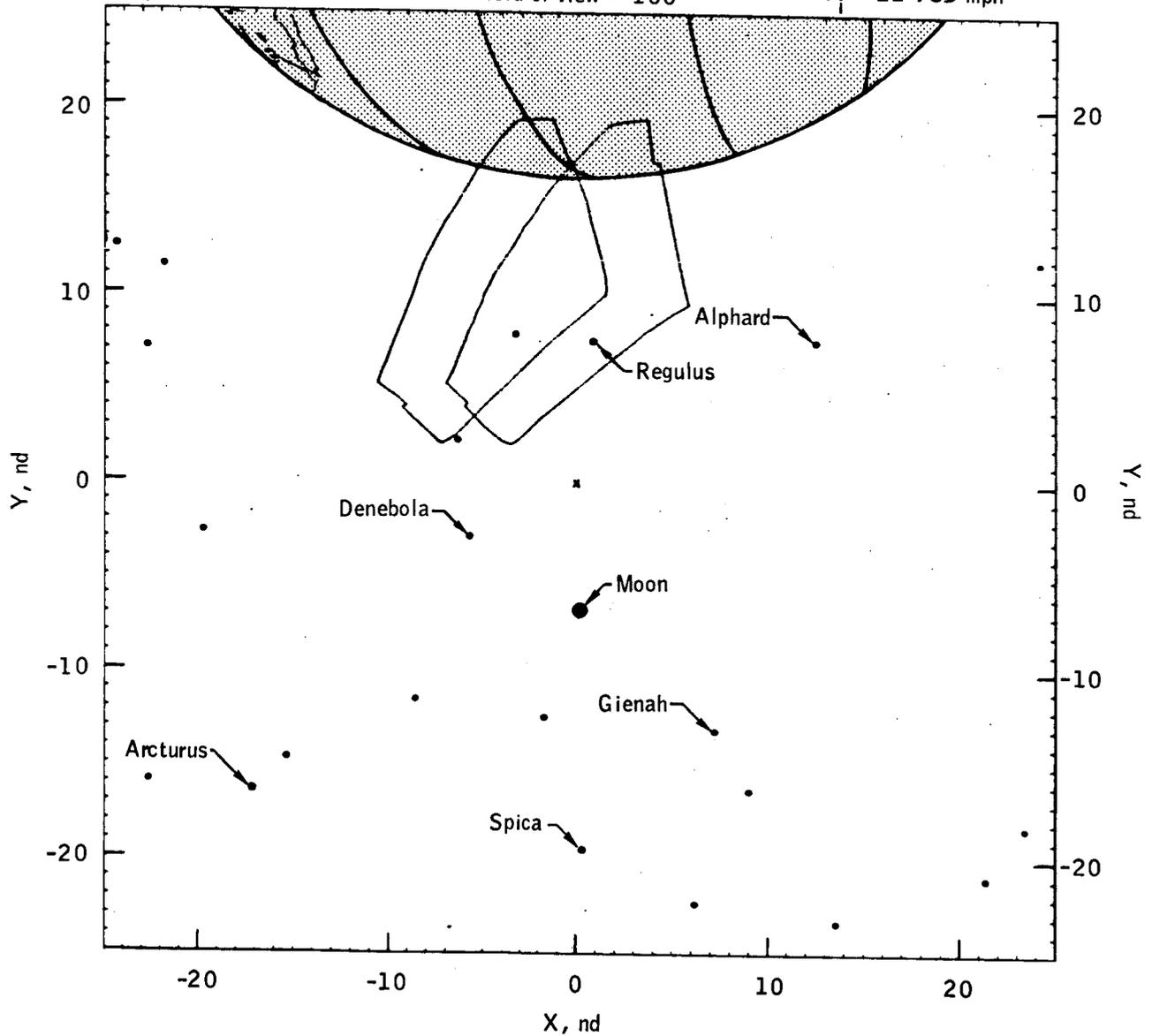
Figure 19. - Continued.

SEQ	377	440	473	480	507	509	515	535	540	545	551	566	569
X	24	12	0	-3	-21	-24	-6	-5	-22	23	7	9	21
Y	12	7	7	8	11	12	2	-2	7	-18	-12	-16	-20

SEQ	570	580	582	589	593	595	610	624	651
X	-1	-19	-8	13	0	6	-15	-17	-22
Y	-12	-2	-11	-23	-19	-22	-14	-16	-15

 $R_E = 4446 \text{ n. mi.}$
 $h_E = 1247 \text{ stat. mi.}$
 $V_i = 32\,242 \text{ fps}$
 $V_i = 21\,983 \text{ mph}$

Field of view = 100°



(d) 9 min prior to entry (g.e.t. = 191:41:32.2).

Figure 19. - Continued.

SEQ	440	473	480	507	515	535	540	545	551	561	566	569	570
X	12	0	-3	-22	-6	-5	-23	22	7	24	8	20	-1
Y	13	14	14	16	8	3	12	-13	-6	-16	-9	-15	-5

SEQ	580	582	589	593	595	599	610	617	621	624	651	655	700
X	-19	-8	12	0	5	20	-14	23	10	-16	-21	-1	-16
Y	2	-5	-17	-12	-15	-20	-8	-23	-21	-10	-10	-23	-23

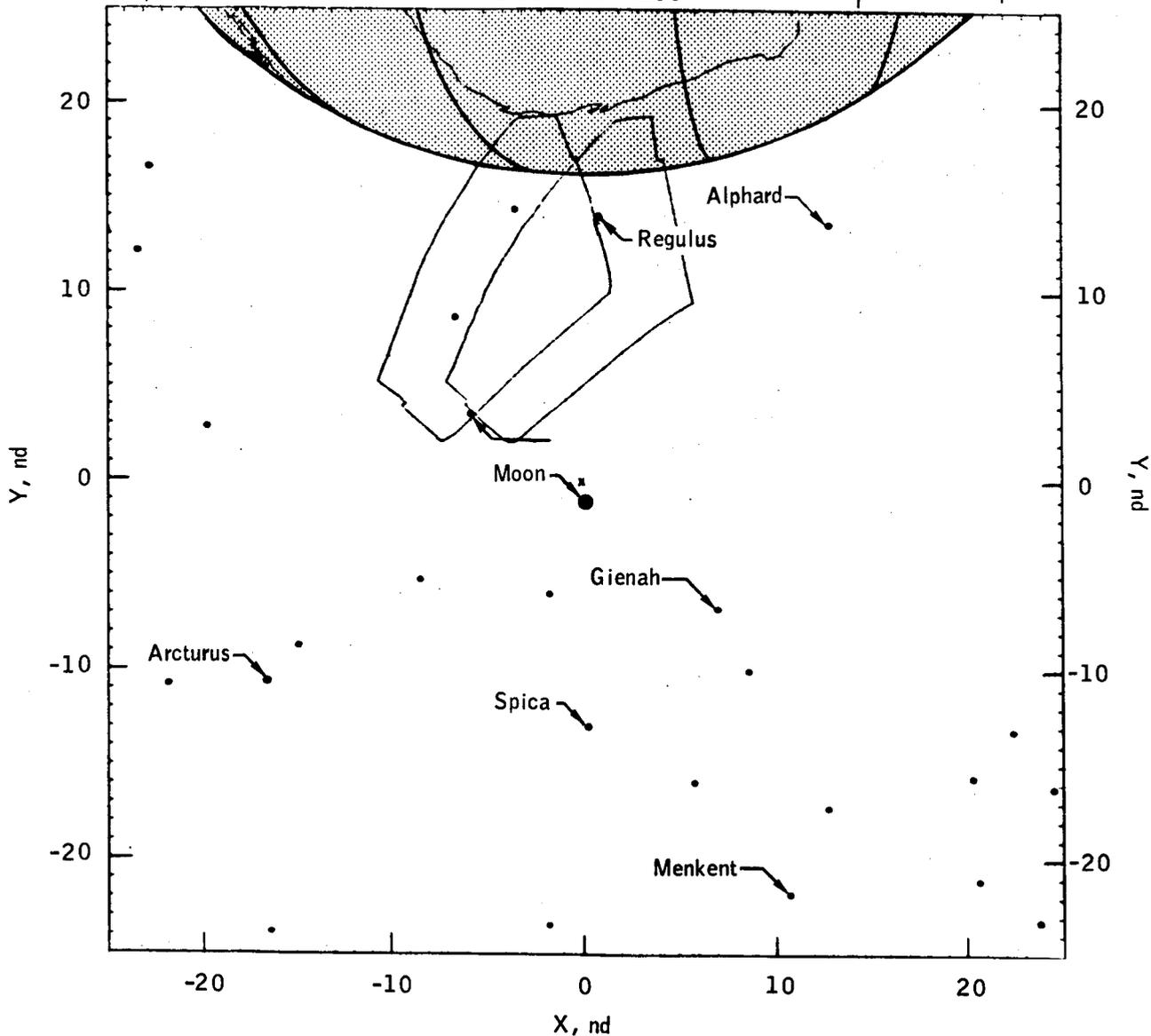
$R_E = 4161$ n. mi.

$h_E = 819$ stat. mi.

$V_i = 33\,330$ fps

$V_i = 22\,725$ mph

Field of view = 100°



(e) 7 min prior to entry (g.e.t. = 191:43:32.2).

Figure 19. - Continued.

SEQ	515	535	540	545	551	561	566	569	570	574	580	582	589	593	595
X	-8	-5	-24	-21	8	23	8	19	-1	24	-20	-8	12	0	5
Y	15	10	17	-7	0	-10	-2	-9	1	-12	9	1	-10	-5	-8
SEQ	599	610	617	621	624	641	643	645	651	655	660	673	688	690	700
X	19	-14	22	10	-16	12	21	14	-21	-1	12	-6	10	-24	15
Y	-14	-1	-17	-14	-4	-18	-20	-19	-4	-16	-20	-17	-23	-9	-17

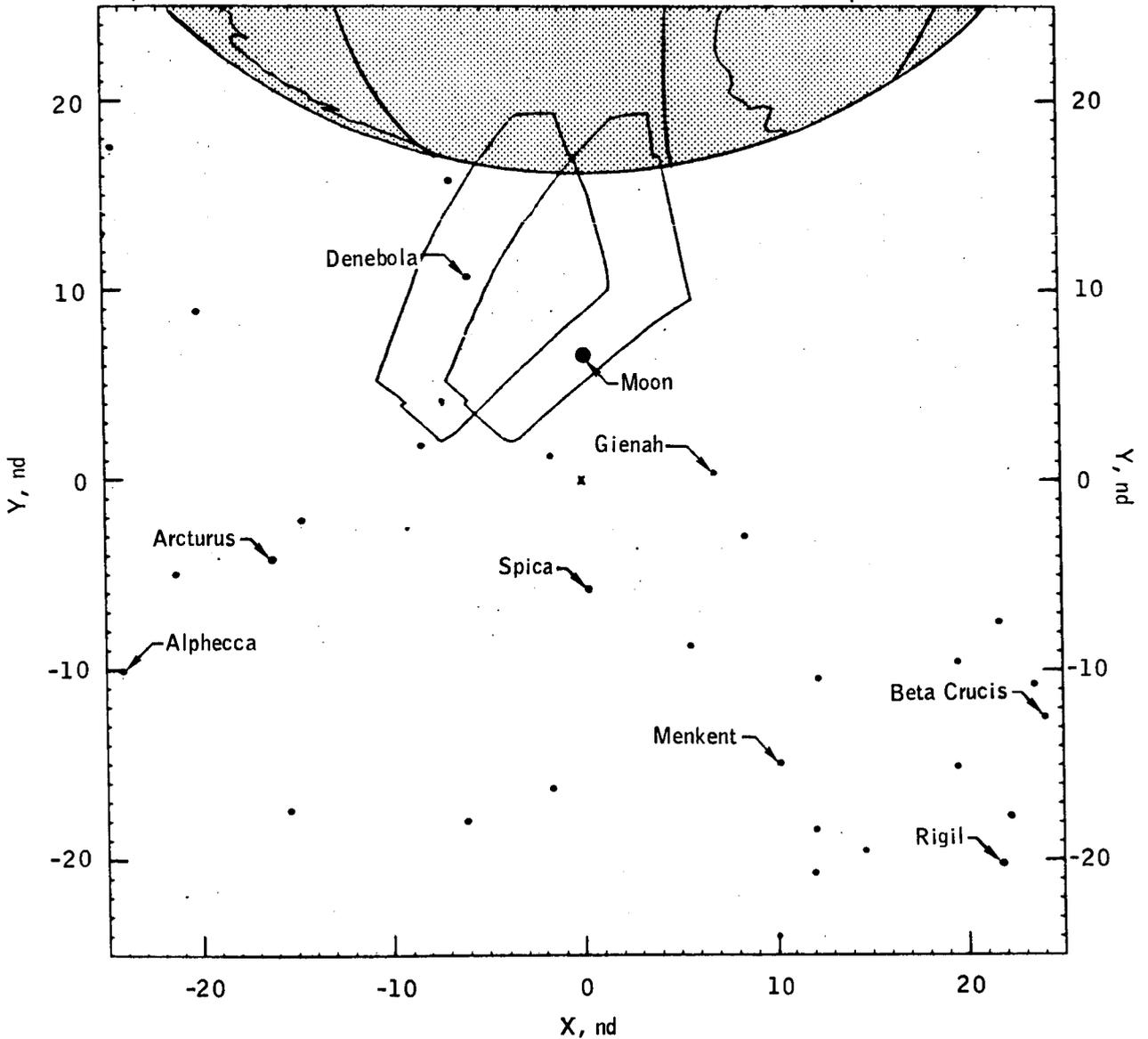
$R_E = 3910$ n. mi.

$V_i = 34\,384$ fps

$h_E = 540$ stat. mi.

$V_i = 23\,444$ mph

Field of view = 100°



(f) 5 min prior to entry (g.e.t. = 191:45:32.2).

Figure 19. - Continued.

SEQ	545	551	561	566	569	570	574	580	582	589	593	595	599
X	21	7	22	8	19	-1	23	-20	-8	12	0	5	10
Y	0	8	-4	5	-2	9	-5	16	10	-2	2	0	-7
SEQ	610	617	621	624	641	643	645	651	655	660	673	688	
X	-14	21	9	-16	11	20	13	-21	-1	11	-5	9	
Y	5	-10	-6	3	-10	-13	-11	2	-7	-12	-9	-15	
SEQ	690	700	717	719	724	736	743	745	751	753	757	759	770
X	-23	-14	1	0	-2	0	0	-23	1	-8	23	4	-6
Y	-3	-9	-16	-16	-16	-19	-20	-11	-20	-19	-20	-22	-23

SEQ 795 803
 X -22 -18
 Y -21 -24

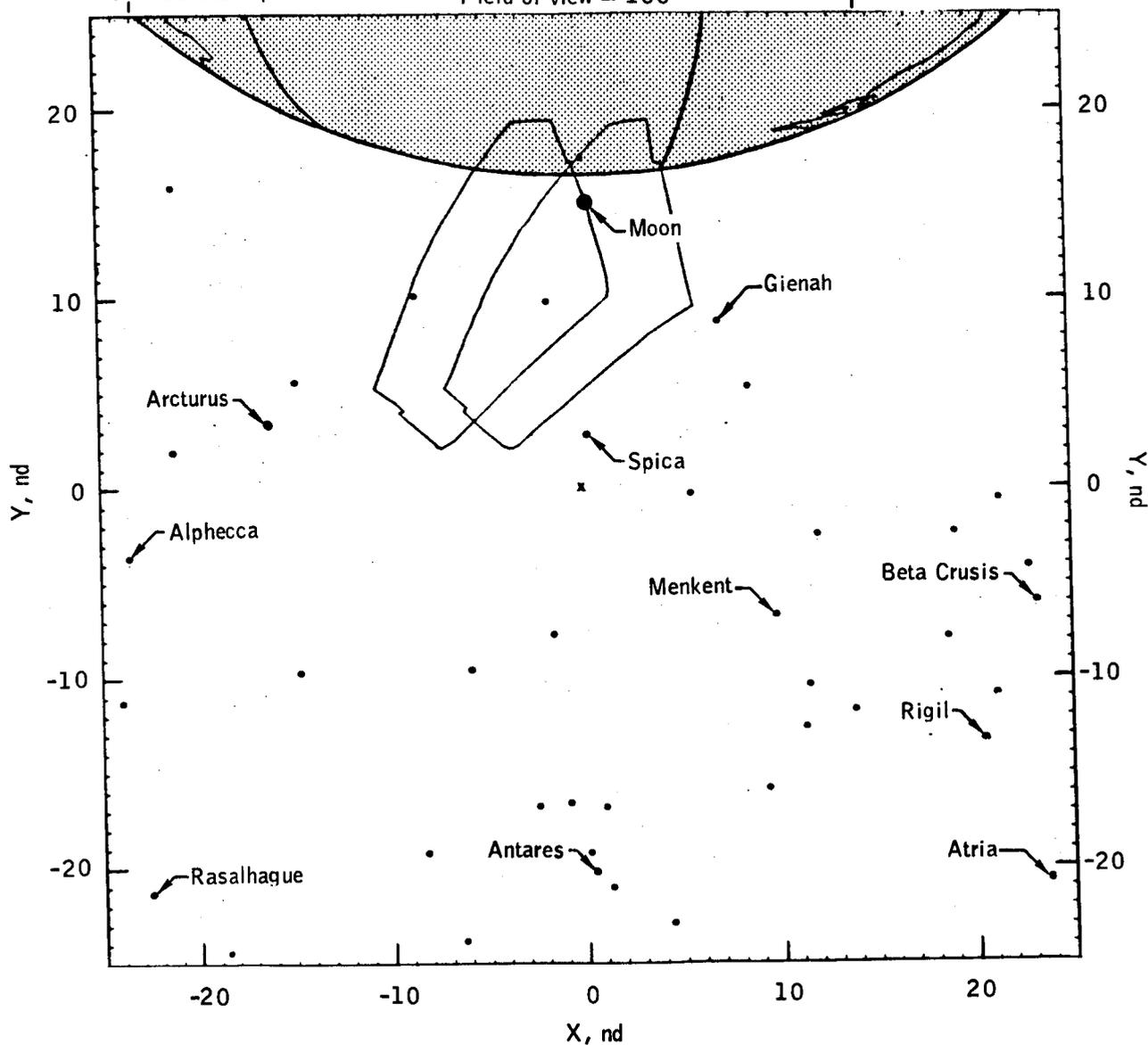
$R_E = 3706$ n. mi.

$V_i = 35\ 325$ fps

Field of view = 100°

$h_E = 304$ stat. mi.

$V_i = 24\ 085$ mph



(g) 3 min prior to entry (g.e.t. = 191:47:32.2).

Figure 19. - Continued.

SEQ	545	561	566	569	574	589	593	595	599	610	617	621	624	641	643
X	21	22	8	19	23	12	0	5	18	-15	20	9	-16	11	19
Y	6	2	13	5	0	5	11	8	0	13	-3	1	11	-1	-5
SEQ	645	651	655	660	673	688	690	700	712	719	724	736	743	745	751
X	13	-21	-1	10	-5	8	-23	-14	8	8	-2	0	0	-23	1
Y	-3	9	1	-4	0	-7	3	-1	-7	-7	-7	-10	-11	-4	-12
SEQ	753	757	769	770	781	789	790	793	795	797	802	803	836	841	844
X	-7	22	4	-5	15	5	12	5	-21	8	6	-17	1	3	-1
Y	-10	-13	-14	-15	-17	-18	-17	-18	-14	-18	-19	-16	-23	-23	-24

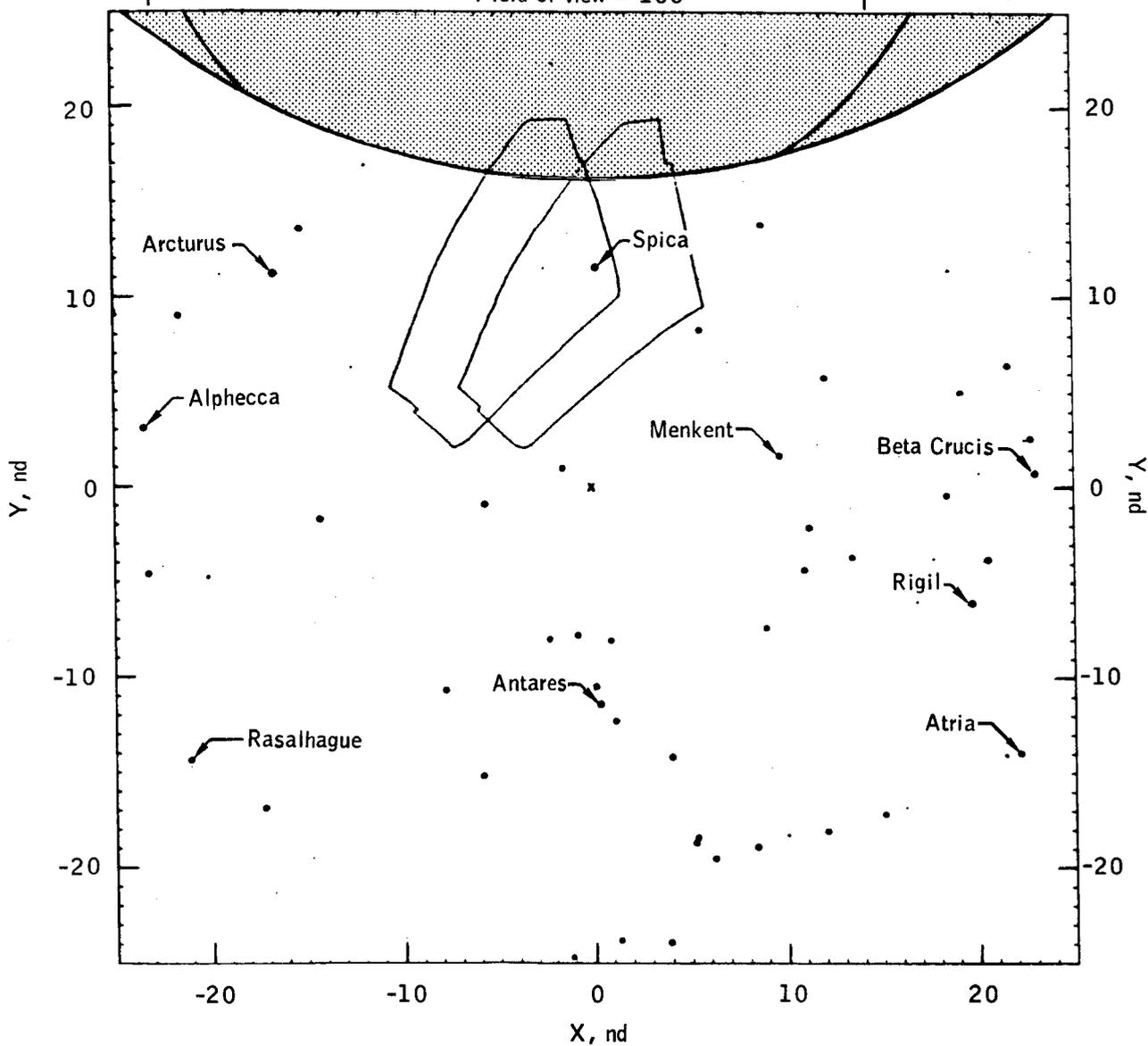
$R_E = 3557$ n. mi.

$h_E = 132$ stat. mi.

$V_i = 36\,055$ fps

$V_i = 24\,583$ mph

Field of view = 100°



(h) 1 min prior to entry (g.e.t. = 191:49:32.2).

140

SEQ	545	546	549	574	589	593	595	599	617	621	641	643	645
X	21	22	19	23	12	0	5	18	20	9	11	19	13
Y	10	6	8	4	10	16	12	3	0	6	2	02	0
SEQ	651	655	660	673	688	690	700	717	719	724	736	743	
X	-21	-1	10	-5	8	-23	-14	0	0	-2	0	0	
Y	12	5	0	3	-2	6	2	-3	-3	-3	-5	-6	
SEQ	745	751	753	757	759	770	781	789	790	793	795	797	802
X	-23	1	-7	21	4	-5	14	5	11	5	-20	8	6
Y	0	-7	-6	-10	-9	-10	-12	-13	-13	-14	-10	-64	-14
SEQ	803	836	841	844	861	871	933						
X	-16	1	3	-1	0	1	18						
Y	-12	-19	-19	-19	-22	-23	-24						

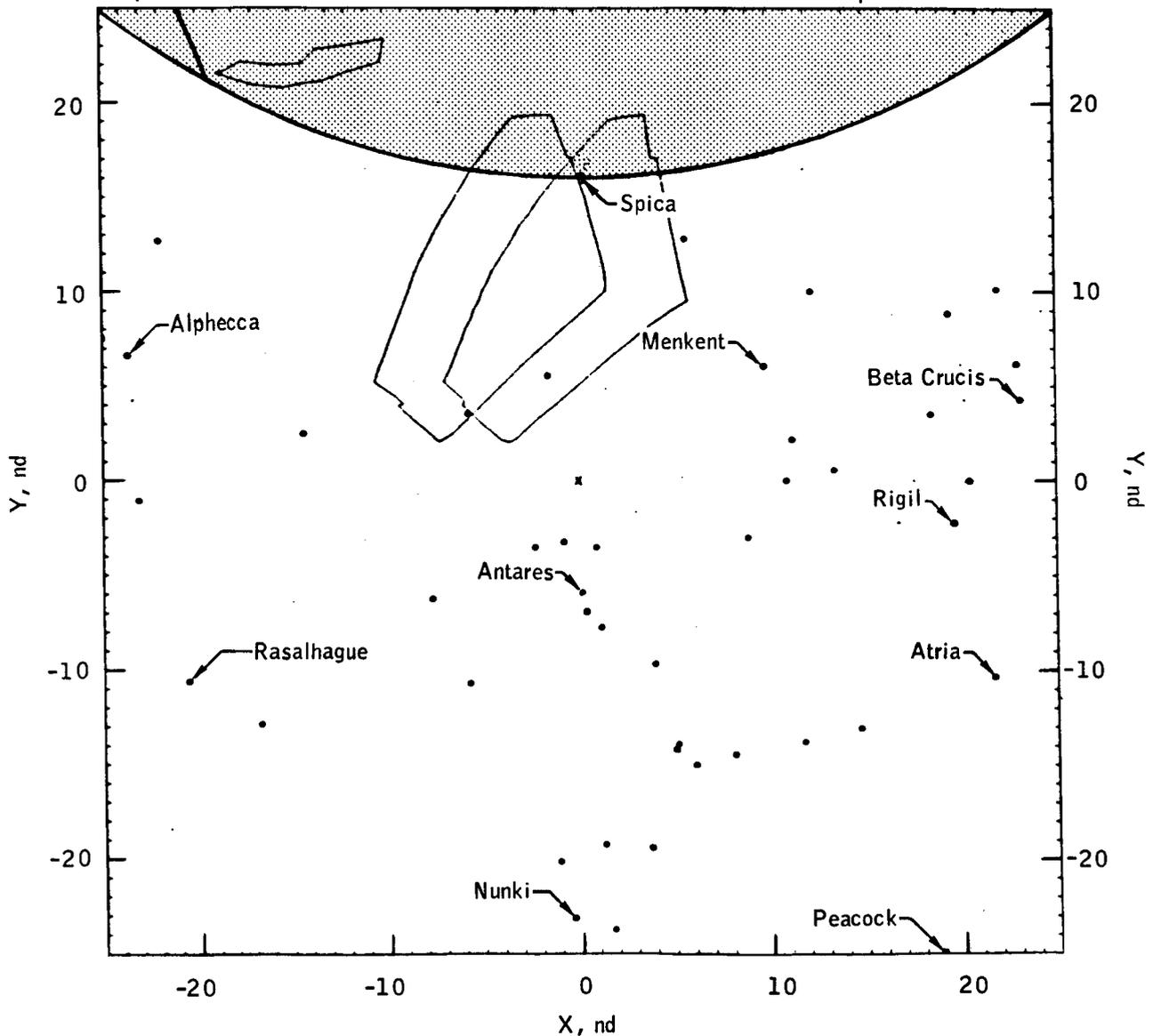
$R_E = 3508$ n. mi.

$V_i = 36\,309$ fps

Field of view = 100°

$h_E = 76$ stat. mi.

$V_i = 24\,756$ mph



(i) Entry interface (g.e.t. = 191:50:32.2).

Figure 19.- Concluded.

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1. Lunde, Alfred N.: Views From the Spacecraft During Apollo 10 (Mission F). MSC IN 69-FM-74, March 21, 1969.
2. Rogers, Joseph E.; and Burton, John K.: Apollo 8 Reentry Crew Charts. MSC memo 68-FM23-216, December 12, 1968.
3. OMAB; LMAB; and LAB: The Spacecraft Operational Trajectory for Apollo 10 (Mission F), Volume II. MSC IN 69-FM-97,